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A fast and robust algorithm for General Defocusing Particle Tracking

Massimiliano Rossi¹^{*} and Rune Barnkob^{2†}

 1 Department of Physics, Technical University of Denmark,

DTU Physics Building 309, DK-2800 Kongens Lyngby, Denmark

 2 Heinz-Nixdorf-Chair of Biomedical Electronics, Department of Electrical and Computer Engineering,

Technical University of Munich, TranslaTUM, 81675 Munich, Germany

The increasing use of microfluidics in industrial, biomedical, and clinical applications requires a more and more precise control of the microfluidic flows and suspended particles or cells. This leads to higher demands in three-dimensional and automated particle tracking methods, e.g. for use in feedback-control systems. General Defocusing Particle Tracking (GDPT) is a 3D particle tracking method based on defocused particle images which is easy to use and requires standard laboratory equipment. In this work, we describe in details a fast and robust algorithm for performing GDPT, which is suitable for automatized and real-time applications. Its key feature is a fast, segmentationfree approach to identify particles and estimate their 3D position. This detection step is followed by a refinement and iteration step to improve accuracy and identification of overlapping particles. We show that the algorithm is versatile and can be applied to different types of images (darkfield and brightfield). We use synthetic image sets of varying particle concentration to evaluate the performance of the algorithm in terms of detected depth coordinate uncertainty, particle detection rate, and processing time. The algorithm is applied and validated on experimental images showing that it is robust towards background or illumination fluctuations. Finally, to test the algorithm on real-time applications, we use synthetic images to set up a simulation framework with experimentally-relevant parameters and where the true particle positions are known.

I. INTRODUCTION

The recent advancements in microfluidic devices, specially in fields like biology or medicine, require more and more precise and continuous measurements of microfluidic flow fields and suspended particles. In particular, two main needs are emerging in this domain: tools that can effectively be operated by non-expert users like biologists or physicians, and automated, real-time methods suitable for active force and flow control (e.g. to allow single-cell manipulation [1]). Since the first application of microscopic PIV [2], about two decades ago, several velocimetry and particle tracking methods have been proposed as diagnostic tools for microfluidics, both in 2D and 3D, using different principles such as defocusing [3, 4], astigmatic aberration [5, 6], evanescent waves [7], holography $[8]$, and tomography $[9]$. However, most of these methods require complex calibration procedures as well as experienced users to properly perform a measurement and are therefore not accessible to a wider community neither for usage nor for further development [10].

One method with the potential to meet these needs is the General Defocusing Particle Tracking (GDPT) which was proposed by Barnkob *et al.* [11] and is illustrated in Fig. 1. The general requirements for the GDPT method is an optical system with small depth of field (particle images must have different shapes depending on their depth positions) and a set of reference images showing the particle image shapes at different known positions. Both requirements are typically fulfilled in microfluidic

applications, where large magnification objective lenses are used and where the calibration images can easily be obtained by a systematic scanning of the microscope focus. Moreover, distortions in microscopic objectives are typically small and the defocusing patterns are consistent across the entire camera sensor [12]. GDPT can indifferently be used on brightfield, darkfield, or fluorescent images as long as the image contrast is sufficiently high. Furthermore, in a standard GDPT algorithm, such as the free-to-use GDPTlab [13], most outliers (i.e. false positive) can be easily filtered out based on a single similarity parameter that evaluates how well a target image is matched to the calibration images. Therefore, and due to its simplicity, GDPT is receiving an increasing interest in microfluidics and lab-on-a-chip communities [14– 16]. Here in particular within the acoustic manipulation of microparticles $[17–22]$, where information about the three-dimensional acoustophoretic behavior is crucial to further development as well as for the translation to industrial and clinical use, where feedback control is essential to secure stable and viable conditions [23, 24].

In this work, we present a new algorithm to perform GDPT measurements in a fast, automated and versatile fashion. Its key feature is a segmentation-free approach to identify particles and estimate their 3D position. This detection step is followed by a refinement and iteration step to improve the accuracy and the identification of overlapping particles. The performance of the algorithm is evaluated using the benchmark dataset provided in Ref. 12 with respect to error, valid detected particles, and processing time. Following, the algorithm is validated on experimental images with distortions and aberrations for the tracking of the three-dimensional motion of tracer particles inside an evaporating drop. Furthermore, we

[∗] rossi@fysik.dtu.dk

[†] rune.barnkob@tum.de

(a) 3D particle tracking using General Defocusing Particle Tracking (GDPT)

FIG. 1. Example of single-camera, 3D particle tracking performed by General Defocusing Particle Tracking (GDPT). (a) Suspended microparticles are imaged with a conventional microscope resulting in 2D images with defocused particle images. The depth positions of the particles are determined by comparing their images to a reference set of already-acquired experimental particle images at known depth positions (calibration model). (b) The calibration model is obtained from a set of calibration images acquired experimentally by taking subsequent images of one or more reference particles displaced at known positions, e.g. by observing sedimented particles using a motorized microscope focusing stage. (c) The depth coordinate uncertainty and processing time can be estimated prior to the experiment by applying the tracking algorithm to the set of calibration images with the calibration model as input.

created a simulation framework to test the algorithm for use in real-time applications. The simulation is created using a combination of synthetic images [25] and analytical predictions of particle trajectories in acoustofluidic devices [26].

II. ALGORITHM DESCRIPTION

The essential elements of the GDPT method is the calibration model consisting of a set of calibration images that maps defocused (or astigmatic) particle images with their respective depth position z and a methodology to compare the similarity between a target particle image and the calibration images. Typically, the set of calibration images is obtained experimentally by taking subsequent images of a reference particle which is displaced at known positions, e.g. using a motorized focusing stage while observing a sedimented particle, see Fig. 1(b) $[11, 12]$. In Refs. 11 and 12, and in this work, we use a calibration model based on calibration images of a single particle (calibration stack) and the

normalized cross-correlation function [27]. The normalized cross-correlation is used to rate the similarity between target and calibration images, using its maximum peak value as the similarity coefficient, referred to as C_m , see Fig. 2(a,ii). The values of C_m can range from 0 to 1, with 1 corresponding to a perfect match between the target image and a calibration image.

A conventional approach for GDPT measurements consists of the following steps [11, 13]:

- identify candidate particles using image segmentation.
- for each candidate particle, identify the best matching calibration image through C_m using an optimized iterative procedure,
- \bullet for each candidate particle, determine the z position with "sub-image" resolution through interpolation in (z, C_m) .

This procedure is very accurate, however, it is relatively slow since it needs to compute a large number of crosscorrelations. For instance, the optimized approach in

FIG. 2. Overview of the detection step. (a) The calibration model is based on a single calibration stack of N_{cal} single-particle calibration images. (i) A subset of N_{sub} calibration images is extracted. (ii) The similarity between two particle images is evaluated through the parameter C_m , which represents the (local) peak value of the normalized cross-correlation (\star) between two images. (iii) By cross-correlating a given calibration image (dashed blue line) with the N_{sub} calibration subset images, a down-sampled C_m prediction profile across the entire measurement height is created. (iv) A C_m prediction map is created by creating down-sampled C_m profiles for each N_{cal} calibration images in the stack. (b) 3D particle detection scheme. (v) Input image of defocused particle images. (vi) The input image is cross-correlated with the $N_{\rm sub}$ calibration subset images resulting in N_{sub} correlation maps. Candidate particles are detected from the correlation maps from the local peaks larger (red areas) than a certain C_m threshold (shown for $C_m = 0.5$). (vii) For a subject candidate particle (dashed magenta lines), the C_m profile is extracted. (viii) The profile for the subject particle is matched to the C_m profile prediction map to determine its depth position with discrete precision h/N_{cal} . Following, the continuous depth position z_p is determined through a three-point estimator to the three best profile map matches.

GDPTlab [13] requires on average average 6-10 crosscorrelations for each candidate particle to converge to the best match. Moreover, the segmentation procedure must be optimized for each image type and fails if the background or the illumination is not uniform, therefore a pre-processing step is often required.

In this work, we present an improved algorithm to perform GDPT measurements based on the following steps^a:

- Detection step: fast and segmentation-free detection of particles with a robust first estimation of the 3D particle position,
- Refinement step: for each candidate particle, refine the depth position walking through the calibration images stack,

which is an open-source GDPT implementation published under the open-source license and available through [https://defocustracking.com/.](https://defocustracking.com/)

The algorithm constitutes "Method 1" in DefocusTracker,

- Sub-image step: for each candidate particle, determine the z position with "sub-image" resolution using a three-point interpolation scheme,
- Iteration step: iteratively repeat the preceding steps, while shading the images of detected particles, to increase the number of detected particles with overlapping images.

The detection and sub-image steps are the base of the algorithm and provide already a complete measurement. The subsequent steps improve the quality of the measurement but at a larger computational cost. The user can decide which strategy is most suitable for the application. All steps are described in details in the following.

A. Detection step: Segmentation-free particle detection and fast particle position estimation

The detection step is summarized in Fig. 2. To prepare the calibration model, we first select a subset of N_{sub} calibration images from the total N_{cal} images in the calibration stack, see Fig. $2(a)$. For each of the N_{cal} calibration images, we calculate an "expected" C_m profile by performing a normalized cross-correlation with the N_{sub} images in the subset. This gives an a priori expected C_m profile mapping, which are used during the evaluation for a fast identification of the particle z positions. The detection step starts by performing normalized crosscorrelations between the full image and the $N_{\rm sub}$ calibration images in the subset, resulting on a total of N_{sub} correlation maps, see Fig. $2(b)$. The correlation maps have values between 0 and 1, with their peak values located in the center of the particle images with shapes similar to the calibration image used to create the map. The center positions of candidate particles are identified collecting the locations of all peaks in the correlation maps with a value above a certain threshold (typically 0.5). Now, for each given candidate particle, the corresponding C_m profile across the N_{sub} number of z positions is immediately available by reading the values of the N_{sub} correlation maps at that location (Fig. $2(b,vii)$). Each correlation profile can following be compared with the mapping of expected C_m profiles to obtain a robust guess of the z position. This is much faster than comparing 2D calibration images since the C_m profiles are 1D arrays of N_{sub} numbers. With this approach we have three significant advantages:

- 1. Automatic detection: The in-plane and out-ofplane positions of candidate particles are determined by setting a single parameter, namely C_m .
- 2. Fast detection: Only N_{sub} cross-correlations are needed, regardless of the number of particles in the image.
- 3. Versatility: The same procedure can be applied for any type of particle images (fluorescent, brightfield,

with non-uniform illumination, etc.) without any additional steps.

B. Refinement, sub-image, and iteration steps

The preceding detection step provides a complete measurement with the identification of the particles and a robust estimation of their three-dimensional position.

Refinement step. The detection step might not necessarily find the best matching calibration image and a refinement can be needed. All particles identified in the detection step is ordered according to their C_m values, from larger to smaller. Then, a walking procedure is applied to the first particle image to find the best match with the images in the calibration stack, searching in positions close to the z value predicted by the first step. When the refined z position is obtained, the particle image is removed from the image by replacing its area with the intensity values of the background. The same procedure is repeated for the second particle and so forth. At the end of the refinement step, all the detected particles have been removed from the image as illustrated in Fig. $4(a)$.

Sub-image step. The determination of the z position, both after the detection step and the refinement step, is produced with discrete output among the N_{cal} images separated by h/N_{cal} . In order to obtain a continuous output with a "sub-image" resolution, the best matching calibration image must have been detected. Consequently, its neighbouring images are included for match interpolation, similar to what is typically done in digital PIV evaluations to obtain sub-pixel resolution, see Fig. $2(b)$. We use here a three-point parabolic estimator [28].

Iteration step. As shown in Fig. $2(b)$, in the detection step, the cross-correlation already filters out particles based on their image shape, i.e. only particle images similar to the calibration images are detected (highlighted in red). This allows to identify overlapping particles of different shapes. However, when the degree of overlapping between two particle images is too large, the height of the correlation peak decreases significantly and it is no longer possible to identify them. A way to improve the detection in this case is to blank out one of the overlapping particle images $[29, 30]$. This is done in the refinement step with the remaining particles images being those that were not identified in the first step. In order to increase the number of detected particles, the preceding steps are repeated, see Fig. 4.

The above steps improve the accuracy and number of detected particles, however more computation time is consumed, therefore it might not be suitable for realtime applications. The relation between accuracy, number of detected particles, and computational time is investigated in the next section.

FIG. 3. Parametric assessment of the presented algorithm on synthetic images in terms of error in the depth coordinate determination σ_z , the relative number of valid detected particles ϕ , and the processing time, as a function of the number of images in the calibration stack N_{cal} , the number of images in the calibration subset N_{sub} , with or without the refinement step. The assessment is performed on synthetic reference images for three values of the particle image concentration: (a) $N_S = 0.05$, (b) $N_S = 0.30$, and (c) $N_S = 0.59$ [12]. Results performed with the software GDPTlab are reported as reference.

III. PERFORMANCE ASSESSMENT ON SYNTHETIC IMAGES

The presented algorithm allows to automatically detect particle images and determine their 3D position from a suitable calibration image set. Only few parameters must be chosen from the user before starting the evaluation, namely:

- The number of images N_{cal} in the calibration stack.
- The number of images N_{sub} in the calibration subset.
- The threshold value of C_m for identifying candidate particle images.
- Refinement step or no refinement step.
- The number of iterations.

For the purpose of automated and real-time measurements, the most relevant parameters to evaluate are the uncertainty in the depth coordinate determination σ_z , the relative number of valid detected particles ϕ (relative to the total number of particles in the image), and the overall processing time for each image. We do not consider here the uncertainty in the in-plane directions $\sigma_{x,y}$, which are normally one or more orders of magnitude less than σ_z . Measured particles with a z-error larger than 0.1 are considered outliers and not counted as valid detected particles. For a complete description of the assessment of GDPT methods, see Ref. 12.

In order to assess the effect of different parameter settings on the algorithm, we used a standardized dataset of synthetic defocused particle images presented in Ref. 12. The images are created using MicroSIG, a synthetic image generator, based on ray tracing, for defocused and astigmatic particle images [25]. The dataset simulate measurements performed on 2-µm-diameter particles, with $10\times$ magnification over a measurement depth of 86 µm. In particular, we used Dataset II, which contains sets of images of different particle image concentrations^b. . The images are gray scale, 16-bit images with size of 1024×1024 pixels. Following Ref. 12, we define the particle image concentration in terms of source density N_S [31, 32], namely, the number of particles in the image multiplied by the particle image area and divided by the total image area (or, alternatively, particle per pixels times average particle image area).

Three parameter configurations have been investigated as a function of using different number of calibration images N_{cal} : Configuration 1 with $N_{\text{sub}} = 5$ and with refinement step (blue circles), Configuration 2 with $N_{sub} = 3$ and with refinement step (red squares), and Configuration 3 with $N_{sub} = 5$ and no refinement step (yellow diamonds). For all the configurations we used a single iteration step and a similarity threshold value $C_m = 0.5$. The choice of C_m is mostly dictated by the user needs

^b The dataset can be downloaded through <https://defocustracking.com/>

FIG. 4. Performance assessment of the iteration step on synthetic images. (a) Portions of the analyzed images and reconstructed particle positions at each iteration. At the end of each iteration, the detected particle images are deleted, and the following iteration determines a new set of particle positions. (b) Error in the depth coordinate determination σ_z , the relative number of valid detected particles ϕ , and processing time as a function of the image concentration N_S . The analysis was performed using $N_{\text{cal}} = 21$, $N_{\text{sub}} = 3$, and the refinement step, and for one, two, and three iterations. Results performed with the software GDPTlab are reported as reference.

for a given experiment: Larger C_m values yield lower uncertainty at the cost of less detected particles and the other way around. The number of detected particles has also an impact on the computational time, as will be discussed later. Overall, different values of C_m do not play a significant role in the trends observed in the following investigation, therefore we show the results for one single C_m value. For reference, we performed the analysis also with a previous GDPT software, GDPTlab [13]. GDPTlab uses a user-defined segmentation step (based on an intensity threshold) for particle identification and a refinement step as described in Section II B for the z determination.

The results are presented in Fig. 3 for three different particle image concentrations $(N_S = 0.05, 0.30, 0.59)$. In general, a use of N_{cal} larger than 10 is required, however values larger than 20 do not improve the performance significantly. Also, the value of N_{cal} minimally affect the processing time as the z estimation in the detection step is done through simple matching of 1D profiles with N_{sub} points, see Fig. 2(b,viii). The refinement step does not decrease the uncertainty significantly, but it results in a significantly larger processing time, which increases proportionally with the particle image concentration. On the other hand, without the refinement step (Configuration 3), the processing time is basically independent of the particle image concentration. All the three configurations provide approximately the same number of valid detected particles, which is however strongly affected by

the particle image concentration. At $N_S = 0.59$, the relative number of detected particles drops to around 30 %.

It is possible to increase the number of valid detected particles by adding more iterations of the refinement step as shown in Fig. 4. In particular, a second iteration brings this value up to 50 %, whereas a third iteration does not improve it much further as the additionallydetected particles have similarity values below the threshold of $C_m = 0.5$. The cost of more iterations in terms of processing time is however significant.

Finally, in comparison with GDPTlab, the results are similar in terms of uncertainty and detected particles, showing that the segmentation-free approach is in this case as good as a conventional segmentation procedure based on an intensity threshold. However, the current analysis was performed on synthetic images with uniform background and no noise. The advantage of the segmentation-free approach is more evident on experimental images with noise and time-varying background, as shown in the next section. In terms of processing time, GDPTlab is strongly affected by the number of processed particles. Although it is faster at lower concentrations, it slows down rapidly as the number of particle increases, whereas the new algorithm allows a faster processing also for larger concentrations.

FIG. 5. Application to experimental images: Particles inside an evaporating drop. (a) Example raw image showing the defocused images of fluorescent particles inside the region of interest (ROI, green area in sketch inset). The image subset inside the cyan-marked rectangle is shown for two frames at time $t = 0$ s and $t = 210$ s, respectively. For each frame, the detected particles are marked (green shapes) for $C_m > 0.7$ and $C_m > 0.9$. No image pre-processing was used to treat the nonhomogeneous background (due to reflections at the drop interface). (b) Particle image shapes in the calibration images and in the experimental images. (c) Uncertainty assessment and correction of systematic errors through evaluation of the calibration images obtained by taking images of sedimented particles at known depth positions z (illustrated in Panel (b) in Fig. 1). The measured (x', y', z') -positions (blue dots) are used to map the systematic error due to the field curvature (face-colored surface). The uncertainty σ_z/h of the measured depth coordinate z' is accessed through (z, z') shown for the normal (left) and the fast (right) GDPT processing as well as with (blue points) and without (grey points) the correction of the systematic error from the field curvature. (d) Measured (x', y', z') particle trajectories inside the evaporating drop taken at 0.1 fps over a time of 210 s when using the normal (top) and the fast (bottom) GDPT processing.

IV. APPLICATION TO EXPERIMENTAL IMAGES

To demonstrate the algorithm on experimental images, we chose images of tracer particles inside an evaporating droplet. We will not discuss the physics of the problem here or the details of the experimental setup, and for this we refer to Ref. 33. As a quick overview, a 2 mm-diameter droplet of pure water was deposited on a transparent glass slide. The drop was seeded with 1 - μ mdiameter polystyrene spheres that were observed from the bottom using an inverted epi-fluorescent microscope. This example is interesting to test the proposed algorithm, since the image background is not uniform and it changes frame after frame due to reflections from the moving air-water interface (as shown in Fig. $5(a)$). Such images would need a pre-processing step for background removal in order to be processed with a conventional segmentation approach, such the one used in GDPTlab. The current segmentation-free algorithm can be applied on raw images, without any pre-processing step.

The evaluation was performed on 16-bit images, with

size of 1280×1080 pixels. The calibration stack was obtained on sedimented particles that were scanned moving the microscope objective focus with steps of $2 \mu m$ across a depth of 100 μ m ($N_{\text{cal}} = 51$). For the calibration, we chose one particle in the center of the image. We should briefly mention two practical aspects here. First, during the calibration, the objective lens moves in air and the particles are fixed, whereas during the measurement the objective lens is fixed and the particles moves in water. Although this has a minimal effect on the shape of the particle images, as shown in Fig. $5(b)$, in order to obtain the same defocusing effect, the distance that a particle must travel in water is different from the distance that the objective lens has travelled in air. In this case, this difference is well-approximated by a pre-factor equal to the refractive index of water 1.33 $[34]$. Second, in experimental images the defocusing patterns might change across the image sensor due to distortions, perspective errors, or other aberrations. These are systematic errors that can in most case be corrected, more information are given in Ref. 12.

To correct for bias errors in the case at hand, we eval-

uated the positions of all the particles in the calibration images, which are particles lying on a flat surface and stuck to fixed in-plane positions. As shown in Fig. $5(c)$, particles across the entire sensor could be measured, perspective or distortion errors are negligible $(0.2 pixels),$ and the only relevant source of error is given by the curvature of the focal plane which is not perfectly flat (shown by the curved mesh in the figure).

We can use these data also to assess the measurement uncertainty. In particular, we used two settings of the presented algorithm: $N_{\text{sub}} = 7$, with refinement step (normal), and $N_{\text{sub}} = 5$, without refinement step (fast). In Fig. $5(c)$, we show the measured versus true z positions for the two settings, the blue dots are the data after bias correction. Larger errors are observed in the top part of the calibration, where the images are dimmer and more blurred. Overall, the uncertainty difference between the two settings is small, and is about 2 % for the normal setting and 3 % for the fast setting (standard deviation of the error normalized on the total measurement depth [12]).

Finally, we show the results of the droplet measurement. The images were acquired at 0.1 frames per second and processed with the two settings described above (normal and fast). The processing time per frame was 3 and 8 s, respectively, using a laptop computer with an Intel Core i7-7600U CPU processor running at 2.80 GHz with a RAM memory of 16 GB. The particle trajectories and velocities where obtained using a simple nearest neighbor approach. No image pre-processing was used, and, as shown in Fig. $5(a)$, the detection process worked properly independently of the background intensity fluctuations. The number of particles that are detected is determined by a threshold on their C_m value: A lower threshold catches more particles but increase also the measurement error and the presence of outliers.

The final particle trajectories using the two settings are reported in Fig. 5(d), and correspond to a measurement volume of about $1600 \times 1300 \times 133 \mu m^{3c}$. Particles on the bulk of the fluid move downwards toward the contact line, whereas particles at the interface move upward due to a thermally-induced Marangoni flow. Although the normal setting catches more tracks than the fast setting, the overall structures of the flow are well captured also by the fast setting. On the other hand, in case of realtime measurement, the fast setting allows a three times faster temporal resolution.

V. SIMULATION OF A REAL-TIME MICROFLUIDIC EXPERIMENT

In this section we set up a simulation framework to test

the performance of the presented algorithm on a real-time application. We use simulations since we need to have access to the true particle positions to assess the algorithm performance. As a real-time application, we chose particle focusing in acoustofluidic devices, which is receiving a growing interest in biomedical applications [35].

Simulation of acoustofluidic focusing. We set up a simulation of a typical acoustofluidic experiment for separation or focusing of particles or cells [36, 37], see Fig. $6(a)$. The simulation consists of 5-µm-diameter polystyrene particles suspended in water in a microchannel of rectangular cross-section (width $w = 200 \text{ \mu m}$, height $h = 100 \text{ }\mu\text{m}$. The particle suspension is transported through the microchannel by an externally-driven flow and the resulting stream-wise particle velocities $u_x^{\text{flow}}(y, z)$ are calculated from the analytical solution of a Poiseuille flow in a rectangular channel with flow rate $Q = 3 \mu l/h$ [38]. The microchannel is acoustically actuated by an attached piezo-electric transducer to induce a vertical half-wave standing acoustic waves of frequency $f_z = c_{wa}/(2h) = 7.49$ MHz across the channel height. The acoustic actuation leads to acoustic radiation forces on the suspended particles [39] (we neglect any effects from acoustic streaming and particle-particle/particlewall interactions $[40]$ and through balance of the viscous drag force and the acoustic radiation force, we can calculate analytically the cross-sectional acoustophoretic particle velocities as

$$
u_z^{\rm rad}(z) = \frac{2\pi}{3} \frac{a^2}{h} \frac{\Phi}{\eta} E_{\rm ac} \sin\left[2\pi \left(\frac{z}{h} + \frac{1}{2}\right)\right],\qquad(1)
$$

where η is the fluid viscosity, Φ the acoustic contrast between particle and suspending fluid, and E_{ac} is the acoustic energy density. We used an acoustic energy density $E_{\text{ac}} = 0.3 \text{ J/m}^3$, which is a low but realistic value corresponding to maximum acoustic particle velocities of approximately 8 μ m/s [26, 41]. Before the onset of the experiment, the particles are randomly distributed inside the channel and the resulting cross-sectional particle positions over a time of 8 seconds are shown in Fig. $6(c)$.

Generation of synthetic images. The acoustofluidic simulations were used to create synthetic images of the particles using MicroSIG [25]. The main setting for the synthetic images were a $10\times/0.3$ objective lens plus astigmatic aberration on a 512×512 pixels sensor (pixel) size of 6.5 μ m, 16 bit). Gaussian noise was added to the images resulting in signal-to-noise ratio SNR for individual particle images ranging from 30 to 240. A typical synthetic image is shown in Fig. $7(a)$, which corresponds to a classical darkfield image used in micro-PIV setups (i.e. fluorescent particles observed with an epi-fluorescent microscope). Additionally, we used two other types of images: Brightfield images obtained by inverting the values of the darkfield images (Fig. 7(b)) and brightfield images with an added intensity disturbance, introduced to simulate non-uniform backgrounds or non-uniform illumination (Fig. $7(c)$). The disturbance consists of a 2D sinusoidal pattern.

 \degree Note that in Ref. 33 a deeper and finer calibration stack was used, yielding a measurement volume of $1400 \times 1300 \times 150 \text{ }\mu\text{m}^3$ and depth uncertainty of $1 \mu m$.

FIG. 6. (a) Schematic of the acoustofluidic experiment object of the simulations: an acoustofluidic device is used to focus particles in the center height of a rectangular microchannel. Real-time GDPT measurements are used to monitor the position of the particles inside the channel and to identify the time $t_{h/3}$, when 90 % of the particles are inside a vertical region of thickness $h/3$ (indicated by red horizontal lines in (c)). (b) Illustration of the percentage of particles that has reached the $h/3$ vertical region as a function of time. The points indicate the real number of particles inside the region, the spacing in the time axes is determined by the frame rate of the acquisition. The circles indicate the number particle inside the region as measured by GDPT, the spacing in the time axis is determined by the computation time. (c) Cross-sectional view of the simulated particle position in the measurement region for different time instants when assuming a Poiseuille flow with flow rate $Q = 3$ μ l/h and acoustic energy density $E_{\text{ac}} = 0.3 \text{ J/m}^3$.

Simulation of real-time experiment. An ad hoc Matlab routine was written to simulate real-time GDPT measurements with a camera frame rate of 25 fps in a section of the microchannel as illustrated in Fig. $6(a)$. The objective of the simulation is to identify the "trigger" time $t_{h/3}$ for which 90 % of the particles have been focused in a vertical center region of thickness $h/3$ (marked with red horizontal lines in Fig. $6(c)$). There are mainly three parameters to consider for the assessment of realtime GDPT measurements: (1) the computational time of a single evaluation, (2) the accuracy of the measurement, and (3) the number of detected particles (this strongly depends on the particle concentration, since it is more difficult to process overlapping particles, see Section III). Improving points (2) and (3) leads to longer computational times therefore a trade-off must be found. The computational time sets also the temporal resolution of the real-time measurement, therefore a random delay time proportional to the temporal resolution is expected. This is shown in Fig. $6(b)$, where the percentage of particles that has reached the $h/3$ vertical region is plotted as a function of time. The points indicate the real number of particles inside the region and the red vertical line indicates the real "trigger time" $t_{h/3}$. The circles show the corresponding GDPT measurements, which have lower

temporal resolution due to the computational time of each frame. The blue vertical line marks the corresponding GDPT "trigger time" $t'_{h/3}$. In the hypothetical case of perfect GDPT measurements, the delay time $t'_{h/3} - t_{h/3}$ is between one and two times the temporal resolution. However, due to the GDPT measurement uncertainty, a smaller or larger delay time can occur. As an example, if the delay time is negative, GDPT detects that 90 % of the particles have reached the region before they actual have.

Results of real-time GDPT measurement. In a first set of experiments, we tested the performance of real-time GDPT measurements on the fluorescent images. As discussed in Section III, we test different strategies to decrease the computational time, namely by reducing the total number of images in the calibration stack N_{cal} , by reducing the number N_{sub} of images in the subset of the calibration stack, and by removing the refinement step. In particular, see Fig. $8(a)$, we calculated the detection delay time $t_{h/3} - t'_{h/3}$ as a function of the average computational time for each image. The grey area indicates the expected results in the case of having no uncertainty in the GDPT measurements. The simulations show that removing the refinement step speeds up signifi-

FIG. 7. The presented algorithm can be applied to different types of images without any additional processing steps, which are here shown by synthetic images generated with MicroSIG. The images are synthetic images of 5-µm particles taken with a $10 \times / 0.3$ objective lens and the use of astigmatic aberration. (a) Fluorescent image. (b) Bright-field image. (c) Bright-field image disturbed with a sinusoidal intensity pattern simulating a non-homogeneous background or illumination.

cantly the computational time with relatively low impact on the accuracy. On the other hand, decreasing the number of images in the calibration stack minimally decrease the computational time but can cause a failure of the measurement. The corresponding average percentage of the number of detected particles is shown in Fig. 8(b).

In a second set of experiments, we tested the performance of the presented algorithm when applied to different types of images: fluorescent, brightfield, and brightfield with disturbance, see Fig. 7. This time we always used $N_{\text{cal}} = 51$ images in the calibration stack. The results of the simulations are presented in Fig. $8(c-d)$ and show that no significant difference is observed when the refinement step is used, proving that the presented approach is suitable for different image types but that in most challenging situation the refinement step is needed.

The simulations were performed on 512×512 -sized, 16bit images on a laptop computer with an Intel Core i7- 7600U CPU processor running at 2.80 GHz with a RAM memory of 16 GB. With this setup it was possible to achieve an evaluation time of about one second.

VI. CONCLUSIONS

We have presented a new algorithm for performing 3D particle tracking using GDPT that does not need preliminary pre-processing or segmentation steps. The presented algorithm needs to compute only few

- [1] Gao D, Jin F, Zhou M, Jiang Y. Recent advances in single cell manipulation and biochemical analysis on microfluidics. Analyst. 2019;144(3):766–781.
- [2] Santiago JG, Wereley ST, Meinhart CD, Beebe DJ, Adrian RJ. A particle image velocimetry system for microfluidics. Experiments in fluids. 1998;25(4):316–319.
- [3] Willert C, Gharib M. Three-dimensional particle imaging with a single camera. Experiments in Fluids. 1992;12(6):353–358.

cross-correlations in comparison with other iterative approaches and is therefore suitable for a fast evaluation time. In addition, the algorithm allows for the detection of overlapping particles. The performance of the algorithm, in terms of uncertainty in the depth determination, detection of valid particles, and processing time, was tested on synthetic and experimental images. The algorithm was tested for real-time application by setting up a framework for real-time simulation of an acoustophoretic experiment, created using synthetic images and an ad hoc Matlab routine. The real-time simulations show, that even without using the refinement step, the presented algorithm is able to perform automated control-tasks and that work robustly on different types of images (darkfield or brightfield) also with fluctuations of the background intensity. The presented algorithm and simulation framework set the base for use of GDPT in real-time applications as well as for the further development and improvement hereof.

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- [4] Pereira F, Gharib M, Dabiri D, Modarress D. Defocusing digital particle image velocimetry: a 3-component 3 dimensional DPIV measurement technique. Application to bubbly flows. Experiments in Fluids. 2000;29(1):S078– S084.
- [5] Cierpka C, Segura R, Hain R, Kähler CJ. A simple single camera 3C3D velocity measurement technique without errors due to depth of correlation and spatial averaging for microfluidics. Measurement Science and Technology.

FIG. 8. Simulation of a real-time application of GDPT on a microparticle acoustophoresis experiment as shown in Fig. 6. The results are shown for different algorithm settings and for (a-b) using different number of images in the calibration stack N_{cal} and (c-d) for different types of images with $N_{\text{cal}} = 51$. (a,c) Measured detection delay time $t_{h/3} - t'_{h/3}$ as a function of the mean evaluation time where the grey area represents the random delay expected for the given evaluation time. (b,d) Average percentage of detected number of particles as a function of time.

2010;21(4):045401.

- [6] Cierpka C, Rossi M, Segura R, K¨ahler C. On the calibration of astigmatism particle tracking velocimetry for microflows. Measurement Science and Technology. 2011;22(1):015401.
- [7] Zettner C, Yoda M. Particle velocity field measurements in a near-wall flow using evanescent wave illumination. Experiments in fluids. 2003;34(1):115–121.
- [8] Hinsch KD. Holographic particle image velocimetry. Measurement Science and Technology. 2002;13(7):R61.
- [9] Kim H, Westerweel J, Elsinga GE. Comparison of Tomo-PIV and 3D-PTV for microfluidic flows. Measurement Science and Technology. 2012;24(2):024007.
- [10] Cierpka C, Kähler CJ. Particle imaging techniques for volumetric three-component (3D3C) velocity measurements in microfluidics. Journal of Visualization. $2012;15(1):1-31.$
- [11] Barnkob R, Kähler CJ, Rossi M. General defocusing particle tracking. Lab on a Chip. 2015;15(17):3556–3560.
- [12] Barnkob R, Rossi M. General defocusing particle tracking: fundamentals and uncertainty assessment. Experiments in Fluids. 2020;61:1–14.
- $[13]$ [GDTPlab how to get it,](https://www.unibw.de/lrt7/gdpt-1/gdptlab-how_to_get_it) Institut für Strömungsmechanik und Aerodynamik, Univeristät der Bundeswher, Werner Heisenberg Weg 39, 85577 Neubiberg, Germany;. Accessed: 3 June 2020. [https://www.unibw.](https://www.unibw.de/lrt7/gdpt-1/gdptlab-how_to_get_it) [de/lrt7/gdpt-1/gdptlab-how_to_get_it](https://www.unibw.de/lrt7/gdpt-1/gdptlab-how_to_get_it).
- [14] Taute K, Gude S, Tans S, Shimizu T. High-throughput 3D tracking of bacteria on a standard phase contrast microscope. Nature communications. 2015;6:8776.
- [15] Liu J, Reisbeck M, Hayden O. Investigation of mechanical and magnetophoretic focusing for magnetic flow cytometry. Current Directions in Biomedical Engineering. 2019;5(1):353–355.
- [16] Boyko E, Eshel R, Gat AD, Bercovici M. Nonuniform Electro-osmotic Flow Drives Fluid-Structure Instability. Physical Review Letters. 2020;124(2):024501.
- [17] Barnkob R, Nama N, Ren L, Huang TJ, Costanzo F, Kähler CJ. Acoustically driven fluid and particle motion in confined and leaky systems. Physical Review Applied. 2018;9(1):014027.
- [18] Karlsen JT, Qiu W, Augustsson P, Bruus H. Acoustic streaming and its suppression in inhomogeneous fluids. Physical review letters. 2018;120(5):054501.
- [19] Volk A, Kähler CJ. Size control of sessile microbubbles for reproducibly driven acoustic streaming. Physical Review Applied. 2018;9(5):054015.
- [20] Qiu W, Karlsen JT, Bruus H, Augustsson P. Experimental Characterization of Acoustic Streaming in Gradients of Density and Compressibility. Physical Review Applied. 2019;11(2):024018.
- [21] Van Assche D, Reithuber E, Qiu W, Laurell T, Henriques-Normark B, Mellroth P, et al. Gradient acoustic focusing of sub-micron particles for separation of bacteria from blood lysate. Scientific reports. 2020;10(1):1– 13.
- [22] Bodé WN, Jiang L, Laurell T, Bruus H. Microparticle Acoustophoresis in Aluminum-Based Acoustofluidic Devices with PDMS Covers. Micromachines. 2020;11(3):292.
- [23] Shaglwf Z, Hammarström B, Shona Laila D, Hill M, Glynne-Jones P. Acoustofluidic particle steering. The Journal of the Acoustical Society of America. 2019;145(2):945–955.
- [24] Nguyen T, Fu Y, Tran V, Gautam A, Pudasaini S, Du H. Acoustofluidic closed-loop control of microparticles and cells using standing surface acoustic waves. Sensors and Actuators B: Chemical. 2020:128143.
- [25] Rossi M. Synthetic image generator for defocusing and astigmatic PIV/PTV. Measurement Science and Technology. 2020;31(1):017003.
- [26] Muller PB, Rossi M, Marin A, Barnkob R, Augustsson P, Laurell T, et al. Ultrasound-induced acoustophoretic motion of microparticles in three dimensions. Physical Review E. 2013;88(2):023006.
- [27] Lewis JP. Fast template matching. In: Vision interface. vol. 95; 1995. p. 15–19.
- [28] Raffel M, Willert CE, Scarano F, Kähler CJ, Wereley ST, Kompenhans J. Tracer Particles. In: Particle Image Velocimetry. 3rd ed. Springer; 2018. p. 39.
- [29] Wieneke B. Iterative reconstruction of volumetric particle distribution. Measurement Science and Technology. 2012;24(2):024008.
- [30] Liberzon A, Gurka R, Hetsroni G. XPIV–Multi-plane stereoscopic particle image velocimetry. Experiments in fluids. 2004;36(2):355–362.
- [31] Adrian RJ. Scattering particle characteristics and their effect on pulsed laser measurements of fluid flow: speckle velocimetry vs particle image velocimetry. Applied optics. 1984;23(11):1690–1691.
- [32] Westerweel J. Theoretical analysis of the measurement precision in particle image velocimetry. Experiments in

Fluids. 2000;29(1):S003–S012.

- [33] Rossi M, Marin A, Kähler CJ. Interfacial flows in sessile evaporating droplets of mineral water. Physical Review E. 2019;100(3):033103.
- [34] Rossi M, Segura R, Cierpka C, Kähler CJ. On the effect of particle image intensity and image preprocessing on the depth of correlation in micro-PIV. Experiments in fluids. 2012;52(4):1063–1075.
- [35] Antfolk M, Laurell T. Acoustofluidic Blood Component Sample Preparation and Processing in Medical Applications. In: Applications of Microfluidic Systems in Biology and Medicine. Springer; 2019. p. 1–25.
- [36] Lenshof A, Magnusson C, Laurell T. Acoustofluidics 8: Applications of acoustophoresis in continuous flow microsystems. Lab on a Chip. 2012;12(7):1210–1223.
- [37] Adams JD, Ebbesen CL, Barnkob R, Yang AH, Soh HT, Bruus H. High-throughput, temperature-controlled microchannel acoustophoresis device made with rapid prototyping. Journal of Micromechanics and Microengineering. 2012;22(7):075017.
- [38] Bruus H. Theoretical microfluidics. vol. 18. Oxford university press Oxford; 2008.
- [39] Karlsen JT, Bruus H. Forces acting on a small particle in an acoustical field in a thermoviscous fluid. Physical Review E. 2015;92(4):043010.
- [40] Barnkob R, Augustsson P, Laurell T, Bruus H. Acoustic radiation-and streaming-induced microparticle velocities determined by microparticle image velocimetry in an ultrasound symmetry plane. Physical Review E. 2012;86(5):056307.
- [41] Barnkob R, Augustsson P, Laurell T, Bruus H. Measuring the local pressure amplitude in microchannel acoustophoresis. Lab on a Chip. 2010;10(5):563–570.