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# Cooperativity and fragility in furan-based polyesters with different glycolic subunits as compared to their terephthalic counterparts

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#### Abstract

This works aims to investigate the effect of the molecular groups found in polyester backbones (type of ring in the acidic subunit and length of the glycolic subunit) on the molecular dynamics. The investigation is done on three furan-based polyesters (PEF, PPF and PBF) as compared to their terephthalic counterparts (PET, PTT, and PBT) after full quenching from the molten state. The segmental molecular dynamics is investigated with MT-DSC, FSC and DRS. It is shown that the cooperativity decreases as the length of the glycolic subunit increases in both furan-based and terephthalic polyesters. No direct correlation between the fragility index and the cooperativity is observed in furan-based polyesters containing glycolic subunits of different lengths. The differences in the isochoric fragilities obtained for the furan-based polyesters and their terephthalic counterparts has been assumed to result from the combination of backbone flexibility and packing efficiency of the macromolecular chains

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in the amorphous phase.

Keywords: molecular mobility, bio-based polyesters, dielectric relaxation spectroscopy, fast scanning calorimetry, backbone flexibility, packing efficiency

## 1. Introduction

New polymers are constantly being synthesized from sustainable resources to replace fossil-based materials. Currently, one of the most promising biosourced chemicals is furandicarboxylic acid (FDCA), which can be produced from vegetable feedstock and used to synthesize polyesters through the combination with different diols, allowing to obtain repeating units with glycolic subunits of different lengths. For example, poly(ethylene furandicarboxylate) (PEF) is obtained by combining FDCA with ethylene glycol, poly(propylene furandicarboxylate) (PPF) is obtained by combining FDCA with 1,3-propanediol, poly(butylene furandicarboxylate) (PBF) is obtained by combining FDCA with 1,4-butanediol [1], and so on. It is worth noting that FDCA exists in the form of three position isomers [2], but the most commonly used is 2,5-FDCA. Among all the mentioned furan-based polyesters, 2,5-PEF is the most studied due to some interesting mechanical and barrier properties, which makes it the best potential bio-based surrogate to poly(ethylene terephthalate) (PET) for packaging [3]. 2,5-PPF is also an interesting polymer with excellent gas barrier properties [4], which makes it a promising substitute for its petroleum-based homologues poly(trimethylene terephthalate) (PTT) and poly(trimethylene naphthalate) (PTN) in packaging applications. Another polymer belonging to the family of furan-based polyesters and worth investigating is 2,5-PBF. This polymer has good thermal, mechanical and barrier properties [5], and could therefore be suitable for food-packaging applications in replacement of its terephthalic counterpart. But before making decisions on whether a polymer can be substituted by another polymer, it is of uppermost importance to have an idea of the potential properties of these promising materials, both in the amorphous state and in the presence of semi-crystalline structures. The literature reports that the presence of a rigid amorphous fraction has a strong effect on the mechanical and barrier properties of semi-crystalline polymers [6, 7, 8, 9, 10], but polymer microstructures can be quite complex [10], and before investigating semi-crystalline samples it may be worth evaluating the molecular mobility of the fully amorphous samples. Investigations of the molecular mobility in amorphous biobased 2,5-PEF and 2,4-PEF as compared to poly(lactic acid) (PLA) and PET, for instance, allowed making a correlation between the glass-forming behaviour of 2,5-PEF and its particularly high value of the dielectric strength with the dipolar moment, the packing efficiency of the macromolecular chains, and therefore the free volume and the barrier properties [11]. Similar investigations performed on a series of amorphous biobased copolyesters obtained with both 2,5- and 2,4-FDCA showed that position isomerism affects the glass transition temperature and the relaxation times associated with the  $\beta$  relaxation processes, but has no obvious effects neither on the fragility index, nor on the cooperativity [12]. Guidotti et al. [13] recently synthesized and characterized a series of four homopolyesters of 2,5-FDCA with glycols of different lengths (i.e. with a number of methylene groups in the glycolic subunit going from 3 to 6). They concluded that the length of the glycolic subunit is a key parameter in determining the kind and fraction of ordered phases developed by the samples during compression molding followed by cooling. They evidenced the formation of a less-ordered (oneor two-dimensional) phase (they called it "mesophase") that, together with the amorphous and the eventually present crystalline phase, significantly impacted the mechanical and barrier properties. Soccio et al. [14] investigated the molecular dynamics of these four poly(alkylene 2,5-furanoate)s and unveiled complex local relaxations (characterized by the simultaneous presence of two components depending on the thermal treatment), plus a segmental relaxation whose relaxation time and strength depended on the glycolic subunit length. In another work, Martínez-Tong et al. [15] reported on the molecular origin of some peculiar physical properties of poly(pentamentylene 2,5-furanoate), observing that the molecular dynamics in polymers can be sensitive to thermal history over a broad temperature range even in the noncrystallized state, due to a possible modulation of the interchain interactions. This further stresses the relevance of investigating polymers in their fully amorphous state prior to evaluate the effect of crystallization. Genovese et al. [16] had previously investigated the effects of chemistry (nature and structure of the ring in the acidic subunits) on the relaxation dynamics of three polyesters, comparing the furan, the terephthalic and the cyclohexane rings, but only focused on the subglass secondary relaxation modes. The advantage of comparing polyesters with different rings is that the corresponding polymer backbones have different flexibilities and can be either aromatic or fully aliphatic. They evidenced a multimodal nature of the subglass  $T_{beta}$  process, detecting three modes for the more flexible polyester (with cyclohexane rings) but just a single mode for the stiffer polyester (with furan rings).

The molecular mobility of polymers in the temperature range corresponding to their glass transition can be described using the approach proposed by Adam and Gibbs [17]. In this approach, the segmental relaxation processes are occurring in so-called Cooperative Rearranging Regions (CRRs). A CRR is defined as the smallest subsystem in which the α-relaxation process can occur independently of the neighboring subsystems; each CRR is characterized by its own relaxation dynamics and thermodynamic variables. An experimental method has been proposed by Donth [18, 19] to estimate the average size of a CRR from calorimetric measurements using equation 1.

$$\xi_{T\alpha}^3 = \frac{1/(C_p)_{solid} - 1/(C_p)_{liquid}}{\rho(\delta T)^2} k_B(T_\alpha)^2 \tag{1}$$

Where  $C_p$  is the isobaric heat capacity,  $k_B$  is the Boltzmann constant,  $\rho$  is the polymer density,  $\delta T_g$  is the average temperature fluctuation within a CRR and  $T_{\alpha}$  is the dynamic glass transition temperature. Donth's approach allows to estimate the average CRR size at the glass transition temperature exclusively from calorimetric experiments. Previous studies led to the development of a method to determine the average CRR size on a wider frequency range, providing access to a more complete spectrum of the structural relaxation. The method proposed by Saiter et al. [20] combines Dielectric Relaxation Spectroscopy (DRS)

and Modulated-Temperature Differential Scanning Calorimetry (MT-DSC) to estimate the CRR size over an extended temperature and frequency range, from the cross-over region through the glass transition.

Cooperativity has been proven to depend not only on temperature, but also on structural constraints such as confinement effects [21, 22, 23, 24]. Numerous studies have also shown that the cooperativity length  $\xi_{\alpha}$  can be highly affected by changes in the intermolecular interactions, e.g. in the presence of a plasticizer or when the polymer backbone bears side chains having different lengths, or simply due to different macromolecular arrangements [25, 26, 27, 28]. Nakanishi et al. [29] proposed a simplified model of hydrogen-bond network based on polyhydric alcohols, and used the Adam and Gibbs' approach to show that the average CRR size increases when the intermolecular interactions increase. Some attempts have also been made to correlate a change in the CRR size with the evolution of the relaxation times. Hong et al. [30] investigated a wide range of glass-forming liquids including polymers, but observed no evident correlation between the cooperativity length and the fragility index. They explained this discrepancy by splitting the fragility index into two contributions, one measured in isochoric conditions  $m_v$  and one only due to volume changes  $(m-m_v)$ . Under this assumption, the fragility m can be expressed using equation 2:

$$m = (m - m_v) + m_v = \frac{\Delta V^{\#}}{\ln(10)k_B} \frac{\alpha_{\tau}}{\kappa} + m_v$$
 (2)

Where  $\alpha_T$  is the thermal expansion coefficient of the supercooled liquid at the glass transition temperature,  $\kappa$  is the compressibility, and  $\Delta V^{\#}$  is approximately equal to 4% of the cooperativity volume. For a wide range of glass-forming liquids including polymers,  $\alpha_T/\kappa$  is comprised between 0.5 and 3  $MPaK^-1$  [30]. According to the literature, only the parameter  $(m-m_v)$  should be straightly correlated to the cooperativity at the glass transition [30, 28]. As a consequence, fragility and cooperativity are expected to be correlated only when the isochoric fragility  $m_v$  remains constant.

Recently, Araujo et al. [31] proposed a structural interpretation of the two contributions governing the fragility in polymer systems. According to their

results,  $(m-m_v)$  depends on the inter-chain interactions, whereas the isochoric fragility  $m_v$  mainly depends on the backbone stiffness. It is therefore likely that any change in the inter-chain interactions induced by structural changes that do not affect the backbone stiffness also lead to a concomitant evolution of fragility and cooperativity. A more recent study from Araujo et al. [25] on plasticized PLA showed that a change of inter-chain interactions induced by the incorporation of a plasticizer results indeed in a correlated evolution of cooperativity and dynamic fragility.

This works aims to investigate the effect of the molecular groups found in polyester backbones (type of ring in the acidic subunit and length of the glycolic subunit) on the molecular dynamics of three furan-based polyesters (2,5-PEF, 2,5-PPF, and 2,5-PBF, simply referred to as PEF, PPF and PBF in the following) as compared to their terephthalic counterparts (PET, PTT, and PBT) after full quenching from the molten state. The segmental molecular dynamics have been investigated through the concept of cooperativity as defined by Adam and Gibbs [17]. Cooperativity has been estimated using MT-DSC according to Donth's model [18, 19]. The approach proposed by Hong et al. [30] has been used to determine the two fragility contributions and then estimate any possible correlation between cooperativity and fragility. The discussion has been focused on the values of isochoric fragility  $m_v$  to get a better understanding of the parameters potentially affecting the properties of the investigated polymers.

# 2. Materials and Methods

# 2.1. Materials

Poly(ethylene 2,5-furandicarboxylate) (PEF), poly(butylene 2,5-furandicarboxylate) (PBF) and poly(trimethylene terephthalate) (PTT) were synthesized in the Food and Biobased Research (FBR) laboratories located in Wageningen, the Netherlands, according to procedures previously reported in the literature [32, 1, 33, 34]. Poly(propylene 2,5-furandicarboxylate) (PPF) was synthesized in

the Department of Civil, Chemical, Environmental and Materials Engineering (DICAM), University of Bologna, Italy, according to the procedure reported in [35]. Poly (ethylene terephthalate) (PET) and poly(butylene terephthalate) (PBT) are industrial grades and were purchased. Prior to measurement, all the samples were stored in a desiccator with  $P_2O_5$  for at least 24h. The samples are listed in Table 1.

#### 2.2. Modulated-Temperature Differential Scanning Calorimetry (MT-DSC)

MT-DSC experiments were performed on a Q100 (TA Instruments) using the Tzero Technology. Prior to measurement, energy, temperature and heat capacity calibrations were carried out using indium and sapphire standards. Every experiment was achieved under a constant nitrogen flow of  $50~mL~min^{-1}$  to avoid oxidative degradation of the samples. The samples were first melted within their MT-DSC pan using a hot plate at a temperature above their melting temperature, and then quenched on a cold plate to obtain fully amorphous samples. After quenching, a heat-only protocol starting from -70°C to a temperature above the melting temperature was applied to each sample. According to [36], the measurements were performed with a heating rate of  $2K~min^{-1}$ , a modulation amplitude of  $\pm 0.318K$  and a period of 60s.

## 2.3. Fast Scanning Calorimetry

FSC experiments were carried out using a Flash-DSC1 calorimeter (Mettler-Toledo) equipped with a HUBER TC100 intracooler. Prior to measurement, each MultiSTAR UFS1 MEMS empty chip was conditioned and corrected according to the manufacturer recommendations. During the analysis, a constant nitrogen flow of 200 mL  $min^{-1}$  was used to prevent any oxidative degradation of the samples. The dynamic thermal lag depends on the selected heating (and cooling) rate [37]; in this work it was measured at  $\beta^h = |\beta^c| = 1000K$  s<sup>-1</sup>. The static thermal lag  $\Delta T_S$  depends on the sample thickness and was calculated as a third of the distance between the melting temperatures of two indium pieces, one placed on the reference sensor and the other placed on top of the sample

[37]. To prevent thermal gradients and ensure small values of static thermal lag, all the samples were prepared with a thickness not exceeding  $10 \pm 3\mu m$  as recommended by Toda et al. [38], and placed in the middle of the sensor as advised by Jariyavidyanont et al. [39]. The sample masses ranged between 14 ng (PEF) and 38 ng (PBF) and were measured by using equation 3:

$$m = \frac{(\Delta C_p)_{am}^{FSC}}{(\Delta C_p)_{am}^{MT-DSC}}$$
(3)

Where  $(\Delta C_p)_{am}^{FSC}$  is the heat capacity step at the glass transition estimated by FSC ( $\beta^h = 1000K \ s^{-1}$ ) and  $(\Delta C_p)_{am}^{MT-DSC}$  is the heat capacity step at the glass transition measured by MT-DSC ( $\beta^h = 2K \ min^{-1} \approx 0.033K \ s^{-1}$ ) on the sample in its reference amorphous state.

## 2.4. Dielectric Relaxation Spectroscopy (DRS)

DRS experiments were performed using interdigitated electrodes (BDS 1410-20-150) from Novocontrol Technologies GmbH (accuracy in  $\tan \delta \approx 0.001$ , sensor diameter 20 mm and combs-gold plated copper). The combs fingers are 150  $\mu m$  in width and 35  $\mu m$  in thickness and are spaced by 150  $\mu m$ . Prior to sample deposition, the electrodes were calibrated by determining their respective geometric (empty) capacity ( $C_0$ ) and substrate capacity ( $C_{SU}$ ) through measurements of a reference material of known permittivity (hydroxy-terminated PPMS, Sigma Aldrich). After the sample deposition, the electrodes were heated on a hot plate to melt the polymer samples before quenching them on a cold plate. The measurements were then carried out in a frequency range of  $10^{-1}$ – $10^6$  Hz by an Alpha-A analyzer (Novocontrol Technologies GmbH). A Quatro Cryosystem (Novocontrol Technologies GmbH) was used to control the temperature with a stability of  $\pm 0.5$ °C. The temperature was increased from -150°C to 150°C using appropriate steps. The Havriliak-Negami (HN) complex function was used to analyze the dielectric relaxation curves:

$$\varepsilon^*(\omega) = \varepsilon_{\infty} + \frac{\Delta \varepsilon_{HN}}{[1 + (i\omega \tau_{HN})^{\alpha_{HN}}]^{\beta_{HN}}}$$
(4)

Equation 4 allows to fit the real and imaginary components (respectively  $\varepsilon'(\omega)$ ) and  $\varepsilon''(\omega)$ ) of the complex dielectric permittivity ( $\varepsilon^*(\omega)$ ). From the fitting results it is possible to estimate the relaxation strength  $\Delta \varepsilon_{HN}$ , the relaxation time  $\tau_{HN}$ , and the symmetric and asymmetric broadening factors  $\alpha_{HN}$  and  $\beta_{HN}$  of the  $\alpha$  and  $\beta$  relaxation processes [40, 41].

#### 3. Results and Discussion

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Figure 1 shows the Reversing Heat Capacity signals obtained from MT-DSC measurements at a heating rate of  $2K \ min^{-1}$  on the fully amorphous samples, except for the PBT sample for which quenching was not successful. With this only exception, all the samples showed a clear glass transition step followed by a cold crystallization peak, and a melting peak corresponding to the crystalline phase formed during the heating ramp. The enthalpies of crystallization and melting were systematically compared to confirm that the samples were fully amorphous in their initial state, i.e. right after quenching, at the beginning of the heating ramp. Table 2 reports the thermal parameters extracted from

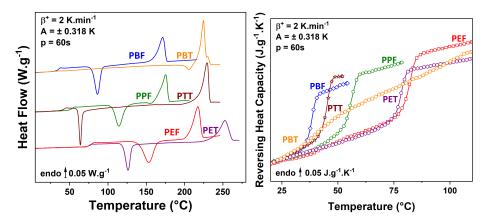


Figure 1: Heat Flow and Reversing Heat Capacity signals measured on the quenched (fully amorphous) samples using a heat-only MT-DSC protocol. Quenching was not successful for the PBT sample.

Figure 1. According to the literature [42, 43, 44, 45], at least two crystalline phases can be observed in furan-based polyesters. The  $\alpha'$  crystals formed at low

temperatures are imperfect, and therefore prone to melt-recrystallization processes during heating; the  $\alpha$  crystals formed at higher temperatures are more perfect [43]. For all samples, the cold crystallization temperature corresponds to the temperature at which the less perfect  $\alpha'$  crystals are formed, whereas the melting temperature is associated with the melting of the more perfect  $\alpha$ crystals. This means that, when the initially amorphous samples are heated up, they crystallize into  $\alpha'$  crystals and then reorganize into  $\alpha$  crystals. At low scanning rates, the crystalline reorganization processes are possible and the measured enthalpies of melting are consequently affected by significant uncertainties. Table 2 shows that for both furan-based and terephthalic polyesters, an increase in the length of the glycolic subunit produces a decrease in the glass transition temperature, as well as a decrease in both the cold crystallization and melting temperatures. The literature reports that a decrease is observed in the characteristic temperatures when the length of the glycolic subunit increases, and that this phenomenon should be attributed to an increased flexibility of the polymer chains [46, 47]. The increased chain flexibility would also explain the width reduction of the cold crystallization peak. The width of a crystallization peak generally indicates how fast the crystallization process occurs; this work suggests that an increased length of the glycolic subunit produces an increase in the crystallization rate. It is therefore quite straightforward to expect that a significant change in the molecular mobility in the amorphous phase should be observed depending on the length of the glycolic subunit.

For terephthalic polyesters and other polymeric systems containing n methylene units in their backbone, the literature reports that the melting temperature follows a so-called even-odd effect [48, 49, 13]. This effect is due to the fact that the melting temperature is not only related to the flexibility of the polymer chains, but also to the chain conformations and to the crystal structure [49]. The even-odd effect has recently been reported in furan-based polymers with a higher number of methylene units (up to 12) by Papamokos et al. [46]. They showed that the polymers with an odd number of methylene units are not able to crystallize when heated at a rate of  $10 \ K \ min^{-1}$  after melt quenching. This

finding indicates that the polymers containing an odd number of methylene units have a lower crystallizability, i.e. crystallization occurs at a lower rate as compared to those containing an even number of methylene units. In a following work Guidotti et al. [13] reported that, after storage at room temperature for one month, only the 2,5-FDCA-based homopolymers containing an even number of -CH<sub>2</sub>- groups in the glycolic subunit (poly(butylene 2,5-furanoate) with n=4 and poly(hexamethylene 2,5-furanoate) with n=6) were able to develop a three-dimensional ordered crystalline phase, the other two (poly(propylene 2,5-furanoate) with n=3 and poly(pentamethylene 2,5-furanoate) with n=5) remained completely amorphous. Table 2 shows that, for both furan-based and terephthalic polyesters, an increased length of the glycolic subunit leads to a decrease in the glass transition temperature (measured as the midpoint of the glass transition) that can be attributed to the increased flexibility of the polymer chains. It also appears that the furan-based samples tend to have higher glass transition temperatures with respect to their terephthalatic counterparts, except when the number of methylene groups is equal to 4. These findings suggest that the furan-based samples have a less flexible backbone and/or develop stronger intermolecular interactions with respect to their terephthalic counterparts. In a recent study comparing the chain motions in PEF and PET, Burgess et al. [3] showed that the furan ring-flipping motions are largely suppressed due to the non-linear axis of ring rotation in addition to a strong ring polarity, which is not the case of the phenyl ring-flipping motions in PET. This further supports the fact that PEF has a less flexible backbone with respect to PET.

The cooperativity length at the dynamic glass transition ( $\xi_{\alpha}$ ) has been estimated for all the samples by using equation 1. From the literature, the possible changes in the CRR size are generally attributed either to chemical and/or physical modifications of the intermolecular interactions [50, 30, 26, 27, 25, 28], or to confinement effects [23, 22, 21]. Table 2 shows that the CRR size decreases as the length of the glycolic subunit increases in both furan-based and terephthalic polyesters. The average CRR size for PBT is much lower compared to PET and PPT because the PBT sample investigated in this work is indeed

semi-crystalline (quenching from the melt was unsuccessful), and the cooperativity length is highly impacted by the confinement effects introduced by the crystallization process [52, 24, 53]. About the other samples, the confinement effects due to crystallization are not a possible explanation for the decrease in the CRR size, since all the samples were confirmed to be in their fully amorphous state prior to measurement. The decreased CRR size could then be explained by a change in the intermolecular interactions resulting from the presence of a longer glycolic subunit in the repeating unit. Indeed, the presence of longer glycolic subunits decreases the dipole density, which in turn decreases the overall strength of the intermolecular interactions, as reported for other polymeric systems [26, 25]. The loss of inter-chain interactions due to an increased length of the glycolic subunit is more pronounced in the furan-based polyesters as compared to their terephthalic counterparts; however, this effect is only observed when the number of methylene groups increases from n=2 to n=3, because the presence of an additional methylene (n = 4) seems to have no significant effect on the value of  $\xi_{\alpha}$ . In the future it would be interesting to investigate longer series of samples (n > 4) to confirm the possible existence of a "cooperativity threshold" at n=3, beyond which the inter-chain interactions are not significantly affected by a further increase in the glycolic subunit's length. Qin et al. [54] compiled literature data for dynamic fragility m for six types of glass-forming liquids including polymers, and showed that different categories of glass-forming liquids may exhibit different behaviours in terms of correlation between m and  $T_g$  (linear increase in m with increasing  $T_g$  for hydrogen-bonding organic, polymeric and metallic glass formers, versus a value of m almost independent of  $T_q$  for inorganic glass formers). They also pointed out a different dependence of the apparent activation energy  $E_g$  on  $T_g$  (increase to the  $2^{nd}$ power for hydrogen-bonding organic, polymeric and metallic glass-forming liquids, versus a linear dependence for inorganic glass formers). Evans et al. [55] investigated the effect of confinement on  $T_q$  in seven polymer systems of singlelayer films supported on silicon substrates (i.e. with no substantial substrate interactions) and concluded that fragility is a key variable governing the extent of  $T_g$ -confinement effects, as it reflects the local packing efficiency in a polymer glass. The fragility index can be obtained from calorimetric experiments if the temperature dependence of the relaxation time is known [56]. This can be done by using the Tool-Narayanaswamy-Moynihan (TNM) equation:

$$\tau = \tau_0 \exp\left(\frac{x\Delta h^*}{RT}\right) \exp\left(\frac{(1-x)\Delta h^*}{RT_f}\right)$$
 (5)

Where  $\tau_0$  is a pre-exponential factor, x is a non-linearity parameter,  $\Delta h^*$  is the apparent activation energy, R is the gas constant and  $T_f$  is the fictive temperature. In equation 5,  $T_f$  depends on the cooling rate and characterizes the instantaneous structure of the glass, i.e. the greater the cooling rate, the higher the fictive temperature [56]. The fragility index m is usually determined from calorimetric experiments by using equation 6:

$$m = \frac{dln(|\beta_c|)}{T_g ln 10 d(1/T_f')} \tag{6}$$

where  $\beta_c$  is the cooling rate and  $T'_f$  is the limiting fictive temperature. The variation of  $ln(|\beta_c|)$  as a function of  $1/T'_f$  is supposed to be linear, and the slope of the corresponding curve is proportional to the fragility index [56].

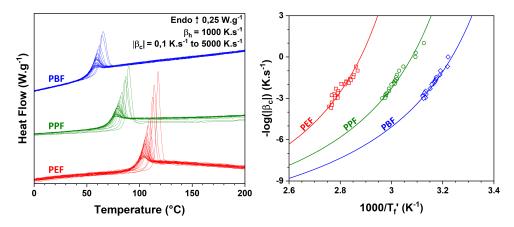


Figure 2: (Left) Heat Flow measured by FSC in the glass transition region on amorphous samples obtained with cooling rate ranging from 0.1 K  $s^{-1}$  to 5000 K  $s^{-1}$  for PEF, PPF, PBF and characterized with a heating rate  $\beta_h$ =1000 K  $s^{-1}$ . (Right) Arrhenius plot of  $\log(|\beta_c|)$  vs.  $1000/T_f'$ .

Figure 2 (left) shows the Heat Flow signals recorded by FSC at a heating rate of  $\beta_h = 1000Ks^{-1}$  on PEF, PPF and PBF samples cooled down from the molten state at different cooling rates ranging from  $|\beta_c| = 0.1Ks^{-1}$  to  $|\beta_c| = 5000Ks^{-1}$ .

The fictive temperature  $T_f$  has been estimated for each cooling rate  $\beta_c$  and the variation of  $ln(|\beta_c|)$  as a function of  $1/T_f'$  has been plotted to estimate the fragility index according to equation 6. As reported in previous studies [57] and clearly shown in Figure 2, the temperature dependence of  $ln(|\beta_c|)$  follows a non-linear trend as also observed by DRS measurements (Figure 3). The temperature evolution can then be described by a Vogel-Fulcher-Tammann (VFT) equation 7:

$$\tau_{\alpha}(T) = \tau_{\infty} exp\left(\frac{DT_0}{T - T_0}\right) \tag{7}$$

Where  $\tau_0$  is a pre-exponential factor, D is a dimensionless parameter related to the slope change (steepness strength), and  $T_0$  is a reference temperature. A modified form of equation 7 is often used to investigate the limiting fictive temperature:

$$ln(|\beta_c|) = A_\beta - \left(\frac{DT_0}{T_f' - T_0}\right) \tag{8}$$

Where  $A_{\beta}$  is a constant. Equation 8 was used to fit the data reported in Figure 2 and successfully followed the temperature dependence of  $ln(|\beta_c|)$ . In the literature, a direct correlation between the cooling rate and the relaxation time was established using the Frenkel-Kobeko-Reiner (FKR) relationship 9 [57]:

$$|\beta_c|\tau = |\beta_c|\omega = C \tag{9}$$

Where  $|\beta_c|$  is the cooling rate,  $\tau$  is the relaxation time, and C is a constant. The FKR relationship allows to directly correlate the results obtained by FSC and the results obtained by DRS. Thus, the same VFT parameters  $(D \text{ and } T_0)$  were used to fit the results obtained by FSC and DRS, with a simple logarithmic shift equal to log(C). The relaxation maps  $(log10 \ [\tau_{max}])$  as a function of 1000/T obtained by DRS on the fully amorphous furan-based samples are reported in Figure 3 (open symbols). Similar values of VFT fitting parameters were obtained with FSC and DRS results (Table 3). The results obtained by

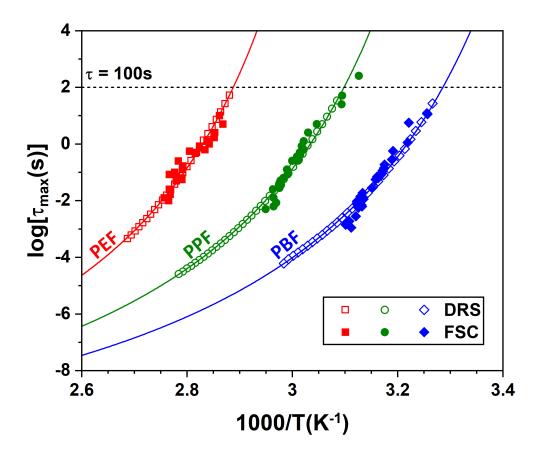


Figure 3: Relaxation maps ( $log10~[\tau_{max}]$  as a function of 1000/T) obtained by both DRS and FSC on fully amorphous PEF, PPF and PBF.

FSC were shifted along the Y-axis using the log(C) values issued from the FKR equation 9, as shown in Figure 3 (close symbols). The FSC and DRS data are consistent with each other, in agreement with the results previously reported in the literature for other polymeric systems [57].

The calculation of the calorimetric fragility should be done taking into account this logarithmic shift of the temperature as a function of the cooling rate whenever the results are to be compared with DRS measurements. Therefore, equa-

tion 6 was rewritten as:

$$m = \left[\frac{d(\log \tau)}{d(\frac{T_g}{T})}\right]_{T=T_g} \tag{10}$$

With  $T_g$  the glass transition temperature measured on a glass formed at a cooling rate  $|\beta_c| = 10^{-2}$  times C. On the other hand, the dielectric fragility was calculated at a temperature  $T_g$  equal to the dielectric glass transition temperature, i.e. the temperature at which a relaxation time of  $\tau = 100s$  is observed. As expected, the calorimetric and dielectric fragilities (Table 3) are in close agreement, which confirms the reliability of the two approaches and the accuracy of both the sets of experimental results.

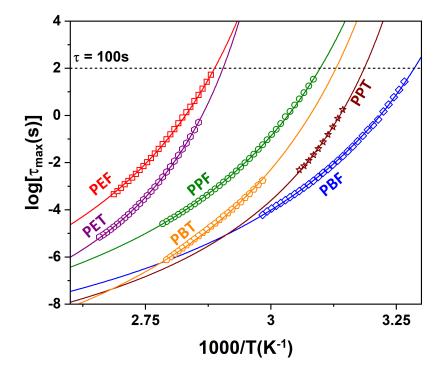


Figure 4: Relaxation maps obtained for amorphous samples of PEF, PPF, PBF, PET, PBT and PPT. The solid lines represent the best fit using VFT equation for the  $\alpha$ -relaxation. The fitting curves of the  $\alpha$ -relaxation have been extrapolated in order to estimate the temperature at which a relaxation time  $\tau=100$ s is observed.

The relaxation maps (log10 [ $\tau_{max}$ ] as a function of 1000/T) obtained by DRS measurements performed on the fully amorphous samples (except PBT) are reported in Figure 4. All the samples show a non-linear dependence of the  $\alpha$ -relaxation time with temperature. The VFT law (equation 7) was used to

fit the experimental data in the  $\alpha$ -relaxation temperature range. The fragility index was estimated using Angell's equation (equation 10). The values of both  $T_g(\tau=100s)$  and the fragility index m are reported in Table 3. The fragility index is not significantly impacted by the increased length of the glycolic subunit (in agreement with the results previously reported by Soccio et al. [14]), only the value of  $T_g(\tau=100s)$  decreases. Besides, the values of the dielectric glass transition temperature are similar to the values of the calorimetric glass transition temperature determined by MT-DSC (Table 2), whose decrease has been attributed to the increased flexibility of the polymer chains. As pointed out in recent studies, the fragility index m is supposed to depend on the packing efficiency of the polymer chains in the amorphous phase [58, 59, 60] as well as on the stiffness of their backbone [30, 61, 31, 62].

If the backbone flexibility actually increases as a consequence of a longer glycolic subunit [63, 64], a decrease in the fragility index should be observed in both the furan-based and the terephthalic polyesters. However, the fragility index of the furan-based samples is constant, independently of the glycolic subunit's length. The same trend has been observed by Papamokos et al. [46] for a larger series of furan-based samples. This observation is consistent with the conclusions previously drawn by Soccio et al. [65] about PBF, asserting that fragility is mainly correlated to the molecular motions of the acidic moiety, in this case the furan ring. The literature reports that, in polymers allowing  $\pi$ -staking, an increase in the glycolic subunit's length can potentially lead to a poorer packing efficiency [66]. It is therefore possible that the increased chain flexibility is compensated by a decreased packing efficiency, and that the overall fragility index remains constant for all the furan-based samples. On the other hand, in the terephthalic polyesters, a slight decrease in the fragility index is observed as the glycolic subunit's length increases, likely explained by an overall increase in chain flexibility accompanied by a slight decrease in the packing efficiency. Table 3 lists the values of fragility index obtained for both the furan-based and the terephthalic polyesters. The furan-based polymers tend to have lower values of m as compared to their terephthalic counterparts, which should mean that they are more flexible and/or have a better chain packing efficiency according to the litterature [30, 61]. However, it has been previously reported that the terephthalic samples have a more flexible backbone as compared to their furan-based counterparts [3], and that furan-based polyesters have a better chain packing efficiency as compared to their terephthalic counterparts. This difference in packing efficiency could be due to the fact that the furan ring allows  $\pi$ -stacking in a more efficient way than the terephthalic ring, probably because of the strong dipolar moment born by the furanic heterocycle [11].

The Kohlrausch-Williams-Watts (KWW) stretching exponent  $\beta_{KWW}$  is an interesting parameter that informs on the distribution of the relaxation times. According to the literature [67], it is possible to calculate the  $\beta_{KWW}$  stretching exponent using the following equation:

$$\beta_{KWW} = (\alpha_{HN}\beta_{HN})^{0.813} \tag{11}$$

Where  $\alpha_{HN}$  and  $\beta_{HN}$  are the Havriliak-Negami fitting parameters. Figure 5 shows the dielectric master curves obtained for all the samples investigated in this study. No differences were observed, suggesting that the flexibility of the polymer backbone of furan-based polyesters has no significant effect on the distribution of the relaxation times. This result, combined with the invariability of the fragility index (Table 3), is supported by the expected correlation between m and the  $\beta_{KWW}$  stretching exponent [68, 69].

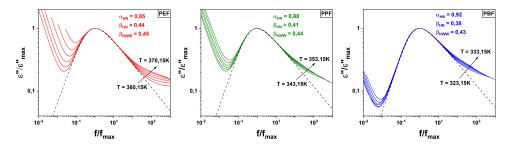


Figure 5: Dielectric master curves obtained for amorphous samples of PEF, PPF and PBF, along with the  $\alpha_{HN}$  and  $\beta_{HN}$  fitting parameters. The  $\beta_{KWW}$  parameter has been estimated according to equation 11.

Figure 6 reports the values of fragility index versus the values of cooperativity for all the investigated samples, as well as for other samples issued from the literature [25, 26]. The theoretical domain corresponding to the volume contribution to fragility (grey area) was determined according to Hong's equation [30] and superimposed on the experimental and literature data. For a given value of  $\alpha_T/\kappa$ , if the change in fragility is only induced by a change in cooperativity, then the evolution of m correlated to the cooperativity length  $\xi_{\alpha}$  should follow a linear trend. This statement is verified here in the case of the terephthalic polyesters. Their behaviour is close to the one observed in PLA with different contents of plasticizer by Araujo et al. [25]. The fact that fragility and cooperativity are correlated means that the isochoric fragility  $m_v$  is constant independently of the length of the glycolic subunit.

This behaviour is not observed in the case of the furan-based polyesters (PEF, PPF and PBF), for which fragility remains constant in spite of a change in cooperativity. A similar trend has also been reported in the case of ethylene-vinyl acetate (EVA) copolymers by Puente et al. [26]. By investigating the segmental mobility of amorphous EVA copolymers with different vinyl acetate (VAc) contents, they showed that the cooperativity decreases as the VAc content decreases (which was attributed to a decrease in the intermolecular interactions), and that the fragility remains constant whatever the VAc content. In other words, they evidenced no direct correlation between fragility and cooperativity. Figure 7 reports the isobaric and isochoric contributions to the fragility index obtained with Hong's equation, and gives a better illustration of the variation of  $m - m_v$  and  $m_v$  in both the furan-based and terephthalic polyester samples. As previously observed, the isochoric fragility  $m_v$  of the terephthalic samples does not depend on the length of the glycolic subunit (except for PBT, whose increased isochoric fragility can be explained by the presence of crystals). On the other hand, the volume contribution of the furan-based samples significantly decreases as the length of the glycolic subunit increases, which can be explained by a decrease in cooperativity. The decrease in volume contribution is accompanied by a significant increase in isochoric fragility; however, this trend is only

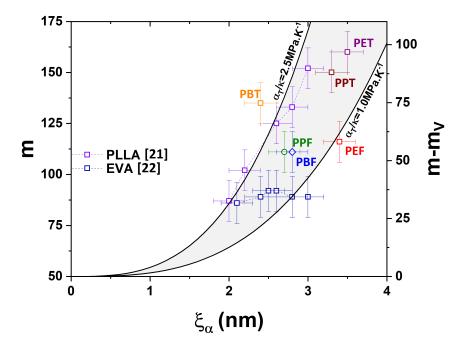


Figure 6: Fragility index versus cooperativity length for PEF, PPF and PBF as compared to PET, PTT and PBT. The data for poly(L-lactic acid) (PLLA) and ethylene-vinyl acetate (EVA) copolymers were extracted from the literature [25, 26] and added for comparison. Dashed lines are also added as a guide for the eye. The black solid lines correspond to the theoretical  $m - m_v$  curves obtained with  $\alpha_T/\kappa$  equal to 1.0 and 2.5  $MPa~K^{-1}$  respectively, which are the extremes of the admitted range for the  $\alpha_T/\kappa$  ratio according to Hong et al. [30]. The grey area represents the theoretical domain where there is a volume contribution to fragility  $m - m_v$ .

observed when the number of methylene groups is increased from n=2 to n=3, whereafter changes in the number of methylene groups has no significant effect, neither on the volume nor on the isochoric contribution. Figure 7 clearly shows that PEF and PET have similar volume contributions to the fragility index, which is expected to correlate with similar cooperativity length. However, PET shows a significantly higher isochoric fragility with respect to PEF.

According to Hong et al. [30], the isochoric fragility depends on the chemical structure of the polymer, and therefore on the type of intermolecular interactions (hydrogen-bonding, ionic or Van der Waals interactions) as well as on the

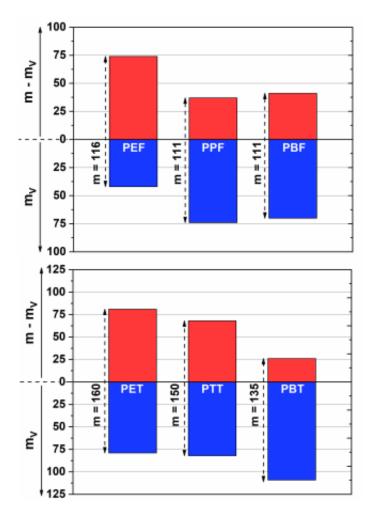


Figure 7: Colored bars represents the two fragility contributions, i.e. the volume contribution  $m - m_v$  (blue) and the isochoric contribution  $m_v$  (red), calculated from experimental measurements on fully amorphous furan-based and terephthalic polyester samples. PBT is an exception, because quenching from the molten state did not yield a fully amorphous sample.

intramolecular degrees of freedom (rotational energy barriers). They showed that an increase in chain flexibility leads to a decrease in the  $m_v$  value. As previously mentioned, the two main parameters affecting the fragility index are the stiffness of the polymer backbone and the packing efficiency of the macromolecular chains [30, 61, 31]. PEF and PET have similar volume contributions

to the fragility index, however PET is known to have a greater chain flexibility compared to PEF; this means that the differences observed in the  $m_v$  values might actually be attributed to strong differences in the chain packing efficiency. The fact that PEF macromolecular chains have a good packing efficiency in the amorphous phase thanks to the  $\pi$ -staking of the aromatic furan rings has already been reported in the literature [11, 46]. This work additionally shows that an increase in packing efficiency also leads to a significant decrease in the isochoric fragility value. This assumption is further supported by the differences in isochoric fragility observed within the series of furan-based polyesters (PEF, PPF and PBF), PEF being the furan-based polyester with the highest packing efficiency. From Figure 7 it is also possible to notice that PPF and PTT have different volume contributions accompanied by different cooperativities, which is not observed when PEF is compared to PET. However, their isochoric fragilities are similar, which can be attributed to a different backbone stiffness and chain packing efficiency, differently compensated in PPF as compared to PTT. Finally, PBT shows a very high value of isochoric fragility as compared to all the other samples; this difference could eventually be due to a much poor chain packing efficiency, but indeed no definite conclusions can be drawn because the applied quenching protocol failed to achieve a fully amorphous PBT sample.

# 3.1. CRR (extended Donth + extended Hong)

The method proposed by Saiter et al.[20] combines calorimetric and dielectric experimental techniques to extend Donth's approach over a wider range of temperatures and frequencies, allowing to investigate the temperature dependence of the CRR size. This approach was applied to the dielectric experiments performed on all the samples (except for PBT, which was not quenched to the fully amorphous state).

Figure 8 reports the evolution of the cooperativity length  $\xi_{\alpha}$  as a function of the temperature normalized to the glass transition temperature obtained from MT-DSC for all the samples in their fully amorphous state. A non-linear temperature dependence of the CRR size is observed in all cases, which is due to

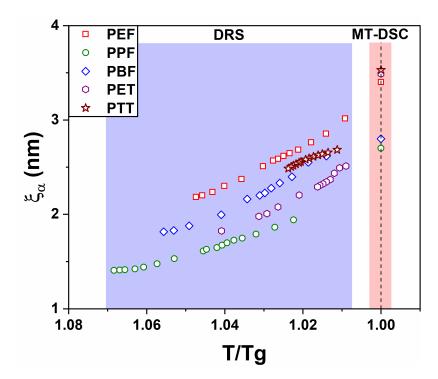


Figure 8: Values of cooperativity length ( $\xi_{\alpha}$ ) obtained from MT-DSC and DRS experiments for all the samples investigated in this work (PEF, PPF, PBF, PET and PTT, except for PBT that could not be quenched to the fully amorphous state) as a function of the temperature normalized to the glass transition temperature obtained from MT-DSC.

the temperature dependence of the relaxation time, as reported in the literature [70]. By combining this approach to the one proposed by Hong et al.[30], the temperature dependence of the dielectric fragility, as well as the temperature dependence of the isobaric and isochoric fragilities, were estimated over a wide range of temperatures.

Figure 9 shows that the isobaric and isochoric fragilities have different temperature dependencies. A strong temperature dependence is observed for the isobaric fragility, which means that its variation is thermo-activated, likely because it is directly proportional to the variation of free volume (expansion/contraction). According to previous works reported in the literature, the variations of iso-

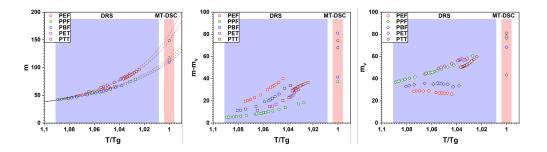


Figure 9: Dielectric (left), isobaric (middle) and isochoric (right) fragilities as a function of temperature, as estimated from the approaches proposed by Saiter et al.[20] and Hong et al.[30]. The dotted line on the left figure represents the best VFT fit.

baric fragility can be mostly attributed to changes in the inter-chain interactions [30, 61]. On the other hand, the isochoric fragility appears to be less temperature dependent, likely because its variation is mainly driven by changes in the intra-molecular interactions, that have been proved to be less affected by temperature fluctuations.

### 4. Conclusion

When the length of the glycolic subunit (that is to say, the number of methylene groups) in a polyester backbone increases, the inter-chain interactions decrease, thus producing a decrease in the cooperativity. This result was obtained for both furan-based and terephthalic polyesters quenched from the melt to their fully amorphous state. However, for the furan-based polyesters, no direct correlation between the fragility index and the cooperativity was observed as a consequence of the different length of their glycolic subunit. The differences in the isochoric fragilities obtained for the furan-based polyesters as compared to their terephthalic counterparts have been considered to result from a combination of backbone flexibility and packing efficiency of the macromolecular chains in the amorphous phase. An increase in chain flexibility generally leads to a decrease in isochoric fragility. However, in the case of furan-based polyesters, this can also be accompanied by a decreased packing efficiency. The comparison

of furan-based and terephthalic polyesters with different lengths of the glycolic subunit suggested that the values of isochoric fragility in the fully amorphous samples depend on both the backbone stiffness and the packing efficiency of the macromolecular chains.

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Table 1: List of the furan-based polyesters and their terephthalic counterparts, with indication of the source, the number-average molecular weight  $(\overline{M}_n)$  and the weight-average molecular weight  $(\overline{M}_w)$ .

SAMPLE	REPETITIVE UNIT	SOURCE	$\overline{M}_n$	$\overline{M}_w$	
			$(gmol^{-1})$	$(gmol^{-1})$	
PEF	Ln	FBR, Wageningen	15 300	18 200	
		The Netherlands			
PPF		DICAM, Bologna	n.a	62 000	
	_	Italy			
PBF	l	FBR, Wageningen	36 000	74 500	
		The Netherlands			
PET		Carolex Co.	31 000	62 000	
PTT	Ju	FBR, Wageningen	16 500	30 500	
		The Netherlands			
PBT	L	Celanex 2500	20 000 to 35 000	n.a.	
	39	Hoechst Co.			

Table 2: Thermal parameters extracted from the MT-DSC curves in Figure 1.  $T_g$  is the glass transition temperature measured as the midpoint of the glass transition.  $T_c$  and  $T_m$  are respectively the cold crystallization and melting temperatures measured at the maximum of the peak.  $\delta T_{cc}$  is the width of the cold crystallization peak measured as the difference between the onset and endset temperatures.  $\Delta T_g$  and  $\Delta C_p^0$  are the width of the glass transition and the Heat Capacity step change at the glass transition temperature estimated from the Reversing Heat Capacity signal using the 16-84% method by Hempel et al. [50].  $T_\alpha$  and  $\delta T_g$  are respectively the temperature and the width of the  $\alpha$ -relaxation peak observed on the Non-Reversing Heat Capacity signal.  $\xi_\alpha$  is the cooperativity length at the dynamic glass transition estimated according to Donth's model[18, 51].

SAMPLE	$T_g$	$\Delta T_g$	$\Delta C_p^0$	$T_{\alpha}$	$\delta T_g$	$\xi_{lpha}$	
	±1 [°C]	±1 [°C]	$\pm 0.01 \ [J \ g^{-1}.^{\circ}C^{-1}]$	±1 [°C]	±1 [°C]	$\pm 0.1 \text{ [nm]}$	
PEF	83	6.8	0.39	82	2.8	3.4	
PPF	57	7.7	0.37	56	2.6	2.7	
PBF	38	4.3	0.33	38	2.6	2.8	
PET	80	4.7	0.32	79	2.1	3.5	
PPT	47	3.9	0.36	44	2.1	3.3	
PBT	43	13.5	n.d	41	4.7	2.4	

Table 3: Parameters obtained with the VFT fitting procedure applied to DRS experimental curves.  $T_g$  ( $\tau$ =100s) is the dielectric glass transition temperature, i.e. the temperature at which a relaxation time of 100s is observed, m is the fragility index,  $(m-m_v)$  and  $m_v$  are the isobaric and the isochoric fragilities, respectively.

	FSC			DRS			
SAMPLE	$\log(C)$	$T_g( \beta_c  = 10^{-2}C) \pm 1 \text{ [°C]}$	m	$T_g(\tau = 100s) \pm 1 \ [^{\circ}\text{C}]$	m	$m-m_v$	$\mathbf{m_v}$
PEF	1.7	75	105	73	116	74	42
PPF	1.4	54	94	58	111	37	74
PBF	1.5	38	96	37	111	41	70
PET	n.a	n.a	n.a	71	160	81	79
PPT	n.a	n.a	n.a	40	150	68	82
PBT	n.a	n.a	n.a	46	135	26	109