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Improved recovery of carboxylic acids using sequential cationic-anionic adsorption steps: A highly competitive ion-equilibrium model

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1	Improved recovery of carboxylic	acids using sequential cationic-			
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## 1 ABSTRACT

2	A strong cationic resin (Lewatit-S2568H) was used to pre-treat four actual broths rich in carboxylic acids
3	(CAs) to obtain free Na <sup>+</sup> streams (final pH 1.5-2.4). Thereafter, three weak anionic resins (AnRes) were
4	compared for the recovery of CAs by performing multicomponent batch adsorption tests using one of the
5	pre-treated broths. Subsequently, further multicomponent adsorption tests were performed using the
6	other three broths and the most performant AnRes (Lewatit-A365). This allowed to define adsorption
7	isotherm profiles of CAs, Cl <sup>-</sup> , phosphates and other organic compounds (COD <sub>Other</sub> ) for each broth. Besides
8	confirming anions competition for resin exchange sites, results also evidenced that Na <sup>+</sup> competed with
9	the AnRes exchange sites for binding the CAs, while COD <sub>Other</sub> exerted a negligible competition for CA
10	adsorption. A homogeneous mass action ideal model, that also considers Na <sup>+</sup> competition, was calibrated
11	using the collected data. It shows a very good capability to predict adsorption isotherms despite very
12	dissimilar broths were used.

13

# 14 **KEYWORDS**

15 Volatile fatty acids; Organic fraction of municipal solid waste; Grape pomace; Fruit and vegetable waste;

16 Ion exchange resin; Agro-industrial by-product valorisation

17

#### 18 **ABBREVIATIONS**

- 19 AnRes anionic resins
- 20 CAs carboxylic acids
- 21 CatRes cationic resin
- 22 COD chemical oxygen demand
- $23 \qquad \mathsf{COD}_{\mathsf{CAs}}\,\mathsf{COD}\,\mathsf{related}\,\mathsf{to}\,\mathsf{the}\,\mathsf{CAs}\,\mathsf{content}$
- 24  $COD_{CI} COD$  related to  $CI^{-}$  content
- 25 COD<sub>Meas</sub> COD measured

- 1 COD<sub>Other</sub> COD related to other organic compounds
- 2 EU European Union
- 3 FVWs fruit-and-vegetable by-products
- 4 GP grape pomace
- 5 ISE ion-selective electrodes
- 6 PO<sub>4</sub><sup>x-</sup> phosphates, all species
- 7 PHAs polyhydroxyalkanoates
- 8 UBWs urban biowaste
- 9

# 10 **1. INTRODUCTION**

The demand for added value chemicals on the one hand and the need to manage and valorise wastes or by-products on the other hand, are two of the most prominent concerns worldwide about circular economy. In such a framework, stands the chance of coupling organic matter valorisation with the biotechnological production of carboxylic acids (CAs). In fact, CAs can be produced by a simple and economic anaerobic acidogenic fermentation process carried out by mixed microbial cultures. Among the numerous applications, CAs can be employed as precursors of valuable molecules such as esters, ketones and polyhydroxyalkanoates (PHAs), among others [1,2].

In this context, urban biowaste (UBWs) valorisation has been recently studied by Majone and co-workers for instance [3]. The proposed valorisation scheme includes the anaerobic fermentation of concentrated sewage sludge and the organic fraction of municipal solid waste. CAs were then used as substrate to produce PHAs by employing a mixed microbial culture system [4]. The parallel esterification of part of the produced CAs has been explored alongside since it would allow obtaining further added value products which in turn can also be used for PHAs extraction and purification. To this end, CAs must be separated from the aqueous fermentation broth before esterification: being water a by-product of esterification reaction, CA recovery in an organic solvent (e.g. ethanol) would move the esterification equilibrium to the
products, this resulting in enhanced reaction yields [5].

Anion exchange resins can serve for the selective adsorption of CAs from wastewaters or from 3 fermentation broths [6-8]. Rodriguez et al. reported an innovative desorption technology but using a 4 5 strong anionic resin, which has low exchange capacity, thus limiting final CA concentration in the desorbed stream. Weak anionic resins, with high exchange capacity, were employed in the other two 6 7 works. Uslu et al. proved the potentiality of the weak anionic resin by utilizing laboratory prepared CA 8 solutions, hence results need to be validated by using actual CA-rich streams. Interestingly, Rebecchi et al. described CA recovery from actual broth obtained from the acidogenic fermentation of grape pomace 9 10 (GP). However, under the explored most favourable pH (i.e. promoting resin functional groups 11 protonation), the overall CA adsorption yield was low (about 30%), this compromising the process economic feasibility. As a whole, the proposed strategy is affected by the fact that CA-rich broths are 12 13 usually close to neutral pH (5<pH<7), this meaning that each mole of carboxylate is paired with a cation 14 (e.g. Na<sup>+</sup>) arising from the base (e.g. NaOH) added during the fermentation to adjust the pH level. Thus, carboxylates are less available for ionic adsorption due to the formation of ion pairs in the solution (R-15 COO<sup>-</sup> Na<sup>+</sup>) [9]. This is in accordance with the fact that a NaOH solution is usually applied for desorbing the 16 17 anions from the resin in an almost stoichiometric relation [8]. Overall, the recovery of CAs using anionic 18 resins depends on the occurrence and interference of all inorganic ions, which must be also considered 19 for modelling adsorption isotherms using mass-action law. Among anions, phosphates (all species, here on called  $PO_4^{x-}$ ) and chloride (Cl<sup>-</sup>) are competitors for exchange sites on the anion resin [10,11]. 20 The present work is aimed to maximize CA extraction from actual fermentation broths by coupling a 21 22 cation adsorption step with a consecutive anion adsorption stage, as shown in the graphical abstract. This 23 would allow to remove Na<sup>+</sup>, rendering R-COO<sup>-</sup> free and available for anion resin exchange. Gonzalez *et al.* 24 applied the same strategy but for the adsorption of inorganic anions rather than the main product (lactic

acid) [12] and a related patent describing the strategy was registered later on [13]. More recently, a 1 similar approach was reported for the adsorption and recovery of D-lactic acid from an actual 2 fermentation broth based on dried distiller's grains with soluble hydrolysates [14]. However, none of 3 these works reported overall ion equilibrium models. Zaini et al [14] just applied pure empirical models 4 5 (having poor extrapolation ability), while the homogeneous ideal model assessed in the previously mentioned work using GP [8] does not include the competitive effects of Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and Na<sup>+</sup> already 6 occurring in the actual broth, while only the added Cl<sup>-</sup>/Na<sup>+</sup> (HCl/NaOH) and carbonates (unlikely present 7 8 at the reported concentrations) were considered as interferents. On the other hand, many authors have developed ideal and non-ideal homogeneous mass action models, but few of them were 9 10 validated/calibrated using actual process streams [15,16]. Indeed, a simplified homogeneous model 11 reflecting anions and cations competitions and validated using actual CA-rich broths has never been 12 proposed. 13 With all this in mind, the specific aims of this study were: a) to verify the exchange capacities of cationic 14 (for Na<sup>+</sup> and NH<sub>4</sub><sup>+</sup>) and anionic (for CAs, Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup>) resins; b) to pre-treat four actual broths using the 15 cationic resin and evaluate the step performance; c) to select the most suitable anionic resin among the 16 tested ones containing tertiary amine or bifunctional groups; d) to verify the feasibility of applying the 17 simple desorption procedure reported elsewhere [8]; e) to propose a simplified ionic equilibrium model 18 (mass action) capable of predicting the total CA concentrations (in the resin and in the liquid phases) by measuring uniquely the pH at the equilibrium; and f) to calibrate and asses the model by using four 19 20 diverse actual CA-rich broths with significantly different ions and matrix compositions, deriving from the acidogenic fermentation of two diverse UBWs (UBW1 and UBW2), fruit-and-vegetable by-products 21 22 (FVWs) and a red grape pomace (GP).

The avant-garde employment of four very dissimilar actual broths allowed progressing beyond the state of art by (1) demonstrating the effectiveness of a cation-exchange pre-treatment which would enable to recover almost 100% of the CAs occurring in broths by using an anionic resin with high exchange capacity,
(2) developing a semi empirical homogeneous mass action ideal model that considers the interferences of
the inorganic ions (Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and Na<sup>+</sup> occurring in the broths) on CA adsorption, (3) demonstrating that
interfering effects due to the occurrence of other non-identified organic compounds are negligible, and
(4) highlighting that Na<sup>+</sup> competition rather than resin's functional-group protonation is a major concern
for recovering CAs from actual broths using anionic resins.

7

#### 8 2. MATERIAL AND METHODS

# 9 2.1. Resins, reagents and acidogenic effluents

The strong cationic resin (CatRes) Lewatit-S2568H, with sulfonic acid functional group in the H<sup>+</sup> form, was 10 used to pre-treat the four actual broths. To evaluate the role of the solid phase in CA recovery, three 11 anionic resins (AnRes) were preliminary selected according to their nominal exchange capacity and a 12 previous experience [8], namely (brand, functional groups, nominal exchange capacity in eq/L): Amberlyst 13 14 A21 (DoW, tertiary amine, 1.3), Lewatit S4528 (Lanxess, tertiary amine, 1.7) and Lewatit A365 (Lanxess, 15 tertiary and quaternary amines, 3.4). Main chemical-physical characteristics of all resins are reported in Sup. Material Table S1. All Lewatit resins were kindly provided by Lanxess-Italy, while Amberlyst A21 and 16 17 all the required reagents were purchased from Merck. The two fermented UBWs (UBWs1 and UBWs2) used in the study were provided by an external research 18 group in the framework of the ResUrbis EU project [3]. UBWs1 and UBWs2 were generated in different 19 20 batches carried out with a pilot acidogenic fermenter located at the wastewater treatment plant of

- 21 Treviso, thus with similar ions (Na<sup>+</sup>, NH<sub>4</sub><sup>+</sup>, CAs, Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup>) and other organic matter (COD<sub>Other</sub>)
- 22 composition. The FVWs and GP were kindly provided by Biosphere S.R.L and Caviro Extra S.p.A
- 23 companies, respectively. Both by-products were stored at 6 °C for less than 4 days before processing.

6

FVWs and GP were anaerobically fermented in 1 L Pyrex bottles under batch conditions (pH 7, 37 °C, 150 1 rpm) until constant CA concentration was achieved (7-10 days), according to the procedures reported 2 elsewhere [17]. All four actual broths were processed for suspended solids removal according the 3 procedure conducted by the PHA pilot plant described elsewhere [4]; in details, the effluents were 4 5 centrifuged and filtered at 0.2 µm (cellulose acetate syringe filters were used instead of the ceramic module used at pilot scale) before use. In the present work they were stored at 4 °C until use. CA 6 compositions in the actual broths were mainly (on % molar bases): acetic (58-69), propionic (2-8), butyric 7 8 (20-25), valeric (0-5) and hexanoic (1-8) acids. Main chemical features of these target broths are reported in Table 1 (UBWs1-pre, UBWs2-pre, FVWs-pre and GP-pre). 9

10

#### 11 **2.2. Experimental approach**

All resins were conditioned according to the suppliers' procedures. Different sets of batch experiments 12 (20-22 conditions each) were conducted for defining single and multi-component adsorption isotherms 13 14 (25°C and 150 rpm). Each experimental point (20-22 points per isotherm) was accomplished by loading a 15 10 mL glass vial with 0.05 to 1.20 g of resin (dry weight) and 2 mL of liquid (i.e. water solutions or actual broth). Total volumes in each container were accurately measured by weighting the empty vials as well as 16 17 the added amounts of resin and liquids. Isotherms experiments were stopped after 120 min, according to dedicated preliminary single-condition tests executed using online continuous pH measurements in a 10 18 19 mL vial (Sup. Material, Section S2.1). At the end of the isotherm-tests, the liquid was separated by means 20 of a syringe, pH was measured and the concentrations of target analytes at the equilibrium were 21 determined, namely: [NH<sub>4</sub><sup>+</sup>]<sub>Eq</sub>, [Na<sup>+</sup>]<sub>Eq</sub>, total CAs ([CAs]<sub>Eq</sub>), [Cl<sup>-</sup>]<sub>Eq</sub>, [PO<sub>4</sub><sup>x-</sup>]<sub>Eq</sub> and [COD<sub>Other</sub>]<sub>Eq</sub> (calculated as 22 reported in Section 2.5).

23 The adsorbed concentrations for each target chemical (q<sub>n</sub>, mol/g dry resin) were calculated as follows:

7

$$1 \qquad q_n = \frac{(C_0 \cdot V_{Sample} - C_{Eq} \cdot V_{Tot})}{m_{res}} \quad (1)$$

where C<sub>0</sub> and C<sub>Eq</sub> represent the initial and equilibrium liquid concentrations of NH<sub>4</sub><sup>+</sup>, Na<sup>+</sup>, CAs, Cl<sup>-</sup> or PO<sub>4</sub><sup>x-</sup>,
V<sub>Sample</sub> the volume of added broth or lab-prepared solution, V<sub>Tot</sub> the total liquid of the system (i.e. V<sub>Sample</sub>
plus the water already contained in the activated resins), and m<sub>res</sub> is the resin dry mass.

# 5 2.2.1. Resins characterisation

All resins were characterised, in terms of exchange capacity and affinity with target ions, by determining single component adsorption isotherms as mentioned above. NH<sub>4</sub><sup>+</sup> and Na<sup>+</sup> isotherms were defined by using ammonium acetate and sodium acetate water solutions (ca. 0.1 M). For the three AnRes, acetic acid (0.5 M), HCl (0.5 M) and H<sub>3</sub>PO<sub>4</sub> (0.35 M) water solutions were separately used to define CAs, Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup> adsorption isotherms. Langmuir ( $q = q_{max}$ .  $C_{Eq}/(K_s + C_{Eq})$ ) and Freundlich (q = k.  $C_{Eq}$ <sup>n</sup>) models were used to fit CatRes and AnRes obtained results [18]. Specifically, the linearized form of the equations and the correlation coefficient (R<sup>2</sup>) were used to evaluate the fittings.

#### 13 2.2.2. Actual broth pre-treatments with the cationic resin

In order to remove cations, UBWs1, FVWs and GP actual broths were separately pre-treated with the 14 CatRes Lewatit S2568H by flowing them through a 60 mL syringe packed with 14.5 g of CatRes (dry bases). 15 First portions (ca. 40 mL) of cation-free effluents were discarded as they resulted diluted with the water 16 contained in the activated-CatRes. Importantly, broths' pH diminishes due to cations removal. Thus, the 17 18 following portions were collected until the resulting pH of the accumulated liquid was 1.51-2.50 (Table 1). 19 Then, the CatRes was regenerated by sequentially manually flowing (ca. 1-2 mL/min): (i) 40 mL of deionised water, (ii) 140 mL of HCl 6%, and (iii) 175 mL of deionised water. Subsequently, a new 20 adsorption-desorption cycle was carried out. Each broth required about two cycles for obtaining ca. 350 21 22 mL of treated liquid to be used in the AnRes experiments. However, without carrying out a proper

breakthrough test, the mentioned pre-treatment cycles did not allow calculating the resin exchange
 capacity.

3	Differently, UBWs2 was pre-treated using a pilot scale column (133 cm high and 2.7 cm diameter), packed
4	with the same CatRes (bed height 77 cm). Five adsorption-desorption cycles were carried out, with the
5	adsorption step performed and monitored as breakthrough test. First flowed portions (ca. 600 mL) were
6	discarded as described above, while the consecutive portions were collected until the resulting pH of the
7	accumulated liquid was 1.46. Subsequently, the effluent reservoir was replaced and the adsorption was
8	conducted until AnRes saturation. Total exchange capacities were calculated by material balance. Then,
9	the CatRes was regenerated by sequentially flowing (ca. 34 mL/min): (i) 0.6 L of deionised water, (ii) 2 L of
10	HCl 6%, and (iii) 2.5 L of deionised water. Pilot column pre-treatment allowed to obtain an effluent
11	portion almost completely deprived of cations (having the lowest pH tested in this work for CA extraction)
12	and with the same concentration of CAs originally present in UBWs2 ( <b>Table 1</b> ).
13	2.2.3. Selection of the most performant AnRes and desorption verification
13 14	To evaluate the performances of the three AnRes when actual complex solutions are used,
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14 15	To evaluate the performances of the three AnRes when actual complex solutions are used, multicomponent adsorption tests were carried out using the pre-treated UBWs1. Hence, three sets of
14 15 16	To evaluate the performances of the three AnRes when actual complex solutions are used, multicomponent adsorption tests were carried out using the pre-treated UBWs1. Hence, three sets of experiments (22 conditions each) were done to define four adsorption isotherms per AnRes, namely: CAs,
14 15 16 17	To evaluate the performances of the three AnRes when actual complex solutions are used, multicomponent adsorption tests were carried out using the pre-treated UBWs1. Hence, three sets of experiments (22 conditions each) were done to define four adsorption isotherms per AnRes, namely: CAs, Cl <sup>-</sup> , PO <sub>4</sub> <sup>X-</sup> and COD <sub>Other</sub> . The 22 experimental points were accomplished according to the general approach
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9

After the adsorption test, the vials containing the corresponding AnRes portions with the adsorbed
 compounds were used to verify the feasibility of applying a simple desorption step, as reported elsewhere
 [8]. Hence, vials were weighted before and after the addition of NaOH-ethanol solution (3 mL, 0.5 M) to
 accurately determine the total liquid volume (left liquid plus the added desorbing solution, V<sub>Des</sub>). After
 120 min (at 25°C and 150 rpm), the liquid was separated and analysed for determining desorbed analytes
 concentrations ([CAs]<sub>Des</sub>, [Cl<sup>-</sup>]<sub>Des</sub>, [PO4<sup>x-</sup>]<sub>Des</sub>, [COD<sub>Other</sub>]<sub>Des</sub>). Total desorbed moles were calculated as
 *C<sub>Des</sub>*. *V<sub>Des</sub>*.

8 2.2.4. Testing the selected AnRes with different actual broths: matrix influence and calibration of a simple
9 ion equilibrium model

Once the AnRes was selected (Section 2.2.3), the other three pre-treated broths (UBWs2, FVWs and GP) were used to define related multicomponent adsorption isotherms by the same experimental procedure described above. This allowed both to *a*) evaluate the resin performance in the treatment of different matrices with different ions mixtures, and *b*) to calibrate a general simplified ion equilibrium model.

14

#### 15 2.3. CA adsorption prediction in multicomponent tests based on single component isotherms

16 Neither the amines (functional group) dissociation nor the other organic compounds (COD<sub>Other</sub>) occurring 17 in actual broths are as significant as inorganic ions on CA adsorption interference. To confirm this hypothesis, CA adsorption isotherms were initially predicted in all the multicomponent adsorption tests 18 (22 experimental conditions each) conducted with actual broths by considering only: (i) the previous 19 20 obtained Langmuir/Freundlich isotherms for single components tests (acetic acid, Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup>, Section 21 **2.2.1**) and (*ii*) the inorganic ions occurring in the actual broths (Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and Na<sup>+</sup>). Thus, 22 expected isotherms points ([CAs]<sub>Eq</sub>"; q<sub>Cas</sub>") were calculated for each multicomponent adsorption tests by following 22 the next rationale (for each experimental point): 23

- 1 1- the overall anion adsorption isotherms ( $q_{Tot anions} vs$  [Tot anions]<sub>Eq</sub>) coincides with the same CA 2 isotherm equations (Langmuir or Freundlich, depending on the AnRes) obtained previously using 3 acetic acid prepared solution (**Section 2.2.1**). Thus, an expected equilibrium concentration of 4 overall anions ([Tot anions]<sub>Eq</sub>, comprising Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and CAs) can be calculated from a presumed 5  $q_{Tot anions}$  and the corresponding isotherm formula, e.g. [ $Tot_anions$ ]<sub>Eq</sub> = ( $q_{tot_anions}/k$ )<sup>1/n</sup> in 6 the case of the Freundlich equation;
- the moles of Na<sup>+</sup> remained in the effluent after CatRes pre-treatment get paired with the
   corresponding molar amount of CAs and prevents CA adsorption. Such concentration can be
   calculated using a charge balance (Eq. S 6 in Sup. Material-Section S3, calculate Na<sup>+</sup><sub>Tot</sub>);
- 10 3- the [Tot\_anions]<sub>Eq</sub> can also be calculated from Eq. 1 (Section 2.2.1) by using  $C_0 =$

11 
$$[Tot\_anions]_0 - Na_{Tot}^+$$
 and the previous presumed  $q_{Tot\_anions}$ ;

- 4- a true [Tot\_anions]<sub>Eq</sub> value can be estimated (as well as q<sub>Tot\_anions</sub>) through iterative minimization
- 13 of the error between both calculated [Tot\_anions]<sub>Eq</sub> by changing the presumed q<sub>Tot\_anions</sub>;
- 14 5- considering the stronger affinities of inorganic anions towards the AnRes active sites, the
- adsorption of CAs takes place (those which are Na<sup>+</sup>-free) on vacant exchange sites. Thus,
- 16 considering total Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup> adsorption ( $q_{Cl} = [Cl]_0 \cdot \frac{V_{Sample}}{m_{res}}$  and  $q_{PO_4}^{x-} = [PO_4^{x-}]_0 \cdot \frac{V_{Sample}}{m_{res}}$ ),
- 17 the adsorbed CAs can be calculated as  $q_{CAS}'' = q_{Tot\_anions} q_{Cl} q_{PO_A}x$ ; and
- 18 6-  $[CAs]_{Eq}$ " can be calculated using Eq. 1 and the obtained  $q_{CAs}$ ".

# 19 **2.4. Ions equilibriums model**

- 20 A homogeneous mass action ideal model (type 1) was proposed based on the following equilibrium
- reactions (equations 2-12), the charge balance (13) and the analytes concentration balances (14-18):

22 
$$K_a^{Res} = [ResHOH] \cdot [H_3O^+] / [ResH^+]$$
 (2)

23  $K_a^{CAs} = [RCOO^-] \cdot [H_3O^+] / [RCOOH]$  (3)

1 
$$K_{a1}^{PO_4} = [H_2 PO_4^{-}] \cdot [H_3 O^+] / [H_3 PO_4]$$
 (4)

2 
$$K_{a2}^{PO_4} = [HPO_4^{2-}] \cdot [H_3O^+] / [H_2PO_4^{-}]$$
 (5)

- 3  $K_a^{Cl^-} = [Cl^-] \cdot [H_3 O^+] / [HCl]$  (6)
- 4  $K_a^{Na^+} = [NaOH] \cdot [H_3O^+] / [Na^+]$  (7)
- 5  $K_{Res}^{Cl^{-}} = [ResHCl]/([ResH^{+}].[Cl^{-}])$  (8)
- 6  $K_{Res1}^{PO_4^{X^-}} = [ResHH_2PO_4]/([ResH^+].[H_2PO_4^-])$  (9)

7 
$$K_{Res2}^{PO_4^{X^-}} = [(ResH)_2 HPO_4] / ([ResH^+]^2. [HPO_4^{2^-}])$$
 (10)

8  $K_{Res}^{CAs} = [ResHRCOO]/([ResH^+].[RCOO^-])$  (11)

9 
$$K_{Na^+}^{CAs} = [NaRCOO]/([Na^+].[RCOO^-])$$
 (12)

10 
$$[RCOO^{-}] + [OH^{-}] + [H_2PO_4^{-}] + [HPO_4^{2^{-}}] \cdot 2 + [Cl^{-}] = [NH_4^{+}] + [Na^{+}] + [H_3O^{+}]$$
 (13)

11 
$$Res_{Tot} = [ResH^+] + [ResHOH] + [ResHCl] + [ResHH_2PO_4] + 2. [(ResH)_2HPO_4] + [ResHRCOO]$$

12 (14)

13 
$$CAs_{Tot} = [RCOOH] + [RCOO^{-}] + [ResHRCOO] + [NaRCOO]$$
 (15)

14 
$$Cl_{Tot} = [HCl] + [Cl^{-}] + [ResHCl]$$
 (16)

15 
$$PO_4^{x-}_{Tot} = [H_3PO_4] + [H_2PO_4^{-}] + [HPO_4^{2-}] + [ResHH_2PO_4] + [(ResH)_2HPO_4]$$
 (17)

16 
$$Na^{+}_{Tot} = [Na^{+}] + [NaOH] + [NaRCOO]$$
 (18)

17 All concentrations are referred to the total volume of liquid (V<sub>Tot</sub>), including the free deprotonated

18 ([ResHOH]), free protonated ([ResH<sup>+</sup>]) and total concentration (Res<sub>Tot</sub>) of the resin, the latter being

19 calculated as the added quantity of dry resin multiplied by a constant *Q* (moles of active sites per gram of

- 20 dry resin) and divided by the final volume (V<sub>Tot</sub>). The proposed homogenous mass action model [16]
- 21 reflects the following simplifications: (1) tertiary and quaternary amines functional groups of the AnRes
- were considered to have the same average dissociation constant; (2) all CAs (acetic, propionic, butyric,
- valeric, hexanoic acids; with an average  $K_a$  of 1.48 x 10<sup>-5</sup> ± 1.68 x 10<sup>-6</sup>) have the same dissociation

constant; (3) adsorption of sulphates (occurring in traces in the employed broths) was neglected; (4) the
molar amount of Na<sup>+</sup> still available after the pre-treatment with the CatRes can get paired with the CAs
since Na<sup>+</sup> have a higher affinity with carboxylates than the AnRes' exchange sites; (5) the low molar
amount of Na<sup>+</sup> was not sufficient to consider associations equilibrium reactions for the inorganic anions.
Moreover, the mass action model does not consider the calculation of activity coefficients, nor for the
liquid phase neither for the solid phase. Instead, these coefficients are included in the resulting
equilibrium constants obtained from the calibration.

From all equations (2-18), six final equalities with pH as the only independent variable were used to state
a simultaneous equation system, namely: the charge balance and five equations with Langmuir-formula
format, one for each of the four anions adsorbed to the resin and one for the CAs paired with the Na<sup>+</sup>.
Detailed information on these equations were reported in Sup. Material-Section S3.

12 Importantly, in the case of phosphates, both adsorbed species were added ( $[(ResH)_2HPO_4] +$ 

13  $[ResHH_2PO_4]$ ) and considered together for the definition of a total phosphates adsorption isotherm

14 
$$(q_{PO_4}^{x-} vs. [PO_4^{x-}]_{Eq}).$$

15 As mentioned, the model was calibrated by using four different actual CA-rich broths, i.e. by determining a common value for the constants Q,  $K_a^{Res}$ ,  $K_a^{CAs}$ ,  $K_{a1}^{PO_4^{X^-}}$ ,  $K_{a2}^{PO_4^{X^-}}$ ,  $K_a^{Na^+}$ ,  $K_w$ ,  $K_{Res}^{Cl^-}$ ,  $K_{Res1}^{PO_4^{X^-}}$ , 16  $K_{Res2}^{PO_4^{X-}}$ ,  $K_{Res}^{CAs}$  and  $K_{Na^+}^{CAs}$  that could describe simultaneously the adsorption on AnRes of target anions 17 occurring in all four effluents. To this aim, a simple MATLAB algorithm was produced. Briefly, it uses the 18 19 built-in function patternsearch to propose a set of guessing values for the constants used in the six pHdependent equations used in each effluent contemporaneously. Thereafter, the built-in function fmincon 20 21 is used to solve the simultaneous equations at each experimental point of the isotherms with constrains expressed as  $[ResHCl] \leq Cl_{Tot}$ ,  $[ResHRCOO] + [NaRCOO] \leq CAs_{Tot}$  and  $[ResHH_2PO_4] + [NaRCOO] \leq CAs_{Tot}$ 22  $[(ResH)_2HPO_4] \le PO_4^{x-}_{Tot}$ . As a result, modelled bond and free analytes concentrations ([ResHCl], 23

 $[ResHH_2PO_4]$ ,  $[(ResH)_2HPO_4]$ , [ResHRCOO], [NaRCOO],  $[Cl]_{eq}$ ,  $[PO_4^{x-}]_{eq}$ ,  $[CAs]_{eq}$ ) are estimated 1 for each point of the isotherms by using only the corresponding measured value of pH at equilibrium. 2 3 Finally, the sum of the weighted square error between the experimental and modelled concentrations is 4 computed as a total of all isotherms for all effluents. This objective function is minimized with the mentioned *patternsearch*. The initial guesses constants values were based on physicochemical known 5 data, namely: resin exchange capacity and affinity-constants observed from the experiments mentioned 6 7 in Sections 2.2.1 and 2.2.3, resin and inorganic ions dissociation constants for diluted systems, and an average CA dissociation constant (mean between all four actual effluent of the composition-weighted-8 9 average  $K_a$ ). The quality of the best fit for each effluent-isotherm and for each compound was evaluated by means of the correlation coefficient  $R^2 = 1 - \left[\sum_{i=1}^{22} (C_{Exp,i} - C_{Model,i})^2\right] / \left[\sum_{i=1}^{22} (C_{Exp,i} - C_{Exp,avg})^2\right]$ 10 and by the residuals  $R\% = 100. (C_{Exp,i} - C_{Model,i})/C_{Exp,i}$ , where  $C_{Exp,i}$ ,  $C_{Model,i}$ ,  $C_{Exp, Avg}$  are the 11 experimental, modelled and average experimental concentrations values of each compound (Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> or 12 13 CAs), respectively.

# 14 2.5. Analytical procedures

CAs, PO<sub>4</sub><sup>x-</sup> and sulphates concentrations were determined by HPLC-RID using the same procedure
reported elsewhere [17]. NH<sub>4</sub><sup>+</sup> and Cl<sup>-</sup> concentrations were determined using two combined ion-selective
electrodes (ISE) (Crison), while a conventional laboratory probe (XS POLYMER PLAST S7) was used for
measuring pH. Resins water content was determined by using a moisture analyser (MB35-OHAUS), which
was operated at 105 °C until constant weight was obtained.

20 Chemical oxygen demand (COD<sub>Meas</sub>) was determined by using a colorimetric commercial kit (AQUALYTIC

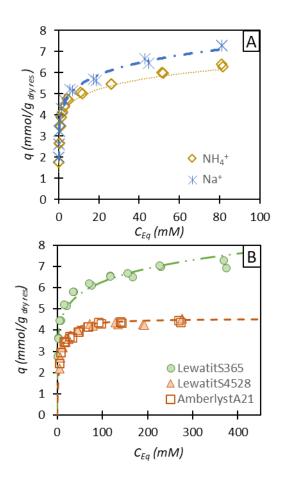
- 21 Vario MR). This parameter determines the overall concentration of all oxidizable compounds, including
- 22 the CAs, Cl<sup>-</sup> and other organic molecules (COD<sub>Other</sub>) occurring in each sample. To determine the COD<sub>Other</sub>,
- 23 the equivalent COD contributions of CAs and Cl<sup>-</sup> were calculated by considering the stoichiometric

oxidation of both (COD<sub>CAs</sub> and COD<sub>Cl</sub>, respectively). Thus, the concentration of the matrix compounds was calculated as  $COD_{Other} = COD_{Meas} - COD_{CAs} - COD_{Cl}$ . Na<sup>+</sup> was determined from the charge balance equation (Sup. Material-Section S3, Eq. S6).

#### 4 **3. RESULTS AND DISCUSSION**

#### 5 3.1. Resin characterization

Single component adsorption isotherms were defined for characterizing the CatRes to be used in the pre-6 treatment of the four actual broths. Fig. 1 A shows the experimental results fitted with Freundlich model 7 for the cases of sodium acetate (k = 3.97, n = 0.13,  $R^2 = 0.95$ ) and ammonium acetate (k = 3.55, n =8  $0.141, R^2 = 0.94$ ). Interestingly, Langmuir model resulted less performant in both cases (Sup. Material 9 Fig. S2), but the obtained CatRes maximal exchange capacities for  $NH_4^+$  ( $q_{max} = 5.30 \text{ mmol/g}_{dry res}$ ) and  $Na^+$ 10  $(q_{max} = 5.35 \text{ mmol/g}_{dry res})$  were in accordance with the value estimated using the datasheet (5.4 11 mmol/g<sub>dry res</sub>). Notably, the effectiveness of using the charge balance equation (Eq. S6 in Sup. Material) to 12 determine [Na<sup>+</sup>]<sub>Eq</sub> was indirectly assessed and verified when carrying out the NH<sub>4</sub><sup>+</sup> adsorption isotherm 13 14 test. Indeed, the comparison between the ISE measured values of  $[NH_4^+]_{Eq}$  (Section 2.5) with those 15 obtained by using Eq. S6 (and the corresponding pH values at the equilibrium) showed high correspondence in a parity plot (Sup. Material Section S2.3, Fig. S3). 16



**Fig. 1:** Resin characterization: Na<sup>+</sup> and NH<sub>4</sub><sup>+</sup> adsorption isotherms with the CatRes Lewatit S2568H (A) and acetic acid adsorption with the three AnRes (B). For the isotherm profiles, markers represent the experimental results whereas lines refer to fittings of Langmuir or Freundlich isotherms. A single modelled curve is presented for acetic acid adsorption onto both tertiary amine resins.

- 1 As for the AnRes, Fig. 1 B shows examples of acetic acid adsorption isotherms for the three AnRes tested
- 2 in this work. Lewatit A365 isotherms have Freundlich behaviours (shown in Fig. 1 B), as typical for
- bifunctional/heterogenous resins [18], with the highest affinity for Cl<sup>-</sup> (k = 7.59, n = 0.08,  $R^2 = 0.93$ ),

followed by PO<sub>4<sup>x-</sup></sub> (k = 5.79, n = 0.13,  $R^2 = 0.89$ ) and CAs (k = 3.51, n = 0.126,  $R^2 = 0.94$ ). 1

2 Conversely, both resins with tertiary amine have extremely similar Langmuir behaviours, e.g. isotherms parameter for CAs were  $q_{CAs,max} = 4.54 \text{ mmol}/g_{drv res}$ ,  $K_s = 4.74 \text{ mM}$ ,  $R^2 = 0.90$ , and the same order 3 4 of affinities previously found for the bifunctional resin was observed ( $Cl^- > PO_4^{x-} > CAs$ ). The obtained results confirm the higher exchange capacity of the bifunctional resin over the others AnRes: Lewatit 5 A365 has a remarkable 1.56 folds increase of the CA adsorption capacity of Lewatit S4528 or Amberlyst 6 7 A21, the last one previously proposed by a study addressed to the same purpose [8]. Furthermore, coupling the adsorption of nutrients such as NH<sub>4</sub><sup>+</sup> and PO<sub>4</sub><sup>x-</sup> to CA extraction is of interest in 8 9 the perspective of maximizing resource recovery from waste and by-products; this approach might represent an improvement towards the entire process sustainability [19,20]. The results obtained with 10 the CatRes reveal that Na<sup>+</sup> and NH<sub>4</sub><sup>+</sup> have similar affinities with the solid phase, while the results attained 11 12 with the anionic resins suggest that single anions recovery could be accomplished by splitting the AnRes step in three dedicated columns addressed to the extraction of Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and CAs, respectively. 13 3.2. Actual broth pre-treatments with cationic resin 14 The feasibility of recovering CAs by employing sequentially cationic and anionic resins was verified with 15 four actual effluents. To this aim, the UBWs1, UBWs2, FVWs and GP broths were treated with the CatRes

as described in Section 2.2.2. While the contents of CAs, inorganic anions and total COD remained almost 17

16

18 unaltered (ca. 90%), the pH dropped since cations were removed and CAs remained as acids (Table 1).

Moderate to low adsorption of COD<sub>Other</sub> by the CatRes was observed in all pre-treatments (< 50%), in 19

accordance with previously reported statements for the treatment of corn stover hydrolysate with 20

- 21 another strong CatRes [21]. The pre-treatment of UBWs1, FVWs and GP broths for obtaining cation-free
- 22 effluents required the implementation of seven adsorption-desorption cycles in 60 mL packed syringe.
- 23 Although those cycles were not conducted as breakthrough tests, the CatRes reusability was preliminary

assessed when treating the UBWs2 at pilot scale by performing five breakthrough test and desorption
cycles (data not shown). The obtained exchange capacity repeatability and low deviations (5.10 ± 0.53
mmol/g<sub>dry res</sub>) can be considered a preliminary promising result which must be confirmed by applying
several cycles at pilot scale.
The effectiveness of the pre-treatments paves the way for future investigation about cation adsorption
isotherms using actual effluents in order to model also this step using ion equilibrium and to better refine

7 the overall two stage process. However, the present work was focused on the recovery of the CAs, which

8 were demonstrated to be inert to the CatRes step.

9 Table 1: CA-rich effluents features before (pre) and after (post) their treatment with the CatRes Lewatit
 S2568H

Effluent	COD <sub>Meas</sub> (mM O <sub>2</sub> ) <sup>a</sup>	<b>CAs</b> (mM) ª	<b>Cl⁻</b> (mM)ª	<b>PO₄×-</b> (mM) ª	COD <sub>Other</sub> (mM O <sub>2</sub> ) <sup>d</sup>	pH ª	<b>NH₄⁺</b> (mM) ª	<b>Na⁺</b> (mM) <sup>b, d</sup>	μ <sup>c</sup> (mM) <sup>d</sup>
UBWs1-pre	1509 ± 26	289 ± 10	44.5 ± 2.1	11.0 ± 0.8	576 ± 50	5.75 ± 0.01	38.36 ± 2.91	279.92 ± 14.92	318.54 + 14.95
UBWs1-post	1350 ± 24	276 ± 7	41.1 ± 3.1	9.5 ± 0.4	398 ± 50	1.51 ± 0.01	0.96 ± 0.29	11.39 ± 3.47	27.79 ± 3.47
UBWs2-pre	2078 ± 200	348 ± 2	44.0 ± 2.8	5.8 ± 0.2	683 ± 206	5.75 ± 0.01	34.78 ± 2.06	323.61 ± 6.88	358.58 ± 6.89
UBWs2-post	1598 ± 14	345 ± 3	36.0 ± 5.6	5.8 ± 0.5	372 ± 24	1.46 ± 0.01	0.23 ± 0.09	2.30 ± 5.78	19.86 ± 5.78
FVWs- <i>pre</i>	1256 ± 39	283 ± 1	23.4 ± 1.4	0.1 ± 0.1	162 ± 45	7.00 ± 0.01	37.93 ± 1.91	266.76 ± 4.43	304.50 ± 4.47
FVWs- <i>post</i>	1261 ± 40	275 ± 3	21.7 ± 2.8	0.1 ± 0.1	259 ± 50	1.80± 0.01	0.72 ± 0.23	5.44 ± 3.07	14.08 ± 3.07
GP-pre	977 ± 63	230 ± 8	26.0 ± 0.4	8.1 ± 0.3	159 ± 90	7.05 ± 0.01	5.44 ± 0.52	313.31 ± 9.30	322.17 ± 9.42
GP-post	962 ± 48	221 ± 4	24.3 ± 1.9	8.3 ± 0.4	191 ± 59	2.44 ± 0.01	0.83 ± 0.11	26.41 ± 2.30	29.09 ± 2.30

11 <sup>a</sup> errors from analytical determination; <sup>b</sup> calculated by charge balance (Supplementary material Eq. S 6), by using the concentration of CAs, Cl<sup>-</sup>,

12 PO<sub>4<sup>x-</sup></sub> and NH<sub>4<sup>+</sup></sub> previously determined; <sup>c</sup> approximate ionic strength calculated as reported elsewhere [22] by considering CAs (i.e. R-COO<sup>-</sup>), Cl<sup>-</sup>

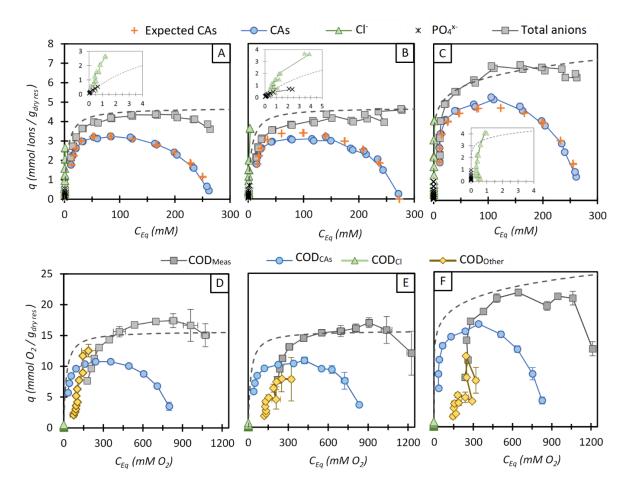
13 ,  $\mathsf{PO}_4{}^{x_*},\mathsf{NH}_4{}^+$  and  $\mathsf{Na}^+;{}^d$  errors calculated by error propagation.

# 14 3.3. Selection of the most performant AnRes and desorption verification

15 For comparing the three AnRes performances, multicomponent adsorption tests were carried out using

16 the pre-treated UBWs1. Fig. 2 A, B and C show the competitive adsorption of CAs, Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> for each

17 AnRes. Complementarily, Fig. 2 D, E and F expose (for the same batch tests) the competitive adsorption in



**Fig. 2:** Multicomponent competitive adsorption batch tests performed using UBWs1 and the AnRes Amberlyst A21 (A & D), Lewatit S4528 (B & E) and Lewatit A365 (C & F). Adsorption experimental trends (markers with lines) in terms of anions (A, B, C) and in terms of COD (D, E, F). For comparison, predicted CA adsorption points (+) were presented as well as the corresponding acetic acid isotherms (Langmuir or Freundlich) obtained from the single component tests (dashed lines).

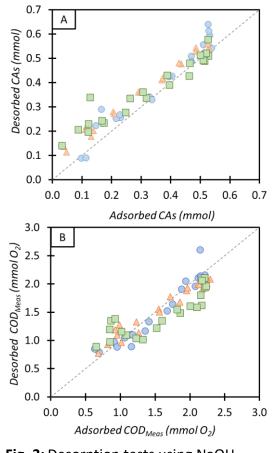
terms of COD<sub>CAS</sub>, COD<sub>CI</sub> and COD<sub>Other</sub>. The experimental points representing the adsorption of total anions (Fig. 2 A, B and C) had similar profiles with respect to those previously obtained with acetic acid (dotted line), while the CA isotherms followed bell-shaped trends. In fact, at low liquid to resin ratios ( $C_{Eq} < 50$ mM) almost all anions were adsorbed, while at higher ratios the resin underwent saturation (i.e. all exchange sites are bound to an anion). When saturated ( $C_{Eq} > 120$  mM), the CA adsorption decreased since the AnRes sites have a higher affinity with the inorganic anions (Cl<sup>-</sup> or PO<sub>4</sub>x<sup>-</sup>). Indeed, expected CA adsorption points were predicted by considering the acetic acid isotherms previously obtained in **Section** 

2.2.1 along with the inorganic cations and anions interferences (rational in Section 2.2.4). The expected 1 points ([CAs]<sub>Eq</sub>"; q<sub>CAs</sub>") resulted quite accurate as shown in **Fig. 2** (marker +), with correlation coefficients 2 (R<sup>2</sup>) of 0.93 (Amberlyst A21), 0.92 (Lewatit S4528) and 0.95 (Lewatit A365). Contrary to what reported 3 elsewhere [8], such an accurate prediction suggests that the adsorption of COD<sub>Other</sub> (Fig. 2 D, E and F) did 4 5 not significantly interfere with CA adsorption mechanism. Therefore, either COD<sub>Other</sub> affinity is lower than that of CAs or its adsorption is due to physisorption (i.e. without occupying exchange sites). The obtained 6 7 results suggest that the key concern is to separate Na<sup>+</sup> as much as possible before applying the anion 8 adsorption step, rather than optimizing the AnRes protonation by adding inorganic anions. The higher affinity of Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup> was confirmed for all AnRes. Indeed, it was not possible to measure the [PO<sub>4</sub><sup>x-</sup>]<sub>Eq</sub> 9 10 for the bifunctional resin (Lewatit A365) case, probably due to the higher affinity and capacity of this AnRes. 11

The resulting CA adsorption isotherms, shown in **Fig. 2 A, B and C**, confirmed the improvement obtained by the application of the proposed strategy. The resins with tertiary amines adsorbed ca. 3.2 mmol/g<sub>dry res</sub> of CAs (**Fig. 2 A and B**); notably, this value is more than 2 times higher than the one reported by [8] for the same Amberlyst A21. Indeed, the UBWs1 employed was almost free of cations while the actual broth used in the cited work contained almost equimolar quantities of Na<sup>+</sup> and CAs. The bifunctional resin (Lewatit A365) exerted a CA adsorption capacity even higher: up to 5.3 mmol CAs/g<sub>dry res</sub> were extracted (**Fig. 2 C**), thus this adsorbent was selected for the consecutive experiments.

Regarding the desorption, the obtained results (shown in **Fig. 3 A and B**) confirmed the feasibility of using a NaOH-Ethanol solution (0.5 M), in agreement with previous evidences [8]. All resins showed almost perfect correspondence between total desorbed CAs or overall COD and the previously adsorbed amounts (on mmol bases). Small deviations from the linear relation were obtained for the conditions containing low amounts of resin, ascribed to the inherent analytical procedures accuracy for determining the  $q_{CAs}$  at those conditions. Moreover, results presented in **Fig. 3 B** allowed inferring that also COD<sub>Other</sub>





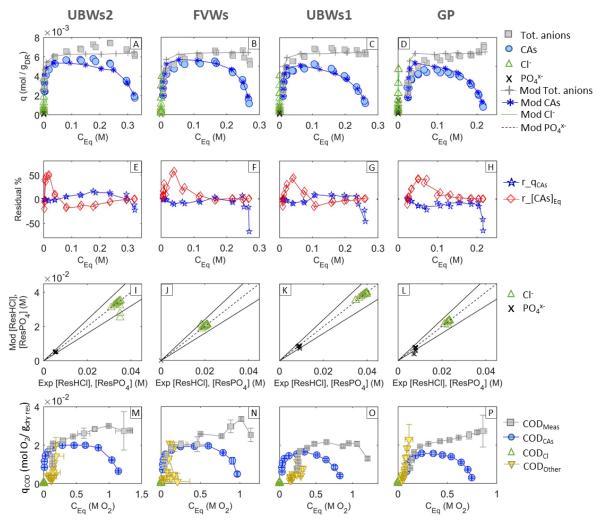
**Fig. 3:** Desorption tests using NaOHethanol solution and the AnRes portions belonging to the previous multicomponent adsorption tests with UBWs1. Total moles desorbed *vs.* total moles previously adsorbed regarding CAs (A) and COD<sub>Meas</sub> (B).

and Cl<sup>-</sup> were desorbed. Regarding PO<sub>4</sub><sup>x-</sup> desorption, due to its low concentration, it was not possible to
accurately determine its titer in the desorption solutions. Notwithstanding this, complete desorption of
phosphates was assumed, in accordance with their lower affinity (with AnRes) than that of Cl<sup>-</sup> ions, which
were completely desorbed as previously mentioned. With all this in mind, and since the desorption step
was verified to be a feasible and effective process, the following research activities were focused on the
adsorption step.

- 1
- 3.4. Testing the selected AnRes with different actual broths: matrix influence and calibration of a simple
   ion equilibrium model

4 To assess the actual broths matrix effects on the performance of Lewatit S365, three more multicomponent competitive adsorption tests were performed using the pre-treated UBWs2, FVWs and 5 GP. The obtained adsorption isotherms are shown in Fig. 4 A-D, also including UBWs1 profiles (Fig. 2 C) 6 for comparison. CA isotherms resulted to have bell-shaped trends for these actual broths as well. They 7 8 were accurately predicted by the expected CA adsorption points ([CAs]<sub>Eq</sub>"; q<sub>CAs</sub>") as indicated by the 9 obtained correlation coefficients (R<sup>2</sup>): 0.90 (UBWs2), 0.90 (FVWs) and 0.94 (GP). Besides, these high 10 correspondences confirmed that the single organic acids occurring in the broths have similar affinities for the AnRes since the method for predicting the CA adsorption points considered the overall CA mole 11 concentration (Section 2.3). In agreement with this, the enrichment factors of each adsorbed acid (EF<sub>i</sub>) 12 13 resulted 1-1.2 for all experimental conditions tested (22 for each broth). All maximal values of q<sub>CAs</sub> 14 indicated that more than 84% of the resin exchange capacity was utilized for adsorbing CAs. Even in the 15 case of the GP broth, containing the highest concentration of Na<sup>+</sup> (pH 2.43), about 70% of the AnRes exchange sites were engaged by CAs. Moreover, as formerly observed for UBWs1, the related low 16 phosphates concentration occurring in UBWs2, FVWs and GP did not allow to determine PO4<sup>x-</sup> 17 concentration in the liquid phase at the equilibrium. 18

A simplified mass action ideal model was proposed for predicting anions adsorption isotherms. Differently from the model previously proposed elsewhere [8], it considered the competitive effects of the anions (CAs, Cl<sup>-</sup> and PO<sub>4</sub><sup>x-</sup>) and cations (Na<sup>+</sup>) naturally occurring in the broths. The model was calibrated by using the multicomponent adsorption results obtained with the four actual broths. The Matlab-function *patternsearch* obtained the best fitting values of the unknow parameters after 50-100 function



**Fig. 4**: Multicomponent competitive adsorption tests performed using the Lewatit A365 and the actual effluents UBWs2 (A, E, I, M), FVWs (B, F, J, N), UBWs1 (C, G, K, O) and GP (D, H, L, P). First row of graphics shows adsorption experimental trends (markers) as well as modelled points (markers with line, e.g. Mod CAs) using the ions equilibrium model. Second graphics row shows  $q_{CAs}$  and  $[CAs]_{Eq}$  residuals (r). Third row shows experimental vs. modelled parity plots (±20%) for adsorbed Cl<sup>-</sup> and PO<sub>4</sub><sup>X-</sup>. Last row shows the averaged adsorption experimental trends in terms of COD.

1 evaluations, namely (initial values): 
$$Q = 6.767 \times 10^{-3} \ mol/g_{dry \, res} (7.5 \times 10^{-3}), \ K_a^{Res} = 9.9999 \times 10^{-14}$$
  
2  $(1 \times 10^{-13}), \ K_a^{CAs} = 1.4427 \times 10^{-5} (1.545 \times 10^{-5}), \ K_{a1}^{PO_4^{X^-}} = 7.2608 \times 10^{-3} (7.11 \times 10^{-3}), \ K_{a2}^{PO_4^{X^-}} =$   
3  $6.3768 \times 10^{-8} (6.32 \times 10^{-8}), \ K_a^{Cl^-} = 1.3317 \times 10^6 (1.2589 \times 10^6), \ K_a^{Na^+} = 1.0003 \times 10^{-15}$   
4  $(1 \times 10^{-14}), \ K_w = 1.0836 \times 10^{-14} (1 \times 10^{-14}), \ K_{Res}^{Cl^-} = 8.1440 \times 10^4 (8 \times 10^4), \ K_{Res1}^{PO_4^{X^-}} =$ 

 $5.7766 \times 10^3$  (6 × 10<sup>3</sup>),  $K_{Res2}^{PO_4^{X^-}} = 7.4879 \times 10^4$  (7 × 10<sup>4</sup>),  $K_{Res}^{CAs} = 5.1651 \times 10^3$  (5 × 10<sup>3</sup>) and  $K_{Na^+}^{CAs} = 5.1651 \times 10^3$ 1  $1.0766 \times 10^6$  (1  $\times$  10<sup>6</sup>), with an objective function error of ca. 15 (initially being ca. 40). The best 2 estimate of the Lewatit A365 exchange capacity (Q) resulted to be in accordance with the average free CA 3 content in the four effluents (ca. 265 mM, representing ca. 90% of total anions) and with the acetic acid 4 isotherm presented in the previous **Section 3.1** ( $3.51 \times 265^{0.126} = 7.09 \times 10^{-3} mol/g_{dry res}$ ). The 5 estimated dissociation constants ( $K_{\alpha}$  for the inorganic acids and bases, respectively) resulted slightly 6 higher than the standard constants for diluted systems (here used as initial guessing values), this in 7 accordance with the electrolytes concentration effects [22]. As shown in Table 2 and Fig. 4 E, F, G and H 8 the proposed pH-dependent model allows a very good overall fit of the experimental CA concentrations 9 10 in the liquid phase ([CAs]<sub>Eq</sub>) and in the solid phase ([ResHRCOO] and q<sub>CAs</sub>), even at higher Na<sup>+</sup> concentration, as in GP broth. Considering the residual trends shown in these graphics, it can be observed 11 that the proposed model is characterised by a good prediction of: (i) the CA concentrations in the solid 12 ([ResHRCOO]) excepting for the last point/s at the lowest amounts of AnRes; (ii) the liquid total CA 13 concentrations ( $[CAs]_{Eq}$ ) for values  $\geq 0.1$  M (errors <20%), while higher errors were detected (up to 50%) 14 at lower concentrations as previously reported elsewhere [8]. However, in the present work such 15 16 deviations are not only ascribed to low intrinsic accuracy of the HPLC-RID analyses at low CA concentrations but also to the likely existence of an inflexion point difficult to be accurately predicted by 17 18 this model. This is evident when observing the GP's residual curve for [CAs]<sub>Eq</sub> (Fig. 4 H, diamond marker), whose maximum value corresponds to a higher [CAs]<sub>Eq</sub> than those of other effluents. Regarding the 19 20 accuracy for inorganic anions, the low liquid concentrations at the equilibrium for Cl<sup>-</sup> and the inability to 21 detect PO<sub>4</sub><sup>x-</sup> forced to analyse the model performance in terms of the adsorbed concentrations prediction (Fig. 4 I, J, K and L). Few points of chloride and phosphates curves did not perfectly fit with the model, this 22 23 was ascribed to the lack of precision when analytes with high affinities for the AnRes occurred at very low

24

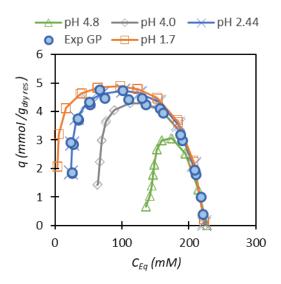
- 1 concentration. Despite this, good correlation values were obtained for  $q_{Cl}$  and  $q_{PO_4}^{x-}$  (**Table 2**). The 2 concordance of prediction capacity among different effluents confirms the model is dependable.
- 3 Table 2: Fitting quality of the proposed model with the different effluents in terms of correlation
- 4 coefficients (R<sup>2</sup>) for the solid and liquid concentrations

EFFLUENT	$R^2_{[ResHRCOO]}$	$R_{q_{CAs}}^2$	$R^2_{[CAs]_{Eq}}$	$R_{q_{Cl}}^2$	$R^2_{q_{PO_4}}$
UBWS2	0.99	0.90	0.99	0.98	0.98
FVWS	0.99	0.95	0.99	0.98	0.96
UBWS1	0.99	0.94	0.99	0.99	0.93
GP	0.96	0.88	0.97	0.99	0.84

<sup>5</sup> 

6 Concerning the AnRes selectivity, COD<sub>Other</sub> was adsorbed in all effluents (Fig. 4 M, N, O and P). Yet, the expected CA isotherms (q<sub>CAs</sub>" vs. [CAs]<sub>Eq</sub>") and the ion equilibrium model both accurately predicted the 7 CA adsorption quantities even when calculations did not consider COD<sub>Other</sub>. This evidence suggests the 8 occurrence of COD<sub>Other</sub> physisorption rather than ionic sorption. Sure enough, even if driven by 9 10 chemisorption, its affinity is lower than that of CAs, since all the COD<sub>Other</sub> isotherms are positioned at the right of the bell-shaped COD<sub>CAs</sub> isotherms. The only exception was the one of GP broth, where the higher 11 Na<sup>+</sup> content (higher pH) made the bell-shape "translation" to the right while the COD<sub>Other</sub> affinity 12 remained invariable. 13 All the obtained results showed that the separation of the Na<sup>+</sup> before recovering CAs by employing an 14 15 AnRes is crucial. Indeed, Zeidan and Marti observed almost identical trends of formic acid adsorption efficiency vs. initial effluent pH when using Amberlite IRA 96 (with tertiary amines) or Lewatit MP 64 (with 16 tertiary and quaternary amines), this meaning that the strong basic quaternary amines resulted to have 17

the same efficiency of a weak basic resin which is not always completely dissociated [23]. Moreover, Fig.



**Fig. 5:** Effect of GP's Na<sup>+</sup>-content on the resulting CA isotherms. Simulated curves using the same portions and GP broth compositions belonging to the results shown in Fig.4 except for the different Na<sup>+</sup> contents represented by different initial pH. For comparison, experimental CA adsorption points obtained using the actual GP at its initial pH of 2.43 were also plot.

- **5** illustrates how Na<sup>+</sup> content (inferable by the effluent's initial pH) would affect the GP's CA-isotherms.
- 2 Four expected CA isotherms were simulated by considering the implementation of the same AnRes
- 3 portions and GP broth composition used in the previous experiment, but with different Na<sup>+</sup>
- 4 concentrations and thus with the following pH values: 1.7, 2.4 (verified experimental condition), 4.0 and
- 5 4.9. It is an advantage to obtain "favourable" CA adsorption isotherms, i.e. the closer the curve to the *q*
- 6 axis the higher the amount of CAs potentially recovered. This can be figured out when considering
- 7 process operating lines and equilibriums for the adsorption equipment design [24].
- 8

It is well known that repeated adsorption-desorption cycles should be carried out to verify the resin 1 reutilization. Hence, a preliminary test was carried out in the present work by performing three 2 consecutive cycles using the UBWs2, the AnRes Lewatit A365 and the same 10 mL vial previously 3 employed. In addition to the desorption carried out with the NaOH solution (also serving to resin 4 regeneration), a water washing step was added. The CA adsorption yielded on average 5.67 mmol/gdry res 5 (± 11.7%), while the desorption yielded 0.95-1.09 mmol of desorbed CAs per mmol of adsorbed CAs. 6 As a whole, the proposal resulted technically feasible and effectively improved the CA recovery using a 7 8 weak AnRes (with high exchange capacity). Notably, the assessed mass action ideal model considers the interferences from Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and Na<sup>+</sup> occurring in typical CA-rich effluents and it is not affected by matrix 9 effects due to type and concentration of undefined compounds occurring in different broths (COD<sub>Other</sub>). 10 11 The model turned out to be accurate for the prediction of various experimental conditions, including different ionic strength conditions along an isotherm and even the employment of very dissimilar broths 12 13 with different type and concentrations of: matrix contained compounds (COD<sub>Other</sub>, 191-398 mM O<sub>2</sub>), CAs 14 (221-348 mM), Na<sup>+</sup> (pH 1.5-2.43, i.e. 6.4-27.2 mM), PO<sub>4</sub><sup>x-</sup> (0.1-9.5 mM) and Cl<sup>-</sup> (21.7-41.1 mM). Regarding the use of concentration equilibrium constants, the obtained accuracy is still justified by the facts that 15 ionic strengths of CA-rich broths were not significantly high (14-29 mM). Thus, exerting low electrolyte 16 effects, e.g.: limited variations of 7% and 8% with respect to the thermodynamic constants of  $K_a^{CAs}$  and 17  $K_w$  were observed. Besides, among potential species that could exert higher electrolyte effects (PO<sub>4</sub><sup>-2</sup> and 18 SO<sub>4</sub><sup>-2</sup>), only PO<sub>4</sub><sup>-2</sup> slightly occurred in the tested broths. Of course, if required, more accurate fittings can 19 20 be obtained by performing calibrations for each effluent or by using thermodynamic constants and activity coefficients. However, the purpose of the present work was to adjust a unique simplified model 21 capable of predicting the adsorption isotherms despite working with different effluents and compositions. 22 23 This can represent an effective tool e.g. *i*) when designing such a recovery process since there would be

no need to dispose of representative experimental adsorption isotherms for a specific effluent, or *ii*) to
 monitor batch adsorption processes by using only a pH-meter.

Results are very encouraging in the perspective of scaling up and optimizing the process at pilot scale, in 3 order to target effective CA extractions for many potential applications in the framework of the 4 5 carboxylate platform. In this regard, adsorption processes at industrial scale are typically run under semi 6 continuous conditions, i.e. columns are set-up in pairs where alternately one operates in adsorption and the other in desorption modes. Therefore, future pilot-scale studies should include (for both cationic and 7 8 anionic resins) i) adsorption break-through tests at different feeding rates using an actual CA-rich stream and *ii*) desorption tests. These studies would allow to: 1) construct curves defining the adsorption 9 capacity utilization yield vs feeding rate; 2) verify and optimize desorption procedures; 3) evaluate the 10 11 repeatability of both resin exchange capacities by the application of a significative number of cycles, including the assessment of resin contamination as well as dedicated regeneration steps for 12 13 decontamination; and, finally, 4) evaluate the process overall economic feasibility.

14

## 15 4. Conclusions

The application of a cationic resin step for adsorbing Na<sup>+</sup> before applying an anionic resin adsorption step 16 17 for recovering CAs from fermentation broths highly improved the CA-capture performance. Obtained 18 recovery yields from actual broths resulted over two folds higher than previously reported values. 19 The proposed calculation-receipt for predicting the CA adsorption isotherms in multicomponent 20 competitive system demonstrated to be an accurate and simple tool for designing adsorption tests. The 21 proposed homogeneous mass action ideal model showed a very good capability to predict 22 multicomponent competitive adsorption isotherms at different conventional process conditions. 23 Interferences from Cl<sup>-</sup>, PO<sub>4</sub><sup>x-</sup> and Na<sup>+</sup> occurring in typical CA-rich broths resulted more significant than

1	inter	interferences due to the adsorption of other organic compounds or than the optimization of anionic					
2	resins dissociation previously reported in the literature.						
3							
4	Decla	aration of Competing Interest					
5	The authors declare that they have no known competing financial interests or personal relationships that						
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11							
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