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A Rational Extended Thermodynamics Model for Metal Electrons in Bounded Domains

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Abstract In this paper we introduce an 8-moment model for metal electrons, deduced through a Rational Extended Thermodynamics macroscopic approach. Afterwards, we focus on an electron gas confined in a bounded domain and discuss the assignment of the boundary data, taking into account also the wall effects.

Keywords Rational Extended Thermodynamics · Metal Electrons · Boundary conditions

1 Introduction

We present a model for the free electrons bounded within a metal. Following the original idea by Sommerfeld [1–4], we assume that the electrons in the metallic body are described as free fermion particles of mass m . Electrons can collide occasionally with a lattice ion (mass M), but their energy is unchanged by a collision, due to the large ratio M/m . In fact, the ions are modeled as rigid spheres, at rest at their lattice point and their density is uniform and constant. Moreover, we suppose that the electrons do not collide with each other.

In order to construct the model, we will refer to Rational Extended Thermodynamics (RET) [4, 5], a macroscopic theory based on a different strategy

Dedicated to Professor Tommaso Ruggeri on his seventieth birthday.

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with respect to Classical Thermodynamics (CT). In fact, RET considers as field variables not only those of CT (mass density, momentum and energy) but also the stress tensor, the heat flux and others. The corresponding field equations are balance laws supplemented by local and instantaneous constitutive equations, that are determined by the requirement of validity of universal physical principles, like the entropy principle (existence of an entropy inequality and concavity of the entropy density) and the principle of relativity. During the last decades, RET proved to be a very powerful theory, capable of describing non-stationary physical phenomena through hyperbolic PDE systems, overcoming the paradox of infinite velocities due to parabolic PDE models. At the beginning, the theory was proposed by Müller, Ruggeri and other researchers for rarefied monatomic gases [4], but in the last years it has been generalized to rarefied polyatomic gases both in the classical [5] and in the relativistic framework [6] and also to quantum systems [7], obtaining relevant results and good agreement with experimental data.

In order to introduce a simple RET model for the metal electron gas, we will focus on the 8-moment model, that was already considered by Müller within the context of the kinetic theory [3,4]. Here we will follow a different macroscopic approach to write the equation system. However, a comparison with the model by Müller will be also presented and the advantages together with the limit of the present procedure of construction will be discussed. From another point of view, the mathematical peculiarities of the RET 8-moment models were summarized by Ruggeri in [8].

A very important question is related to the assignment of the boundary data when the electron gas is confined in a bounded domain, which is, of course, a very natural problem for the physical phenomena we are dealing with. Here, the boundary data prescription will be analyzed both from a macroscopic and a microscopic point of view, presenting, for the first time, the boundary conditions that have to be imposed to account for the interaction between the electrons and the boundaries.

2 Balance equations

In order to derive the balance equations, following [1,2], we assume that the state of the electron gas is described by the phase density $f(\mathbf{x}, \mathbf{c}, t)$ of electrons at the position \mathbf{x} , with the velocity \mathbf{c} and at the time t . The phase density must satisfy the Boltzmann equation, which assumes the form

$$\frac{\partial f}{\partial t} + c_i \frac{\partial f}{\partial x_i} + f_i \frac{\partial f}{\partial c_i} = S, \quad (1)$$

where S stands for the collision term, while f_i represents the specific external force acting on the particles which, in a metal gas, is the Lorentz force

$$f_i = -\frac{q}{m} [E_i + (\mathbf{c} \wedge \mathbf{B})_i], \quad (2)$$

with $-q$ the charge of an electron, m its mass, ' \wedge ' the symbol of the vector product, \mathbf{E} the electromotive intensity and \mathbf{B} the magnetic flux density.

The multiplication of equations (1) by a generic function $\varphi(\mathbf{x}, \mathbf{c}, t)$ and the subsequent integration over the whole range of \mathbf{c} provides the generic moment equation for the electron gas that is

$$\frac{\partial \bar{\varphi}}{\partial t} + \frac{\partial c_i \bar{\varphi}}{\partial x_i} - \frac{\partial \varphi}{\partial t} + c_i \frac{\partial \varphi}{\partial x_i} + (f_i + i_i^c) \frac{\partial f}{\partial c_i} = \int \varphi S d\mathbf{c}. \quad (3)$$

The symbol $\bar{\varphi}$ denotes the moment $\int \varphi f d\mathbf{c} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{+\infty} \varphi f d c_1 d c_2 d c_3$.

In order to construct our macroscopic equation model, setting $\varphi = m, m c_i, m c^2, m c^2 c_i, \dots$ in equation (3), it is possible to construct an infinite hierarchy of moment equations that we truncate to the first eight moments:

$$\begin{aligned} \text{the mass density} & \quad \rho = \int m f d\mathbf{c}, \\ \text{the mass flux or the momentum density} & \quad J_i = \int m c_i f d\mathbf{c}, \\ \text{the energy density} & \quad e = \frac{1}{2} \int m c^2 f d\mathbf{c}, \\ \text{the heat flux} & \quad q_i = \frac{1}{2} \int m c^2 c_i f d\mathbf{c}. \end{aligned} \quad (4)$$

We also recall that $S_i = -\frac{q}{m} J_i$ is the electric current density.

From equation (3), we get the set of eight balance equations for the eight field variables ρ, J_i, e and q_i which assumes the form

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \frac{\partial J_k}{\partial x_k} &= 0, \\ \frac{\partial J_i}{\partial t} + \frac{\partial P_{ik}}{\partial x_k} - \left(-\frac{q}{m} E_i\right) \rho - \left(-\frac{q}{m} \epsilon_{ijk} B_k\right) J_j &= G_i, \\ \frac{\partial e}{\partial t} + \frac{\partial q_k}{\partial x_k} - \left(-\frac{q}{m} E_k\right) J_k &= 0, \\ \frac{\partial q_i}{\partial t} + \frac{1}{2} \frac{\partial \rho_{lik}}{\partial x_k} - \left(-\frac{q}{m} E_k\right) (P_{<ik>} + \frac{5}{3} e \delta_{ik}) - \left(-\frac{q}{m} \epsilon_{ijk} B_k\right) q_j &= H_i. \end{aligned} \quad (5)$$

In the previous equations, ϵ_{ijk} is the Levi-Civita tensor, $P_{ij} = \int m c_i c_j f d\mathbf{c}$ represents the momentum flux, $\rho_{lik} = \int m c^2 c_i c_k f d\mathbf{c}$ denotes the trace of the fourth moment, δ_{ik} the Kronecker tensor, G_i and H_i the productions, while the square brackets stand for the traceless part of a symmetric tensor.

In order to obtain a closed set of field equations from system (5), the fluxes $P_{<ik>}$ and ρ_{lik} and the productions G_i and H_i must be expressed in terms of the eight field variables ρ, J_i, e and q_i , by material dependent relations.

First of all, in the spirit of RET, we assume that these relations are local in space and time, so that at the time t and in the position \mathbf{x} , they depend on the field at the same time and position, that is

$$\begin{aligned} P_{<ij>} &= P_{<ij>}(\rho, J_i, e, q_i), \\ \rho_{lik} &= \rho_{lik}(\rho, J_i, e, q_i), \\ G_i &= G_i(\rho, J_i, e, q_i), \\ H_i &= H_i(\rho, J_i, e, q_i). \end{aligned} \quad (6)$$

Then, there are different ways to close the truncated moment system (see for example [4,5]) referring to the kinetic theory through a microscopic approach or following a macroscopic approach, based on the validity requirement

of physics principle. Here, as already said in the introduction, we will close the system at a macroscopic level.

3 The closure of the equation system

3.1 The entropy principle

The entropy principle asserts the existence of a concave entropy density h , an entropy flux ϕ_i and a non-negative entropy production Σ , such that the balance equation

$$\frac{\partial h}{\partial t} + \frac{\partial \phi_i}{\partial x_i} = \Sigma \geq 0 \quad (7)$$

holds for every thermodynamic process in an electron gas, that is to say for every solution of the field equation. Also the entropy quantities must be expressed in terms of the field variables by constitutive relations as (6), i.e.

$$\begin{aligned} h &= h(\rho, J_i, e, q_i), \\ \phi_i &= \phi_i(\rho, J_i, e, q_i). \end{aligned} \quad (8)$$

In this section, we will refer to the RET procedure [4] and we will use the entropy principle in order to restrict the functional form of the constitutive functions (6) and (8):

The key of the evaluation of the entropy principle is that the entropy inequality (7) must hold for every thermodynamic process, that is for every solution of the balance equations (5). In this way, equations (5) can be considered as constrains for the fields to satisfy the entropy inequality and these constrains can be taken into account using the Lagrange multipliers, known as main field variables [9,10]. The main field components play a very relevant role: if we refer to them as independent field variables, the PDE system becomes symmetric hyperbolic and this fact guarantees the best mathematical properties of the solutions (see [5] for a historical review of this subject). Here, we assume the existence of eight main field components Λ , Γ_i , Ψ and Π_i that can be expressed in terms of the field variables through constitutive functions of the form (6), so that the inequality

$$\begin{aligned} &\frac{\partial h}{\partial t} + \frac{\partial \phi_i}{\partial x_i} - \Lambda \left[\frac{\partial \rho}{\partial t} + \frac{\partial J_k}{\partial x_k} \right] \\ &- \Gamma_i \left[\frac{\partial J_i}{\partial t} + \frac{\partial P_{ik}}{\partial x_k} - g_i \rho - l_{ij} J_j - G_i \right] \\ &- \Psi \left[\frac{\partial e}{\partial t} + \frac{\partial q_k}{\partial x_k} - g_k J_k \right] \\ &- \Pi_i \left[\frac{\partial q_i}{\partial t} + \frac{1}{2} \frac{\partial \rho u_{ik}}{\partial x_k} - g_k (P_{<ik>} + \frac{5}{3} e \delta_{ik}) - l_{ik} q_k - H_i \right] \geq 0, \end{aligned} \quad (9)$$

must be valid for all ρ , J_i , e and q_i .

For the sake of simplicity, in equation (9) we have set

$$g_i = -\frac{q}{m}E_i \quad \text{and} \quad l_{ij} = -\frac{q}{m}\epsilon_{ijk}B_k. \quad (10)$$

Inserting the constitutive relations (6,8) into inequality (9), one obtains an expression which is linear in the derivatives of ρ , J_i , e and q_i with respect to t and x_k . Then, since the inequality (9) must hold for every field variable, it holds also for every derivative of these quantities. Therefore, imposing that the coefficients of the derivatives vanish, one gets the following set of equations for the entropy density

$$\frac{\partial h}{\partial \rho} = \Lambda, \quad \frac{\partial h}{\partial J_i} = \Gamma_i, \quad \frac{\partial h}{\partial e} = \Psi, \quad \frac{\partial h}{\partial q_i} = \Pi_i, \quad (11)$$

and the the entropy flux

$$\begin{aligned} \frac{\partial \phi_k}{\partial \rho} &= \Gamma_i \frac{\partial P_{<ik>}}{\partial \rho} + \frac{1}{2} \Pi_i \frac{\partial \rho_{lik}}{\partial \rho}, \\ \frac{\partial \phi_k}{\partial J_i} &= \Gamma_j \frac{\partial P_{<jk>}}{\partial J_i} + \frac{1}{2} \Pi_j \frac{\partial \rho_{ljk}}{\partial J_i} + \Lambda \delta_{ik}, \\ \frac{\partial \phi_k}{\partial e} &= \frac{2}{3} \Gamma_k + \Gamma_i \frac{\partial P_{<ik>}}{\partial e} + \frac{1}{2} \Pi_i \frac{\partial \rho_{lik}}{\partial e}, \\ \frac{\partial \phi_k}{\partial q_i} &= \Gamma_j \frac{\partial P_{<jk>}}{\partial q_i} + \frac{1}{2} \Pi_j \frac{\partial \rho_{ljk}}{\partial q_i} + \Psi \delta_{ik}, \end{aligned} \quad (12)$$

while the residual inequality reads

$$\Sigma = \Gamma_i [g_i \rho + l_{ij} J_j + G_i] + \Psi g_k J_k + \Pi_i \left[g_k \left(P_{<ik>} + \frac{5}{3} e \delta_{ik} \right) + l_{ij} q_j + H_i \right] \geq 0. \quad (13)$$

Relations (11-13) summarizes all restrictions for the constitutive functions that can be derived from the entropy inequality.

3.2 Approximation in the neighborhood of the equilibrium

Relations (11-13) cannot be easily used in order to determine the required constitutive functions, for this reason we restrict our attention to processes not far away from the equilibrium state, characterized by vanishing fluxes J_i and q_i . In this way, it is reasonable to approximate the constitutive functions for the entropy quantities, the fluxes and the main field components as

$$\begin{aligned} h &= h_E(\rho, e) + h_1(\rho, e) J^2 + h_2(\rho, e) J_l q_l + h_3(\rho, e) q^2, \\ \phi_i &= \phi_1(\rho, e) J_i + \phi_2(\rho, e) q_i, \\ P_{<ij>} &= 0, \\ \rho_{lij} &= a(\rho, e) \delta_{ij}, \\ \Lambda &= \Lambda_E(\rho, e) + \Lambda_1(\rho, e) J^2 + \Lambda_2(\rho, e) J_l q_l + \Lambda_3(\rho, e) q^2, \\ \Gamma_i &= \Gamma_1(\rho, e) J_i + \Gamma_2(\rho, e) q_i, \\ \Psi &= \Psi_E(\rho, e) + \Psi_1(\rho, e) J^2 + \Psi_2(\rho, e) J_l q_l + \Psi_3(\rho, e) q^2, \\ \Pi_i &= \Pi_1(\rho, e) J_i + \Pi_2(\rho, e) q_i, \end{aligned} \quad (14)$$

where the subscript "E" denotes the equilibrium quantity. We recall that a linearization of the constitutive expression for the fluxes requires that for the entropy quantities and the main field components also the quadratic terms are taken into account [4].

The assumptions (14) and the relations (11,12) yield the following set of equations

$$\begin{aligned}
\frac{\partial h_E}{\partial \rho} &= \Lambda_E, & \frac{\partial h_E}{\partial e} &= \Psi_E, \\
\frac{\partial h_1}{\partial \rho} &= \Lambda_1, & \frac{\partial h_2}{\partial \rho} &= \Lambda_2, & \frac{\partial h_3}{\partial \rho} &= \Lambda_3, \\
\frac{\partial h_1}{\partial e} &= \Psi_1, & \frac{\partial h_2}{\partial e} &= \Psi_2, & \frac{\partial h_3}{\partial e} &= \Psi_3, \\
2h_1 &= \Gamma_1, & h_2 &= \Gamma_2 = \Pi_1, & 2h_3 &= \Pi_2, \\
\frac{\partial \phi_1}{\partial \rho} &= \frac{1}{2}\Pi_1 \frac{\partial a}{\partial \rho}, & \frac{\partial \phi_2}{\partial \rho} &= \frac{1}{2}\Pi_2 \frac{\partial a}{\partial \rho}, \\
\frac{\partial \phi_1}{\partial e} &= \frac{1}{2}\Pi_1 \frac{\partial a}{\partial e} + \frac{2}{3}\Gamma_1, & \frac{\partial \phi_2}{\partial e} &= \frac{1}{2}\Pi_2 \frac{\partial a}{\partial e} + \frac{2}{3}\Gamma_2, \\
\phi_1 &= \Lambda_E, & \phi_2 &= \Psi_E.
\end{aligned} \tag{15}$$

that must be exploited. We start considering the relations (15)_{1,2} and, referring to them, we can deduce that

$$dh_E = \Lambda_E d\rho + \Psi_E de. \tag{16}$$

Comparing (16) and the Gibbs relation

$$dh_E = -\frac{g}{T}d\rho + \frac{1}{T}de, \tag{17}$$

it is possible to obtain the expression of Λ and Ψ at equilibrium:

$$\Lambda_E = -\frac{g}{T} \quad \text{and} \quad \Psi_E = \frac{1}{T}, \tag{18}$$

where T denotes the absolute temperature, $g = \frac{e}{\rho} - \frac{Th_E}{\rho} + \frac{p_E}{\rho}$ is the specific free enthalpy and p_E represents the equilibrium pressure.

Through some rearrangements of relations (15), it is possible to write a partial differential equation for a as a function of ρ and e :

$$\frac{\partial^2 h_E}{\partial e^2} \frac{\partial a}{\partial \rho} - \frac{\partial^2 h_E}{\partial \rho \partial e} \frac{\partial a}{\partial e} = \frac{4}{3} \frac{\partial^2 h_E}{\partial \rho^2}. \tag{19}$$

It is easily verified that, if the expression of the entropy density at equilibrium h_E is known and equation (19) is integrated, all the remaining constitutive relations are determined explicitly from (15). Indeed, in terms of h_E and a , we get

$$\begin{aligned}
\Lambda_E &= \phi_1 = \frac{\partial h_E}{\partial \rho}, & \Psi_E &= \phi_2 = \frac{\partial h_E}{\partial e}, \\
\Pi_1 &= h_2 = \Gamma_2 = \frac{\frac{\partial \Lambda_E}{\partial \rho}}{\frac{1}{2} \frac{\partial a}{\partial \rho}}, & \Gamma_1 &= 2h_1 = \frac{3}{2} \left[\frac{\partial \Lambda_E}{\partial e} - \frac{\frac{\partial \Lambda_E}{\partial \rho}}{\frac{\partial a}{\partial \rho}} \frac{\partial a}{\partial e} \right], & \Pi_2 &= 2h_3 = \frac{\frac{\partial \Psi_E}{\partial \rho}}{\frac{1}{2} \frac{\partial a}{\partial \rho}}, \\
\Lambda_1 &= \frac{\partial h_1}{\partial \rho}, & \Lambda_2 &= \frac{\partial h_2}{\partial \rho}, & \Lambda_3 &= \frac{\partial h_3}{\partial \rho}, \\
\Psi_1 &= \frac{\partial h_1}{\partial e}, & \Psi_2 &= \frac{\partial h_2}{\partial e}, & \Psi_3 &= \frac{\partial h_3}{\partial e}.
\end{aligned} \tag{20}$$

3.3 Change of the independent variables

To simplify the integration of equation (19), we change the independent variables from ρ and e to $-\frac{g}{T}$ and $\frac{1}{T}$ as usually done in RET [4]. So, from the Gibbs relation (17) and the Legendre transformation $h_E = \frac{p_E}{T} - \frac{g}{T}\rho + \frac{1}{T}e$, we get

$$d\left(\frac{p_E}{T}\right) = -e d\left(\frac{1}{T}\right) - \rho d\left(-\frac{g}{T}\right), \quad (21)$$

where $p_E = p_E\left(\frac{1}{T}, -\frac{g}{T}\right)$, and

$$e\left(\frac{1}{T}, -\frac{g}{T}\right) = -p_E - \frac{1}{T} \left(\frac{\partial p_E}{\partial\left(\frac{1}{T}\right)} \right)_{\frac{g}{T}}, \quad \rho\left(\frac{1}{T}, -\frac{g}{T}\right) = -\frac{1}{T} \left(\frac{\partial p_E}{\partial\left(-\frac{g}{T}\right)} \right)_T. \quad (22)$$

The subscribed symbols denote that the indicated quantities are maintained constants during the derivations.

After some calculations, equation (19) can be rewritten in terms of the new independent variables as

$$\frac{\partial a}{\partial\left(-\frac{g}{T}\right)} = -\frac{4}{3} \left[2 \frac{\partial p_E}{\partial\left(\frac{1}{T}\right)} + \frac{1}{T} \frac{\partial^2 p_E}{\partial\left(\frac{1}{T}\right)^2} \right]. \quad (23)$$

Furthermore, since we are dealing with a monatomic gas, we have $p_E = \frac{2}{3}e$ so from equation (22)₁ we get

$$p_E\left(\frac{1}{T}, -\frac{g}{T}\right) = T^{\frac{5}{2}} F\left(-\frac{g}{T}\right). \quad (24)$$

The previous relation expresses the thermal equation of state as a product of functions depending on a single independent variable. Consequently, from (22) and integrating (23) we can write

$$\begin{aligned} e\left(\frac{1}{T}, -\frac{g}{T}\right) &= \frac{3}{2} T^{\frac{5}{2}} F\left(-\frac{g}{T}\right), \\ \rho\left(\frac{1}{T}, -\frac{g}{T}\right) &= -T^{\frac{3}{2}} F'\left(-\frac{g}{T}\right), \\ a\left(\frac{1}{T}, -\frac{g}{T}\right) &= -5T^{\frac{7}{2}} \int F\left(-\frac{g}{T}\right) d\left(-\frac{g}{T}\right) + K\left(\frac{1}{T}\right). \end{aligned} \quad (25)$$

The problem of the determinations of the constitutive functions in the neighborhood of equilibrium is reduced to the determinations of the two single-variable functions $F\left(-\frac{g}{T}\right)$ and $K\left(\frac{1}{T}\right)$. Once we know them, the complete set of field equations appropriate to this process can be recovered from (20).

3.4 Determination of the unknown functions

The unknown function $F\left(-\frac{g}{T}\right)$ can be determined referring to statistical thermodynamics. In fact, as it is well-known, electrons are fermions and their corresponding equilibrium distribution function reads

$$f_E = \frac{y}{e^{-\frac{m}{k_B} \frac{g}{T} + \frac{mc^2}{2k_B} \frac{1}{T}} + 1} = \frac{y}{e^{-\frac{m}{k_B} \frac{g}{T} + \frac{mc^2}{2k_B} \frac{1}{T}} + 1}, \quad (26)$$

where k_B denotes the Boltzmann constant. From $p_E = \frac{1}{3} \int mc^2 f_E dc$ and (26), we obtain the explicit expression for the equilibrium pressure that is

$$p_E = \frac{4}{3} \pi m y \left(2 \frac{k_B}{m} T\right)^{\frac{5}{2}} i_4(\alpha), \quad (27)$$

with

$$\alpha = -\frac{m}{k_B} \frac{g}{T} \quad \text{and} \quad i_n(\alpha) = \int_0^{+\infty} \frac{x^n}{e^{\alpha+x^2} + 1} dx. \quad (28)$$

The integral function $i_n(\alpha)$ is well-known in the framework of degenerate gases theory and several techniques have been developed to calculate it numerically, for an exhaustive review see [11]. Such a function presents some peculiar properties, we recall, among the others, the following recurrence relation

$$\frac{di_n(\alpha)}{d\alpha} = -\frac{n-1}{2} i_{n-2}(\alpha), \quad (29)$$

Now, from comparison of (27) and (24), it is possible to get the explicit form of the function $F\left(-\frac{g}{T}\right)$, that is

$$F\left(-\frac{g}{T}\right) = \frac{4}{3} \pi m y \left(2 \frac{k_B}{m} T\right)^{\frac{5}{2}} i_4(\alpha) \quad (30)$$

and, from (25) and (29), we also get

$$\begin{aligned} e\left(\frac{1}{T}, -\frac{g}{T}\right) &= 2\pi m y \left(2 \frac{k_B}{m} T\right)^{\frac{5}{2}} i_4(\alpha), \\ \rho\left(\frac{1}{T}, -\frac{g}{T}\right) &= 4\pi m y \left(2 \frac{k_B}{m} T\right)^{\frac{3}{2}} i_2(\alpha), \\ a\left(\frac{1}{T}, -\frac{g}{T}\right) &= \frac{4}{3} \pi m y \left(2 \frac{k_B}{m} T\right)^{\frac{7}{2}} i_6(\alpha) + K\left(\frac{1}{T}\right). \end{aligned} \quad (31)$$

The remaining unknown function $K\left(\frac{1}{T}\right)$ cannot be determined through a macroscopic closure procedure. Hence, we conclude that our macroscopic approach furnishes a family of PDE systems that contain an arbitrary function $K(1/T)$. Such a function can be fixed only phenomenologically by a comparison with some physical results or microscopically by a comparison with the results of kinetic theory.

3.5 Concavity of the entropy density

Here we analyze the consequences of the concavity requirement, a condition which follows directly from the entropy principle and that must hold also for the present equation system. Since h must be a concave function of its arguments, at least in the neighborhood of the equilibrium state, we have to impose that the Jacobian of h_E

$$\left\| \begin{array}{cc} -\frac{\partial^2 h_E}{\partial \rho^2} & -\frac{\partial^2 h_E}{\partial \rho \partial e} \\ -\frac{\partial^2 h_E}{\partial \rho \partial e} & -\frac{\partial^2 h_E}{\partial e^2} \end{array} \right\| \quad (32)$$

is a positive-definite matrix.

Taking into account expressions (25) and the change of the independent variables described in the subsection 3.3, the requirement of concavity at equilibrium implies the following conditions for the function $F(\alpha)$:

$$F > 0, \quad F'' > 0, \quad 5FF'' > 3F'^2. \quad (33)$$

It is possible to prove the following theorem:

Theorem 1 *The equation system (5) is equipped with an entropy law with concave entropy density in the neighborhood of equilibrium, if the gas is not completely degenerate.*

Proof 1 *The proof is available in Appendix A.*

3.6 Summary of the results

Here, we briefly summarize the results concerning the constitutive relations, obtained in the previous subsections. Explicitly the field equations are

$$\begin{aligned} \frac{\partial \rho}{\partial t} + \frac{\partial J_k}{\partial x_k} &= 0, \\ \frac{\partial J_i}{\partial t} + \frac{2}{3} \frac{\partial e}{\partial x_i} - g_i \rho - l_{ij} J_j &= G_i \\ \frac{\partial e}{\partial t} + \frac{\partial q_k}{\partial x_k} - g_k J_k &= 0, \\ \frac{\partial q_i}{\partial t} + \frac{1}{2} \frac{\partial a}{\partial x_i} - \frac{5}{3} e g_i - l_{ij} q_j &= H_i, \end{aligned} \quad (34)$$

while the entropy quantities and the main field components read

$$\begin{aligned} h &= \frac{4}{3} \pi m y \theta^{\frac{3}{2}} \left[\frac{k}{m} I_4(\alpha) - \frac{g}{T} I_2(\alpha) \right] + h_1 J^2 + h_2 J_l q_l + h_3 q^2, \\ \phi_i &= \frac{1}{T} q_i - \frac{g}{T} J_i, \\ \Lambda &= -\frac{g}{T} + \Lambda_1(\rho, e) J^2 + \Lambda_2(\rho, e) J_l q_l + \Lambda_3(\rho, e) q^2, \\ \Gamma_i &= \Gamma_1 J_i + \Gamma_2 q_i, \\ \Psi &= \frac{1}{T} + \Psi_1(\rho, e) J^2 + \Psi_2(\rho, e) J_l q_l + \Psi_3(\rho, e) q^2, \\ \Pi_i &= \Pi_1 J_i + \Pi_2 q_i. \end{aligned} \quad (35)$$

where

$$\begin{aligned}
\Pi_1 &= h_2 = \Gamma_2 = 3\beta\theta^{-\frac{7}{2}} \frac{I_4}{I_2 I_6 - I_4^2}, \\
\Pi_2 &= 2h_3 = -6\beta\theta^{-\frac{9}{2}} \frac{I_2}{I_2 I_6 - I_4^2}, \\
\Gamma_1 &= 2h_1 = -\frac{3}{2}\beta\theta^{-\frac{5}{2}} \frac{I_6}{I_2 I_6 - I_4^2}, \\
\Lambda_1 &= \frac{3}{16} \frac{m}{k_B} \beta^2 \theta^{-4} \frac{7I_4^4 - 5I_2 I_4^2 I_6 - 5I_2^2 I_6^2 + 3I_0 I_4 I_6^2}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)}, \\
\Lambda_2 &= -\frac{9}{4} \frac{m}{k_B} \beta^2 \theta^{-5} \frac{3I_2 I_4^2 - 4I_2^2 I_6 + I_0 I_4 I_6}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)} I_4, \\
\Lambda_3 &= \frac{9}{4} \frac{m}{k_B} \beta^2 \theta^{-6} \frac{2I_2^2 I_4^2 + I_0 I_4^3 - 3I_2^3 I_6}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)}, \\
\Psi_1 &= -\frac{3}{8} \frac{m}{k_B} \beta^2 \theta^{-5} \frac{7I_2 I_4^3 - 10I_2^2 I_4 I_6 + 5I_0 I_4^2 I_6 - 2I_0 I_2 I_6^2}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)}, \\
\Psi_2 &= \frac{3}{2} \frac{m}{k_B} \beta^2 \theta^{-6} \frac{2I_2^2 I_4^2 + 7I_0 I_4^3 - 5I_2^3 I_6 - 4I_0 I_2 I_4 I_6}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)}, \\
\Psi_3 &= \frac{9}{2} \frac{m}{k_B} \beta^2 \theta^{-7} \frac{I_2^2 I_4 - 4I_0 I_4^2 - 5I_2^3 I_6 + 3I_0 I_2 I_6}{(I_2 I_6 - I_4^2)^2 (I_0 I_4 - I_2^2)} I_2,
\end{aligned} \tag{36}$$

with the following notations

$$\theta = 2 \frac{k_B}{m} T, \quad \beta = \frac{1}{\pi y m^2}, \quad I_n(\alpha) = (n+1) i_n(\alpha).$$

The PDE system can be also rewritten focusing on the eight new independent field variables (α, J_i, T, q_i) . Indeed, from the previous relation, it is easily proven that

$$\begin{aligned}
\rho_T &= 4k_B \pi y \theta^{\frac{1}{2}} I_2(\alpha), & \rho_\alpha &= -2\pi m y \theta^{\frac{3}{2}} I_0(\alpha), \\
e_T &= 2k_B \pi y \theta^{\frac{3}{2}} I_4(\alpha), & e_\alpha &= -\pi m y \theta^{\frac{5}{2}} I_2(\alpha), \\
a_T &= \frac{4}{3} k_B \pi y \theta^{\frac{5}{2}} \left(I_6(\alpha) - \frac{\tilde{K}(1/T)}{T^2} \right), & a_\alpha &= -\frac{2}{3} \pi m y \theta^{\frac{7}{2}} I_4(\alpha),
\end{aligned} \tag{37}$$

with $K(1/T) = \frac{4}{3} k_B \pi y \theta^{\frac{5}{2}} \tilde{K}(1/T)$. Then, taking into account such relations, the model equation can be also rewritten as

$$\begin{aligned}
4k_B \pi y \theta^{\frac{1}{2}} I_2(\alpha) \frac{\partial T}{\partial t} - 2\pi m y \theta^{\frac{3}{2}} I_0(\alpha) \frac{\partial \alpha}{\partial t} + \frac{\partial J_k}{\partial x_k} &= 0, \\
\frac{\partial J_i}{\partial t} + \frac{4}{3} k_B \pi y \theta^{\frac{3}{2}} I_4(\alpha) \frac{\partial T}{\partial x_i} - \frac{2}{3} \pi m y \theta^{\frac{5}{2}} I_2(\alpha) \left[\frac{\partial \alpha}{\partial x_i} + \frac{1}{\frac{k_B}{m} T} g_i \right] - l_{ij} J_j &= G_i, \\
2k_B \pi y \theta^{\frac{3}{2}} I_4(\alpha) \frac{\partial T}{\partial t} - \pi m y \theta^{\frac{5}{2}} I_2(\alpha) \frac{\partial \alpha}{\partial t} + \frac{\partial q_k}{\partial x_k} - g_k J_k &= 0, \\
\frac{\partial q_i}{\partial t} + \frac{2}{3} k_B \pi y \theta^{\frac{5}{2}} \left(I_6(\alpha) - \frac{\tilde{K}(T^{-1})}{T^2} \right) \frac{\partial T}{\partial x_i} - \\
-\frac{1}{3} \pi m y \theta^{\frac{7}{2}} I_4(\alpha) \left[\frac{\partial \alpha}{\partial x_i} + \frac{1}{\frac{k_B}{m} T} g_i \right] l_{ij} q_j &= H_i.
\end{aligned} \tag{38}$$

3.7 Production terms

The validity of the entropy principle involves also that the production terms G_i and H_i must satisfy the residual inequality (13). Referring to relations (35) and (36), one can easily verify that the residual inequality reduces to the following expression if terms of order higher than the second one are neglected:

$$\Sigma = \Gamma_i G_i + \Pi_i H_i \geq 0. \quad (39)$$

Moreover, the production terms have to be linearized in the neighborhood of the equilibrium according to the approximation approach used in the previous sections. Starting from these two requirements, it is natural to assume that Σ is a positive quadratic form in the main field components Γ_i and Π_i . Hence, if we denote by $\mathbf{\Gamma} = (\Gamma_1, \Gamma_2, \Gamma_3)$ and $\mathbf{\Pi} = (\Pi_1, \Pi_2, \Pi_3)$ and define $\mathbf{A} = \mathbf{A}(\alpha, 1/T)$ as a 6×6 symmetric positive-definite matrix, that could possibly depend only on the equilibrium variables α and $1/T$, we have

$$\mathbf{w} = (\mathbf{\Gamma}, \mathbf{\Pi})^T \quad \Sigma = \mathbf{w}^T \mathbf{A} \mathbf{w} \geq 0. \quad (40)$$

This implies that the production terms are expressed as

$$(\mathbf{G}, \mathbf{H})^T = \mathbf{A} \mathbf{w} \quad (41)$$

and, since the main field components Γ_i and Π_i are expressed as linear combination of J_i and q_i , it is easily verified that the production terms are also combination of J_i and q_i .

In this case, as usual, we cannot determine the explicit expression of the matrix \mathbf{A} referring only to the macroscopic principles. In fact, it is possible to go behind the generic properties of \mathbf{A} only through a comparison with physical phenomena or with kinetic theory results. This fact is not surprising since at a macroscopic level we are not able to prescribe the nature of the interactions between particles: only the physical macroscopic effects can be added to a phenomenological model.

4 A comparison with the kinetic theory closure

As already said in the introduction, the RET 8-moment model was already derived by Müller [3,4] through a microscopic closure. Such an approach is based on the expansion of the distribution function near equilibrium, obtaining a Grad-type expression [12] for $f = f_E(T) + f^{(1)}(c_1, c_2, c_3)$

$$f = \frac{y}{e^{-\frac{m}{k_B} \frac{q}{T} + \frac{mc^2}{2k_B} \frac{1}{T}} + 1} - \frac{y e^{-\frac{m}{k_B} \frac{q}{T} + \frac{mc^2}{2k_B} \frac{1}{T}}}{\left(e^{-\frac{m}{k_B} \frac{q}{T} + \frac{mc^2}{2k_B} \frac{1}{T}} + 1 \right)^2} \left(mc_i \Gamma_i + mc^2 c_i \hat{\Pi}_i \right), \quad (42)$$

where $\hat{\Pi}_i = \Pi_i/2$, and thanks to (6), it is possible to write:

$$\begin{bmatrix} J_i \\ 2q_i \end{bmatrix} = \begin{bmatrix} K_2 & K_4 \\ K_4 & K_6 \end{bmatrix} \begin{bmatrix} \Gamma_i \\ \hat{\Pi}_i \end{bmatrix} \quad (43)$$

with

$$K_A = -\frac{4\pi m^2 y}{3} \int \frac{e^{-\frac{m}{k_B} \frac{q}{T} + \frac{mc^2}{2k_B} \frac{1}{T}}}{\left(e^{-\frac{m}{k_B} \frac{q}{T} + \frac{mc^2}{2k_B} \frac{1}{T}} + 1\right)^2} c^A dc = -\frac{2}{3} \pi m^2 y \theta^{\frac{A+3}{2}} I_A(\alpha). \quad (44)$$

Relation (43) can be inverted, obtaining the expressions for Γ_i and Π_i in accordance with (35) and (36). Carrying on the calculation, one obtains the same results for all the densities and the fluxes except for a . A rapid comparison between our results and those in [3,4] shows that the closure at microscopic level implies that $K(1/T)$, the arbitrary function of our model, must vanish.

The kinetic theory is able to furnish also an explicit expression of the production terms, indeed after some calculations [3,4], the production terms read

$$\begin{bmatrix} G_i \\ 2H_i \end{bmatrix} = -\frac{1}{l} \begin{bmatrix} K_3 & K_5 \\ K_5 & K_7 \end{bmatrix} \begin{bmatrix} \Gamma_i \\ \hat{\Pi}_i \end{bmatrix}, \quad (45)$$

where l denotes the mean free path of an electron between two collisions.

These production terms can be seen as a special case of (41) and it is possible to show that the corresponding matrix \mathbf{A} is positive definite (the proof is similar to the one in Appendix A).

In conclusion, the 8-moment equations that we have introduced in the previous sections can be seen as a family of PDE system that contains also the model from the kinetic theory.

5 Hyperbolicity property

In the previous sections we have approximated the constitutive functions in the neighborhood of an equilibrium state. Therefore we have obtained an equation system that could satisfy the hyperbolicity property characteristic of RET only in a neighborhood of the equilibrium. In this section we will check the validity of such a property. To this aim we recall that a PDE system in the vector form

$$A^0 \frac{\partial \mathbf{U}}{\partial t} + A^i \frac{\partial \mathbf{U}}{\partial x_i} = \mathbf{B}, \quad (46)$$

is defined hyperbolic in the t -direction if $\det(A^0) \neq 0$ and if the eigenvalue problem

$$\det(A^i n_i - \lambda A^0) = 0, \quad (47)$$

admits only real eigenvalues λ and a set of linearly independent right eigenvectors \mathbf{d} , for all unit vectors \mathbf{n} .

In the present model, if we consider as field components $\mathbf{U} = (\alpha, J_i, T, q_i)^T$, we have

$$\det(A^0) = \det \begin{bmatrix} \rho_\alpha & 0 & \rho_T & 0 \\ 0 & 1 & 0 & 0 \\ e_\alpha & 0 & e_T & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \rho_\alpha e_T - e_\alpha \rho_T, \quad (48)$$

which, taking into account (31), yields $\det(A^0) = -4\pi^2 k_B m y^2 \theta^3 (I_0 I_4 - I_2^2) \neq 0$ (see Appendix B).

The characteristic equation (47) reads

$$\det \begin{bmatrix} -\lambda \rho_\alpha & n_i & -\lambda \rho_T & 0 \\ \frac{2}{3} e_\alpha n_i & -\lambda & \frac{2}{3} e_T n_i & 0 \\ -\lambda e_\alpha & 0 & -\lambda e_T & n_i \\ \frac{1}{2} a_\alpha n_i & 0 & \frac{1}{2} a_T n_i & -\lambda \end{bmatrix} = 0, \quad (49)$$

which becomes

$$(\rho_\alpha e_T - e_\alpha \rho_T) \lambda^4 + \frac{1}{2} (\rho_T a_\alpha - \rho_\alpha a_T) \lambda^2 + \frac{1}{3} (e_\alpha a_T - e_T a_\alpha) = 0. \quad (50)$$

When the function $K(1/T) = 0$, that is to say for the model obtained through a comparison with the kinetic theory, the characteristic polynomial reads:

$$(I_0 I_4 - I_2^2) \left(\frac{\lambda}{\sqrt{2 \frac{k_B}{m} T}} \right)^4 + \frac{1}{3} (I_2 I_4 - I_0 I_6) \left(\frac{\lambda}{\sqrt{2 \frac{k_B}{m} T}} \right)^2 + \frac{1}{9} (I_2 I_6 - I_4^2) = 0. \quad (51)$$

We are dealing with a biquadratic equation and it is reasonable to conjecture (see Appendix B) that it presents two couple of real opposite eigenvalues unless the gas is completely degenerate. So, we can conclude that the approximated system is always hyperbolic.

6 Boundary data assignment

In RET the prescription of the boundary conditions represents often a hurdle, well-known in the literature and different methods have been proposed to prescribe the conditions in different frameworks (some examples can be found in [13–16]). The reason is easily understood, if we recall that the field variables in RET include stress tensor components or higher order moments whose values cannot be observed or fixed in an experiment.

If we consider the metal electrons confined in a bounded domain, we have to carefully analysis the questions related to assignment of the boundary data. In this section, we will focus on this problem, limiting our attention to the 1D case, that is to say we imagine the electrons confined in a wire, whose section is negligible with respect to its length. For time-dependent phenomena associated to this system we deal with 4 hyperbolic PDEs with 4 non-vanishing

characteristic velocities, 2 positive and two negative ones (see Appendix B). Hence, we have to prescribe at each wire end two boundary data. A possibility is to assign at the ends of the wire the temperature values and the electric current density.

In the particular case of a stationary phenomenon, the number of boundary data required to solve the system of ODEs is the same as before, since it corresponds to the number of non-zero characteristic velocities. The stationary assumption implies that the electric current density is conserved and so an additional condition is required in order to deal with a well-posed stationary problem. However, in this case, the total number of electrons inside the wire is conserved and the electron number conservation represents the additional condition we are looking for. In other words, in the present case we do not deal with non-controllable boundary data, since the number of the physical quantities that can be prescribed at the boundary is exactly the same as the number of data that are required for the integration of the equation system. So, at a macroscopic level the problem of the boundary data assignment is completely solved.

Nevertheless, if we want to take into account the interaction effect between the electrons and the metal walls, we can refer to an approach similar to that used by Grad [12] in order to describe the interaction between the molecules of a monatomic rarefied gas and the boundary. The idea (already known in kinetic theory for this case [17]) is to account simultaneously two different mechanisms: the specular reflection and the diffuse reflection. We recall that a particle is specularly reflected by the boundary if it is scattered elastically at the surface with reversal of the velocity component normal to the surface, while it is perfectly diffuse reflected if it is brought to thermal equilibrium at the surface.

To better illustrate the basis of the method, we consider a wire of length L lying on the x_1 axis, so that its ends are at $x_1 = 0$ and $x_1 = L$. As an example, we just focus on the boundary at $x_1 = 0$. We denote the incident distribution function as $f^-(c_1, c_2, c_3)$, so $f^-(c_1, c_2, c_3) = 0$ if $c_1 > 0$, and the reflected distribution function by $f^+(c_1, c_2, c_3)$, where $f^+(c_1, c_2, c_3) = 0$ if $c_1 < 0$. Therefore, the distribution function at the boundary reads:

$$f(c_1, c_2, c_3) = f^-(c_1, c_2, c_3) + f^+(c_1, c_2, c_3). \quad (52)$$

We assume that the reflected function is expressed as a combination of specular and diffuse reflections:

$$f^+(c_1, c_2, c_3) = pf^-(-c_1, c_2, c_3) + \mathcal{K}f_E(T_B), \quad (53)$$

where f_E is the distribution function at equilibrium, T_B represents the temperature of the metal boundary, \mathcal{K} is a suitable quantity that will be determined later and the parameter $p \in [0, 1]$ represents the portion of electron specularly reflected by the wall.

Following Grad's approach, we firstly concentrate on the particular case $p = 1$, that is to say the completely specular reflection, for such a case the

distribution function at the boundary

$$f(c_1, c_2, c_3) = f^-(c_1, c_2, c_3) + f^-(-c_1, c_2, c_3) \quad (54)$$

is even in c_1 . Hence, it is possible to prescribe conditions for the moments corresponding to odd powers of c_1 that turn out to be always zero at the boundaries, while the moments corresponding to even powers of c_1 cannot be fixed automatically. In this way, the number of prescription at each boundary is equal to the number of moments corresponding to an odd power of c_1 .

This last result is valid for completely specular reflection, but we want to extend here the method also for the cases $p < 1$ and we take into account only the moments J_1 and q_1 (see (5)).

Let us consider the stationary case and $-qJ_1/m$ denotes the constant value of the electric current density in $x_1 = 0$, we impose that

$$\begin{aligned} J_1 &= \int mc_1 f(c_1, c_2, c_3) d\mathbf{c} = \\ &= \int_{c_1 < 0} mc_1 f^-(c_1, c_2, c_3) d\mathbf{c} + \int_{c_1 > 0} mc_1 f^+(c_1, c_2, c_3) d\mathbf{c} = \\ &= (p-1) \int_{c_1 > 0} mc_1 f^-(-c_1, c_2, c_3) d\mathbf{c} + \mathcal{K} \int_{c_1 > 0} mc_1 f_E(T_B) d\mathbf{c}. \end{aligned} \quad (55)$$

Recalling that in the present case the expression of the linearized distribution function for 1D systems is (42), the previous formula (55) is rewritten as

$$\begin{aligned} J_1 &= \int_{c_1 > 0} mc_1 [(p-1)f_E(T) + \mathcal{K}f_E(T_B)] d\mathbf{c} + \\ &+ (p-1) \int_{c_1 > 0} mc_1 f^{(1)}(-c_1, c_2, c_3) d\mathbf{c}. \end{aligned} \quad (56)$$

After some calculations (see Appendix C for details) we get

$$\begin{aligned} J_1 &= m\pi y \left[((p-1)\theta^2 + \mathcal{K}\theta_B^2) i_3(\alpha) + \right. \\ &\left. + (p-1)m \left(\Gamma_1 \theta^{5/2} i_2(\alpha) + \frac{5}{3} \hat{\Pi}_1 \theta^{7/2} i_4(\alpha) \right) \right] \end{aligned} \quad (57)$$

and from the previous formulas we can deduce \mathcal{K} :

$$\mathcal{K} = 0 \quad \text{if } c_1 < 0 \quad \text{and} \quad \mathcal{K} = (1-p) \frac{\theta^2}{\theta_B^2} + \frac{(p+1)}{2m\pi y \theta_B^2 i_3(\alpha)} J_1 \quad \text{for } c_1 > 0. \quad (58)$$

Likewise, we write now the relation for q_1

$$\begin{aligned} q_1 &= \frac{1}{2} \int mc^2 c_1 f d\mathbf{c} = \\ &= \int_{c_1 < 0} mc^2 c_1 f^-(c_1, c_2, c_3) d\mathbf{c} + \int_{c_1 > 0} mc^2 c_1 f^+(c_1, c_2, c_3) d\mathbf{c} = \\ &= (p-1) \int_{c_1 > 0} mc^2 c_1 f^-(-c_1, c_2, c_3) d\mathbf{c} + \mathcal{K} \int_{c_1 > 0} mc^2 c_1 f_E(T_B) d\mathbf{c}. \end{aligned} \quad (59)$$

Again, recalling formula (42), we have:

$$\begin{aligned} q_1 &= \int_{c_1 > 0} mc^2 c_1 [(p-1)f_E(T) + \mathcal{K}f_E(T_B)] d\mathbf{c} + \\ &+ (p-1) \int_{c_1 > 0} mc^2 c_1 f^{(1)}(-c_1, c_2, c_3) d\mathbf{c}. \end{aligned} \quad (60)$$

After some cumbersome calculations similar to the previous ones, we conclude that

$$q_1 = \frac{\pi m y}{6(1+p)} [(p-1)\theta^3 + \mathcal{K}\theta_B^3] I_5(\alpha), \quad (61)$$

which can be also rewritten as

$$q_1 = \frac{\pi m y}{6} \frac{1-p}{1+p} \theta^2 (\theta_B - \theta) I_5(\alpha) + \frac{1}{3} \theta_B \frac{I_5(\alpha)}{I_3(\alpha)} J_1. \quad (62)$$

This last equation gives the implicit relation between the temperature of the metal at the boundary and the electron temperature at the boundary that has to be used in the ODE integration.

Similar steps can be followed to obtain the boundary conditions at $x_1 = L$.

7 Appendix A

Proof of Theorem 1

In subsection 3.5 we have already recalled that the concavity condition for our model at equilibrium reduces to the three conditions for $F(\alpha)$ given in (33). In what follows we prove that these conditions are verified if $F(\alpha)$ is the function in (30) except for a completely degenerate gas. Indeed, from (29) and (31), it is immediately verified that $F > 0$ and $\frac{d^2 F}{d\alpha^2} > 0$. So, now we focus on the third condition (33)₃. Explicitly, we have

$$5FF'' - 3(F')^2 = \left(\frac{8}{3} \pi m y \left(\frac{2k_B}{m} \right)^{3/2} \right)^2 \left[-\frac{15}{2} i_4(\alpha) \frac{di_2(\alpha)}{d\alpha} - 3 \left(\frac{di_4(\alpha)}{d\alpha} \right)^2 \right]. \quad (63)$$

Hence, the validity of (33)₃ is proven if the term in (63) inside the square bracket is positive. First of all, from (29) we have $-5i_4(\alpha)/2 = \frac{di_6(\alpha)}{d\alpha}$, so condition (33)₃ holds if

$$I = \left[\frac{di_6(\alpha)}{d\alpha} \frac{di_2(\alpha)}{d\alpha} - \left(\frac{di_4(\alpha)}{d\alpha} \right)^2 \right] > 0, \quad (64)$$

furthermore, I can be rewritten explicitly as

$$I = \int_0^\infty \int_0^\infty \frac{\partial f_E(x, \alpha)}{\partial \alpha} \frac{\partial f_E(x, \alpha)}{\partial \alpha} (x^6 y^2 - x^4 y^4) dx dy. \quad (65)$$

Since the expression of the integrand in (65) can be rewritten also exchanging the integration variables x and y , it holds

$$\begin{aligned} I &= \frac{1}{2} \int_0^\infty \int_0^\infty \frac{\partial f_E(x, \alpha)}{\partial \alpha} \frac{\partial f_E(x, \alpha)}{\partial \alpha} (x^6 y^2 - x^4 y^4 + y^6 x^2 - x^4 y^4) dx dy = \\ &= \frac{1}{2} \int_0^\infty \int_0^\infty \frac{\partial f_E(x, \alpha)}{\partial \alpha} \frac{\partial f_E(x, \alpha)}{\partial \alpha} x^2 y^2 (x^2 - y^2)^2 dx dy. \end{aligned} \quad (66)$$

The integrand in (66) is a non-negative function; moreover, its support has clearly a non-zero measure in R^2 , therefore its double integral is strictly positive ($I > 0$).

When the gas is completely degenerate, that is to say when $\alpha \rightarrow -\infty$ and when $I_n(\alpha) \simeq \sqrt{-\alpha}^{n+1}$, the integrand function vanishes and the theorem is no more valid.

We have shown that the entropy density is concave at equilibrium. The same technique as in (64,65) can be used to show that $-(h - h_E)$ is a positive definite quadratic form. Hence, by continuity arguments, one can conclude that h has to be concave in a neighborhood of the equilibrium state.

8 Appendix B

In this appendix we present some results aimed to verify the hyperbolicity property of the model. Following the definition in Section 5, we have preliminarily to show that A^0 is a non-singular matrix and this is true thanks to the proof of Theorem 1.

Then, we focus on (51) in order to verify that the eigenvalues are real and there is a set of linearly independent right eigenvectors. Due to the linearization of the system the matrix \mathbf{A}^i does not depend on J_i and q_i . The characteristic polynomial is a biquadratic form, of the type: $\gamma_1 x^4 + \gamma_2 x^2 + \gamma_3 = 0$. From Appendix A we already know that $\gamma_1 = I_4 I_0 - (I_2)^2 > 0$ if the gas is not completely degenerate. Permuting the integration variables with the same method as in Appendix A, we show that

$$\begin{aligned} \gamma_2 &= \frac{1}{3}(I_2 I_4 - I_0 I_6) = \\ &= -\frac{2}{3} \int_0^\infty \int_0^\infty \frac{\partial f_E(x,\alpha)}{\partial \alpha} \frac{\partial f_E(x,\alpha)}{\partial \alpha} x^2 y^2 (x^2 - y^2)^2 (x^2 + y^2) dx dy < 0, \end{aligned} \quad (67)$$

and

$$\begin{aligned} \gamma_3 &= \frac{1}{9}(I_2 I_6 - (I_4)^2) = \\ &= \frac{2}{9} \int_0^\infty \int_0^\infty \frac{\partial f_E(x,\alpha)}{\partial \alpha} \frac{\partial f_E(x,\alpha)}{\partial \alpha} x^4 y^4 (x^2 - y^2)^2 dx dy > 0, \end{aligned} \quad (68)$$

if the gas is not completely degenerate.

We conjecture that under the same conditions $\gamma_2^2 - 4\gamma_1\gamma_3 > 0$. This idea is supported by several numerical evaluations. If the conjecture is true, we have 4 distinct real eigenvalues (two positive and two negative) and the hyperbolicity requirement is satisfied. In the case of complete degeneration, when $I_n(\alpha) \simeq \sqrt{-\alpha}^{n+1}$, all coefficients of (51) vanish identically, so that no sound can propagate in that case [4].

9 Appendix C

Here, we list the principal integral used to prescribe the boundary conditions as described in section 7. For more clarity, we recall that the symbol $\int \cdot dc$

represents a triple integral, so, here, we consider a transformation in spherical coordinates:

$$\begin{aligned} \int_{c_1 > 0} f_E(T) c^{2n} c_1^l d\mathbf{c} &= \int_0^\infty \int_0^{2\pi} \int_0^\pi \frac{y}{e^{\alpha + \frac{c^2}{\theta}} + 1} c^{2n} c^l \cos^l(\vartheta) c^2 \sin(\vartheta) d\vartheta d\Phi dc = \\ &= \frac{2\pi y}{l+1} \theta^{(2n+l+3)/2} i_{2n+l+2}(\alpha). \end{aligned} \quad (69)$$

$$\begin{aligned} \int_{c_1 > 0} \frac{y e^{\alpha + \frac{c^2}{\theta}}}{(e^{\alpha + \frac{c^2}{\theta}} + 1)^2} c^{2n} c_1^l d\mathbf{c} &= \int_0^\infty \int_0^{2\pi} \int_0^\pi \frac{y e^{\alpha + \frac{c^2}{\theta}}}{(e^{\alpha + \frac{c^2}{\theta}} + 1)^2} c^{2n} c^l \cos^l(\vartheta) c^2 \sin(\vartheta) d\vartheta d\Phi dc = \\ &= \frac{\pi y (2n+l+1)}{l+1} \theta^{(2n+l+3)/2} i_{2n+l}(\alpha). \end{aligned} \quad (70)$$

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