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Random Sampling via Sensor Networks: Estimation Accuracy vs. Energy Consumption

Flavio Zabini, Alex Calisti, Davide Dardari, and Andrea Conti

Abstract—The estimation of spatial processes from sparse sensing nodes is fundamental for many applications, including environmental monitoring and crowd-sourcing. In this paper, we analyze the impact of measurement errors on the estimation of a finite-energy signal sampled by a set of sensors randomly deployed in a finite d -dimensional space according to homogeneous Poisson Point Process. The optimal linear space invariant interpolator is derived. Based on such an interpolator, analytical expressions of both the estimated signal energy spectral density and the normalized estimation mean square error are obtained. An asymptotic analysis for high sensors density with respect to the signal bandwidth is given for scenarios subjected to estimation energy constraint. The normalized estimation mean square error is derived for large wireless sensor networks with constraints on the capacity-per-volume and on battery duration.

I. INTRODUCTION

Self-organizing wireless sensor networks (WSN) has attracted considerable attention in the last years [1]. The possibility to create a network infrastructure composed of low-cost, small-size and energy-limited sensing devices (sensors) has created a large number of applications in smart home, environmental monitoring, crowdsensing and Internet of Things.

For the classical regular sampling, the well-known Whittaker-Kotelnikov-Shannon sampling theorem states that a signal can be perfectly reconstructed from its samples provided that the sampling frequency is larger than twice its bandwidth. For the irregular sampling, a theorem of Landau [2], [3] establishes necessary conditions on samples density for the perfect estimation. In the case of a random sampling in time, the estimation accuracy is usually evaluated in the terms of mean square error (MSE) [4]. In particular, if the sample positions are the output of a stationary Poisson point process (PPP), Marvasti [5] shows that the reconstruction is still possible via ideal low pass (ILP) filtering provided that the average samples density is higher than twice the signal bandwidth, and that the spectrum of the estimated signal is that of the original signal immersed in a white noise floor.

Recently, the extension of Marvasti's result to a multidimensional domain has gained interest due to its application on WSN for environmental monitoring [6]–[10]. The assumption that nodes in a WSN are deployed according to a homogeneous PPP (homogeneous in \mathbb{R}^d corresponds to stationary in \mathbb{R}) is widely adopted [11]–[14].¹ However, many works do not

consider that the ILP filtering is no more optimal for irregular sampling, as widely known in the one-dimension domain in case of jitter [16]–[18]. Moreover, in a realistic sensing scenario, the distortion due to measurement errors and sensors energy consumption have to be considered [19]–[21].

In this paper, by following the approach in [15], we derive the optimal LSI interpolator minimizing the normalized estimation mean square error (NEMSE) by jointly taking into account random sampling, measurement errors and energy consumption. In particular, the estimated signal energy spectral density (ESD) and NEMSE are derived as functions of important parameters such as samples density and distortion. These results aim to answer the following question in multidimensional signal estimation: *given a certain amount of energy spent for the estimation, is it better to have few accurate samples or many inaccurate ones?* Anyway, in an actual WSN, the most relevant estimation energy constraint is not on the whole network, but on each sensor, due to the battery duration limitation. In addition, a constraint on the capacity of each sensor for sending the samples to the interpolation entity has to be taken into account. Therefore, another relevant question is: *when the estimation accuracy of a large WSN is dominated by the capacity-per-volume and when by the sensor lifetime?* By modeling the communication channel between each nodes and the interpolator as an erasure channel, and by considering the capacity-per-volume as a constraint for a large WSN, we derive a simple analytical expression for the NEMSE as a function of both the estimation rate and the capacity-per-volume.

II. SYSTEM MODEL

Consider the signal $z(\mathbf{x}) \in \mathbb{C}$ with support $\mathcal{A} \subseteq \mathbb{R}^d$, finite energy E_z , and ESD $\mathcal{E}_z(\boldsymbol{\nu})$, where $\mathbf{x}, \boldsymbol{\nu} \in \mathbb{R}^d$. Let $\mathcal{F}\{\cdot\}$ and $\delta(\cdot)$ be the Fourier transformation and the Dirac delta generalized function in \mathbb{R}^d , respectively [22]. The homogeneous Poisson sampling process can be expressed as

$$\mathcal{P}(\mathbf{x}) = \sum_{n \in \mathcal{N}(\boldsymbol{\Pi})} \delta(\mathbf{x} - \mathbf{x}_n) \quad (1)$$

where $\boldsymbol{\Pi}$ is the homogeneous PPP in \mathbb{R}^d with intensity ρ [23], \mathbf{x}_n denotes the position of the n -th sample according to $\boldsymbol{\Pi}$, and $\mathcal{N}(\cdot)$ is the index set operator. It is known [24] that

$$\mathbb{E}\{\mathcal{P}(\mathbf{x})\} = \rho \quad (2a)$$

$$\mathbb{E}\{\mathcal{P}(\mathbf{x})\mathcal{P}(\mathbf{x} - \boldsymbol{\tau})\} = \rho^2 + \rho\delta(\boldsymbol{\tau}) . \quad (2b)$$

The sampled signal with measurement errors is given by

$$z_e(\mathbf{x}) = \sum_{n \in \mathcal{N}(\boldsymbol{\Pi}_A)} \hat{z}_n \delta(\mathbf{x} - \mathbf{x}_n) \quad (3)$$

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¹Multidimensional signal reconstruction from inhomogeneous Poisson sampling has been analyzed in [15], where the optimal linear space invariant (LSI) interpolator is derived accounting for random sampling and signal properties.

where $\mathcal{N}(\mathbf{\Pi}_A)$ is the index set of the points of $\mathbf{\Pi}$ falling in A . The n -th sample affected by measurement is

$$\hat{z}_n = z(\mathbf{x}_n) + \mathbf{e}_n \quad (4)$$

where the \mathbf{e}_n 's are zero-mean independent random variables (RVs) with variance σ_n^2 , independent of $\mathcal{P}(\mathbf{x})$. The distortion due to measurement errors is defined as

$$D \triangleq \mathbb{E} \left\{ \sum_{n \in \mathcal{N}(\mathbf{\Pi}_A)} |\mathbf{e}_n|^2 \right\}. \quad (5)$$

Consider the estimation performed by a LSI interpolator $\theta(\mathbf{x})$ with Fourier transform $\Theta(\boldsymbol{\nu})$. In the d -dimensional domain, the term space-invariant takes the place of the usual time-invariant in the one-dimension domain. The estimated signal is given by

$$\hat{z}(\mathbf{x}) = (z_\epsilon * \theta)(\mathbf{x}) = \sum_{n \in \mathcal{N}(\mathbf{\Pi}_A)} \hat{z}_n \theta(\mathbf{x} - \mathbf{x}_n). \quad (6)$$

Two metrics are employed to evaluate the signal estimation accuracy: the ESD of the estimated signal (6) and the NEMSE. The former is

$$\mathcal{E}_{\hat{z}}(\boldsymbol{\nu}) \triangleq \mathcal{F} \left\{ \int_{\mathbb{R}^d} \mathbb{E} \{ \hat{z}(\mathbf{x}) \hat{z}^\dagger(\mathbf{x} - \boldsymbol{\tau}) \} d\boldsymbol{\tau} \right\} = \mathbb{E} \left\{ |\hat{Z}(\boldsymbol{\nu})|^2 \right\} \quad (7)$$

with $\hat{Z}(\boldsymbol{\nu}) \triangleq \mathcal{F} \{ \hat{z}(\mathbf{x}) \}$. The latter is

$$\epsilon_S \triangleq \frac{\int_{\mathbb{R}^d} |z(\mathbf{x}) - \hat{z}(\mathbf{x})|^2}{E_z} \quad (8)$$

where the expectation is with respect the measurement errors and the samples positions. To perform an asymptotic analysis for large sample intensity, we also introduce the following quantities normalized to the signal bandwidth-per-dimension B_z :² the (normalized) spatial frequency $\check{\boldsymbol{\nu}} \triangleq \boldsymbol{\nu}/2B_z$, the Poisson sampling process intensity $\check{\rho} \triangleq \rho/(2B_z)^d$, distortion $\check{D} \triangleq \frac{D}{E_z(2B_z)^d}$, signal ESD $\check{\mathcal{E}}_z(\check{\boldsymbol{\nu}}) \triangleq \frac{(2B_z)^d}{E_z} \mathcal{E}_z(2B_z\check{\boldsymbol{\nu}})$, and estimated signal ESD $\check{\mathcal{E}}_{\hat{z}}(\check{\boldsymbol{\nu}}) \triangleq \frac{(2B_z)^d}{E_z} \mathcal{E}_{\hat{z}}(2B_z\check{\boldsymbol{\nu}})$.

III. SIGNAL ESTIMATION

Lemma 1 (Optimal LSI Interpolator): The transfer function of the LSI which minimizes the NEMSE defined in (8) is given by

$$\Theta(\boldsymbol{\nu}) = \frac{\mathcal{E}_z(\boldsymbol{\nu})}{\rho \mathcal{E}_z(\boldsymbol{\nu}) + E_z \left(1 + \frac{D}{E_z \rho} \right)}. \quad (9)$$

Proof: By extending the Wiener filtering theory to \mathbb{R}^d as done in [15], it can be shown that the LSI interpolator minimizing (8) results in

$$\Theta(\boldsymbol{\nu}) = \frac{Z(\boldsymbol{\nu}) \mathcal{U}_{z_\epsilon}^\dagger(\boldsymbol{\nu})}{\mathcal{E}_{z_\epsilon}(\boldsymbol{\nu})} \quad (10)$$

where $Z(\boldsymbol{\nu}) \triangleq \mathcal{F} \{ z(\mathbf{x}) \}$, $\mathcal{U}_{z_\epsilon}(\boldsymbol{\nu}) \triangleq \mathcal{F} \{ \mathbb{E} \{ z_\epsilon(\mathbf{x}) \} \}$, and $\mathcal{E}_{z_\epsilon}(\boldsymbol{\nu}) \triangleq \mathcal{F} \{ R_{z_\epsilon}(\boldsymbol{\tau}) \}$ with $R_{z_\epsilon}(\boldsymbol{\tau}) \triangleq$

²For finite energy signals with infinite band in \mathbb{R}^d , we consider, for normalization purpose, the extension of the well-known Gabor's bandwidth to \mathbb{R}^d , i.e. $B_z \triangleq \sqrt{\int_{\mathbb{R}^d} \frac{|\boldsymbol{\nu}|^2 \mathcal{E}_z(\boldsymbol{\nu}) d\boldsymbol{\nu}}{E_z}}$.

$\int_{\mathbb{R}^d} \mathbb{E} \{ z_\epsilon(\mathbf{x}) z_\epsilon^\dagger(\mathbf{x} - \boldsymbol{\tau}) \} d\mathbf{x}$. In the sense of distributions, we have from (3), (4), and (6) that

$$z_\epsilon(\mathbf{x}) = z(\mathbf{x}) \sum_{n \in \mathcal{N}(\mathbf{\Pi})} \delta(\mathbf{x} - \mathbf{x}_n) + \sum_{n \in \mathcal{N}(\mathbf{\Pi}_A)} \mathbf{e}_n \delta(\mathbf{x} - \mathbf{x}_n) \quad (11)$$

where the first term follows by the definition of support of $z(\mathbf{x})$. From (2a), (2b), (11), and the independence between \mathbf{e}_n and \mathbf{x}_n , it follows that

$$\begin{aligned} \mathbb{E} \{ z_\epsilon(\mathbf{x}) z_\epsilon^\dagger(\mathbf{x} - \boldsymbol{\tau}) \} &= z(\mathbf{x}) z^\dagger(\mathbf{x} - \boldsymbol{\tau}) [\rho^2 + \rho \delta(\boldsymbol{\tau})] \\ &+ \mathbb{E} \left\{ \sum_{n \in \mathcal{N}(\mathbf{\Pi}_A)} \sigma_n^2 \delta(\mathbf{x} - \mathbf{x}_n) \delta(\mathbf{x} - \boldsymbol{\tau} - \mathbf{x}_n) \right\} \end{aligned}$$

and

$$\mathbb{E} \{ z_\epsilon(\boldsymbol{\tau}) \} = \rho z(\boldsymbol{\tau}) \quad (12a)$$

$$R_{z_\epsilon}(\boldsymbol{\tau}) = [\rho^2 + \rho \delta(\boldsymbol{\tau})] \int_{\mathbb{R}^d} z(\mathbf{x}) z^\dagger(\mathbf{x} - \boldsymbol{\tau}) d\mathbf{x} + D \delta(\boldsymbol{\tau}). \quad (12b)$$

By Fourier transforming (12) in \mathbb{R}^d we obtain

$$\mathcal{U}_{z_\epsilon}(\boldsymbol{\nu}) = \rho Z(\boldsymbol{\nu}) \quad (13a)$$

$$\mathcal{E}_{z_\epsilon}(\boldsymbol{\nu}) = \rho^2 \mathcal{E}_z(\boldsymbol{\nu}) + E_z \left(\rho + \frac{D}{E_z} \right) \quad (13b)$$

which, together with (10) and $\mathcal{E}_z(\boldsymbol{\nu}) = |Z(\boldsymbol{\nu})|^2$, provides (9). \square

Remark 1: By using normalized quantities, for $\check{\rho} \rightarrow +\infty$, the optimal LSI interpolator in (9) tends to $\frac{1}{\rho} \mathbf{1}_{\mathcal{B}_z}(\boldsymbol{\nu})$ where $\mathbf{1}_{\mathcal{B}_z}(\boldsymbol{\nu})$ denotes the indicator function equal to 1 for $\boldsymbol{\nu} \in \mathcal{B}_z$ and 0 otherwise. It means that the ILP filter considered in [6], [8], [9] is an asymptotic optimal choice when the samples intensity which is much higher than the signal band cardinality in \mathbb{R}^d .

Remark 2: In the particular case of $D = 0$ and $d = 1$, (9) reduces to the optimal linear time invariant interpolator for stationary Poisson sampling process found by Leneman in [16] once the ESD is replaced by the power spectral density.

Corollary 1 (Normalized Estimated Signal ESD): When the optimal LSI interpolator in (9) is employed, the normalized ESD of the estimated signal is given by

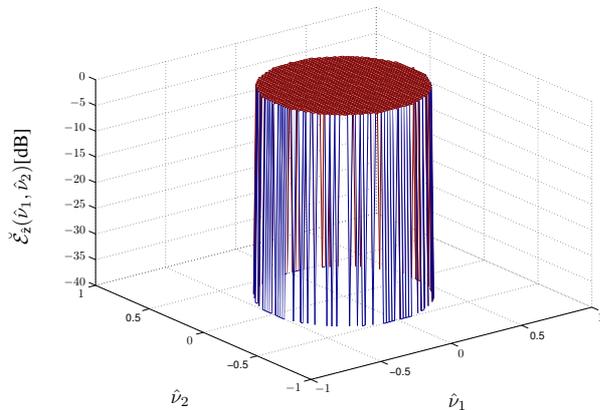
$$\check{\mathcal{E}}_{\hat{z}}(\check{\boldsymbol{\nu}}) = \check{\mathcal{E}}_z(\check{\boldsymbol{\nu}}) \left[\frac{\check{\mathcal{E}}_z(\check{\boldsymbol{\nu}})}{\check{\mathcal{E}}_z(\check{\boldsymbol{\nu}}) + \frac{1}{\check{\rho}} \left(1 + \frac{\check{D}}{\check{\rho}} \right)} \right]. \quad (14)$$

Proof: From (6) and (7), the ESD of the estimated signal $\hat{z}(\boldsymbol{\nu})$ results in $\mathcal{E}_{\hat{z}}(\boldsymbol{\nu}) = |\Theta(\boldsymbol{\nu})|^2 \mathcal{E}_{z_\epsilon}(\boldsymbol{\nu})$, which from (13b) and (9) becomes (14) in terms of normalized quantities. \square

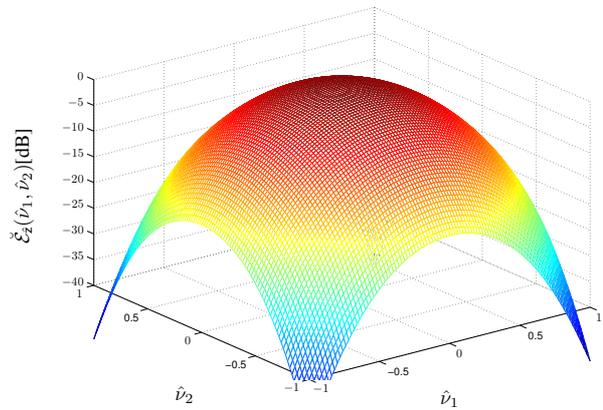
Remark 3: While the use of an ILP interpolator in a PPP causes a white noise floor on the estimated signal ESD [5], the optimal LSI interpolator introduces only a scaling factor point outs in square brackets in (14).

We now introduce two examples.

Example 1 (Bessel-type autocorrelation function): Consider a signal $z(\mathbf{x})$ ($\mathbf{x} \in \mathbb{R}^2$) with a Bessel-type autocorrelation function such that its normalized ESD results in $\check{\mathcal{E}}_z(\check{\boldsymbol{\nu}}) = \frac{\check{\rho}}{\pi} \mathbf{1}_{\mathcal{C}_0}(\check{\boldsymbol{\nu}})$, where \mathcal{C}_0 denotes the 2-dimensional ball centered in the origin with radius 1/2. The corresponding normalized



(a) The case of Bessel-type autocorrelation function



(b) The case of Gaussian autocorrelation function

Fig. 1. Estimated signal normalized ESD in \mathbb{R}^2 for $\check{\rho} = 10^2$ and $\check{D} = 10^2$.

estimated signal ESD according to (14) is depicted in Fig. 1(a).

Example 2 (Gaussian-type autocorrelation function): Consider a signal $z(\mathbf{x})$ ($\mathbf{x} \in \mathbb{R}^2$) with a Gaussian-type autocorrelation function, such that its normalized ESD results in $\check{\mathcal{E}}_z(\check{\nu}) = \frac{4}{\pi} e^{-4|\check{\nu}|^2}$ (i.e., an infinite band signal where the standard deviation is considered as the practical bandwidth per dimension for normalization purpose). The corresponding estimated signal normalized ESD according to (14) is depicted in Fig. 1(b).

Note that, in both the examples, the typical noise floor due to homogeneous Poisson sampling and measurement errors does not arise when using the optimal LSI interpolator (9).

Corollary 2 (NEMSE): When the optimal LSI interpolator in (9) is employed, the NEMSE results in

$$\epsilon_S = 1 - \int_{\mathbb{R}^d} \frac{\check{\mathcal{E}}_z^2(\check{\nu})}{\check{\mathcal{E}}_z(\check{\nu}) + \frac{1}{\check{\rho}} \left(1 + \frac{\check{D}}{\check{\rho}}\right)} d\check{\nu}. \quad (15)$$

Proof: By using the fundamental isometry presented in [4], the NEMSE corresponding to the optimal LSI interpolator results in

$$\epsilon_S = 1 - \frac{1}{E_z} \int_{\mathbb{R}^d} \frac{|\mathcal{E}_{z,z_c}(\nu)|^2}{\mathcal{E}_{z_c}^\dagger(\nu)} d\nu$$

which, from (13a) and (13b), provides (15) in terms of normalized quantities. \square

Remark 4: From (15), the distortion effect can be described by an equivalent diminished normalized intensity

$$\check{\rho}_{\check{D}} \triangleq \frac{\check{\rho}}{1 + \frac{\check{D}}{\check{\rho}}}. \quad (16)$$

Example 3 (NEMSE for ILP ESD Signals): For signals of the example 1, the NEMSE results in

$$\epsilon_S = \left(\frac{1}{\check{\rho}_{\check{D}}}\right) / \left(1 + \frac{1}{\check{\rho}_{\check{D}}}\right)$$

TABLE I
TABLE OF THE MAIN QUANTITIES RELATED TO A LARGE WSN FOR SIGNAL ESTIMATION (u IS THE MEASUREMENT UNIT FOR THE SIGNAL).

Quantity	Significance	Unit
$z(\mathbf{x})$	Signal to be reconstructed	u
\mathbf{x}	Spatial coordinate in \mathbb{R}^d	m
\mathbf{x}_n	Random position of the n -th sample in \mathbb{R}^d	m
\hat{z}_n	n -th random sample of $z(\mathbf{x}) \in \mathbb{C}$ (4)	u
ν	Spatial frequency coordinate in \mathbb{R}^d	m^{-1}
E_z	Energy of the signal	$u^2 m^d$
$\mathcal{E}_z(\nu)$	ESD of $z(\mathbf{x})$	$u^2 m^{2d}$
$ \mathcal{A} $	Cardinality of $z(\mathbf{x})$ domain in \mathbb{R}^d	m^d
B_z	Bandwidth-per-dimension of $z(\mathbf{x})$	m^{-1}
D	Distortion due to sensing errors	u^2
E_M	Overall estimation energy	J
T	Time duration of the sensing	s
σ_M^2	Measurement error variance for each sensor	u^2
W_s	Power consumption for each sensor	W
κ_M	Proportional constant between $W_s T$ and $1/\sigma_M^2$	$J u^2$
c	Capacity-per-volume	$\frac{\text{symbol/ch. use}}{m^d}$
$\check{\cdot}$	Normalized version of a quantity	

Example 4 (NEMSE for Gaussian ESD Signals): For signals of the example 2, the NEMSE results in

$$\epsilon_S = \frac{\pi}{4\check{\rho}_{\check{D}}} \ln \left(1 + \frac{4\check{\rho}_{\check{D}}}{\pi}\right)$$

Fig. 2 shows the NEMSE as a function of the normalized sampling intensity $\check{\rho}$ for different values of the normalized distortion for both examples 3 and 4. It can be noticed that the distortion effects vanish for $\check{\rho}$ approaching the infinity. The different asymptote in the case of Gaussian ESD is due to its infinite signal bandwidth.

IV. ESTIMATION ENERGY CONSTRAINT

Consider the energy spent by the n -th sensor for the estimation of its own $1/\sigma_n^2$ through the hardware-dependent constant κ_M expressed in $[J u^2]$ where u is the measurement unit for the signal (see Table IV). For $\sigma_n^2 = \sigma_M^2$ for all n , the overall estimation energy is $E_M = \kappa_M \frac{\rho |\mathcal{A}|}{\sigma_M^2}$ and the distortion

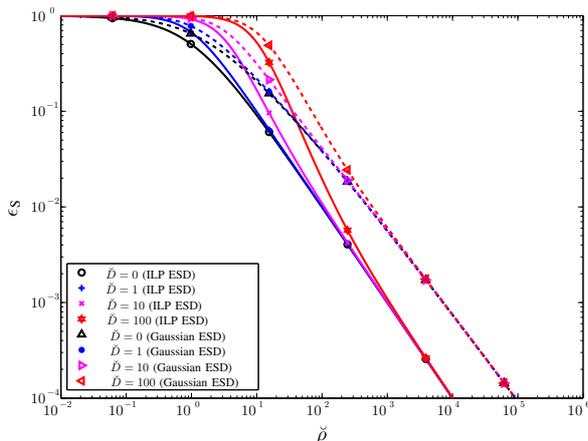


Fig. 2. NEMSE as a function of normalized sampling intensity

results in $D = \rho|\mathcal{A}|\sigma_M^2$. It follows that $\check{D} = \kappa_M \check{\rho}^2 \frac{|\mathcal{A}|^2(2B_z)^d}{E_M E_z}$ which, substituted in (15), provides

$$\epsilon_S = 1 - \int_{\mathbb{R}^d} \frac{\check{\mathcal{E}}_z^2(\check{\nu})}{\check{\mathcal{E}}_z(\check{\nu}) + \frac{1}{\check{\rho}} + \kappa_M \frac{|\mathcal{A}|^2(2B_z)^d}{E_M E_z}} d\check{\nu}. \quad (17)$$

Equation (17) shows that the NEMSE is decreasing with respect to the energy spent for the estimation E_M and increasing with respect to the signal domain Lebesgue measure $|\mathcal{A}|$ and to the signal band Lebesgue measure $(2B_z)^d$. The fact that (17) is also decreasing with respect to the signal energy E_z is simply due to the normalization choice in (8).

Remark 5: Given the overall estimation energy E_M , (17) shows that having more samples (higher $\check{\rho}$) with higher measurement error variance σ_M^2 reduces the NEMSE with respect to the case of less samples with higher precision. This is thanks to the employment of the optimal LSI interpolator (9).

Remark 6: For every finite set of samples, the NEMSE is lower bounded by $\epsilon_S > 1 - \int_{\mathbb{R}^d} \frac{\check{\mathcal{E}}_z^2(\check{\nu})}{\check{\mathcal{E}}_z(\check{\nu}) + \kappa_M \frac{|\mathcal{A}|^2(2B_z)^d}{E_M E_z}} d\check{\nu}$. Note that such a bound is asymptotically approached for both the normalized samples intensity and the normalized distortion approaching the infinity.

V. NETWORK CAPACITY CONSTRAINT

Consider now large WSN with constraints in the capacity of each sensor of sending the samples to the interpolation entity. Here we study the effect of network capacity constraint when a large WSN is employed to reconstruct the signal $z(\mathbf{x})$ (expressed in unit) in $\mathcal{A} \in \mathbb{R}^2$. Assume that the sensor positions are the output of an homogeneous PPP with intensity λ and that each sensor is able to transmit the samples to the entity performing the interpolation with probability q . Thus, the sampling point process results in (1) with $\rho = q\lambda$, that is

$$\check{\rho} = \frac{q\lambda}{(2B_z)^d}. \quad (18)$$

A. Capacity-per-unit volume Constraint

A general and simple way to model the network capability to collect data and forward them to the interpolation entity is to

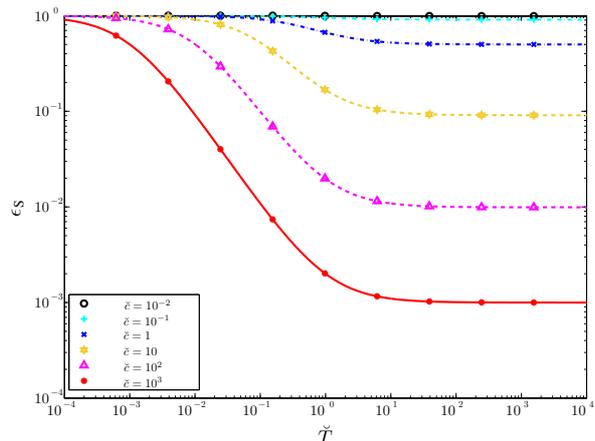


Fig. 3. Large WSN for signal estimation: MSE as a function of normalized capacity and lifetime

assume the WSN can guarantee a certain capacity-per-volume c . Such a value is a function of network bandwidth and protocols (MAC, routing, physical layer, etc.³). For homogeneous Poisson distribution of the sensors positions, the capacity of the channel between the n -th sensor and the interpolator for large WSN is

$$C_n = \frac{C}{|\mathbf{\Pi}_{\mathcal{A}}|} \approx \frac{c|\mathcal{A}|}{\mathbb{E}\{|\mathbf{\Pi}_{\mathcal{A}}|\}} = \frac{c}{\lambda} \quad (19)$$

where C is the overall capacity in [symbols/channel use] and $|\cdot|$ denotes the cardinality. If the channel between the n -th sensor and the interpolator is modeled as an erasure channel, it results

$$C_n = 1 - \epsilon \quad (20)$$

where ϵ is the erasure probability, which is considered equal for all sensors. From (19) and (20) it follows that the sample availability can be written as

$$q \triangleq 1 - \epsilon = C_n \approx \frac{c}{\lambda}. \quad (21)$$

Since $0 \leq C \leq 1$ and $|\mathbf{\Pi}_{\mathcal{A}}| \geq 1$ (for each PPP realization, a WSN is obviously constituted by at least one sensor), it is $0 \leq q \leq 1$.

B. Sensor Lifetime Constraint

Consider all sensors have the same power consumption W_s such that the measurement error variance results in

$$\sigma_M^2 = \frac{\kappa_M}{W_s T}, \quad \forall n \quad (22)$$

where T is the estimation process duration in seconds. By substituting (22) in (5) we obtain $D = \rho|\mathcal{A}|\frac{\kappa_M}{W_s T}$, thus

$$\frac{\check{D}}{\check{\rho}} = \frac{\kappa_M|\mathcal{A}|}{E_z W_s T}. \quad (23)$$

³For the impact of fading and interference see, e.g., [25] and [26].

C. NEMSE for a large WSN

By substituting (21) in (18) we obtain

$$\check{\rho} \approx \frac{c}{(2B_z)^d} \quad (24)$$

that highlights how in a large WSN, the effectively available samples intensity depends on the capacity-per-volume (and no more on the sensors intensity). From (15), (23), and (24), we obtain

$$\epsilon_S = 1 - \int_{\mathbb{R}^d} \frac{\check{\xi}_z^2(\check{\nu})}{\check{\xi}_z(\check{\nu}) + \frac{1}{\check{c}} \left(1 + \frac{1}{\check{T}}\right)} d\check{\nu} \quad (25)$$

where $\check{c} \triangleq \frac{c}{(2B_z)^d}$ and $\check{T} \triangleq \frac{E_z W_c T}{\kappa_M |A|}$ are two fundamental parameters for the network capacity and the sensors battery lifetime, respectively.

Remark 7: If the signal is rigorously band-limited, from (25) and for large \check{c} it is

$$\epsilon_S = \frac{1}{\check{c}} \left(1 + \frac{1}{\check{T}}\right) + o\left(\frac{1}{\check{c}}\right). \quad (26)$$

Example 5: In the case of Bessel-type autocorrelation function for the signal, it results $\epsilon_S = \frac{1}{\check{c}} \left(1 + \frac{1}{\check{T}}\right) / \left[1 + \frac{1}{\check{c}} \left(1 + \frac{1}{\check{T}}\right)\right]$. Fig. 3 shows the NEMSE as a function of the normalized estimation time for different values of normalized capacity. It can be seen the capacity-limited region for large \check{T} , corresponding to the horizontal asymptotes, and the energy-limited region for low \check{T} .

Remark 8: For infinite normalized estimation time, the asymptotical MSE is given by

$$\epsilon_S^{(\infty)} \triangleq \lim_{\check{T} \rightarrow +\infty} \epsilon_S = 1 - \int_{\mathbb{R}^d} \frac{\check{\xi}_z^2(\check{\nu})}{\check{\xi}_z(\check{\nu}) + \frac{1}{\check{c}}} d\check{\nu}.$$

VI. CONCLUSION

The estimation of a finite-energy signal from its samples affected by measurement errors and scattered in \mathbb{R}^d according to an homogeneous PPP has been analyzed. The expression of the optimal LSI interpolator in the MSE sense has been derived and verified that such an expression in \mathbb{R}^d includes a result previously known in the literature as special case.

When the optimal interpolator is used, the effect of both the random sampling and the measurement errors on the estimated signal ESD is an attenuation of the original signal ESD instead of a noise floor as for the case of ILP interpolator. Moreover, the effect of the distortion due to measurement errors on the NEMSE is shown to be equivalent to that of a reduction of samples intensity, which can be compensated by increasing the number of nodes inside the sampling area.

If a constraint in the overall estimation energy is imposed, we verified that an increasing number of sensors leads to a decreasing NEMSE in spite of the corresponding increasing measurement error for each sensor. For the case when the energy constraint is imposed on each sensor due to the battery lifetime limitation, as usual in the large WSN scenario, we derived a simple but significant expression for the NEMSE as a function of the estimation time and the capacity-per-volume.

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