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This is the final peer-reviewed author's accepted manuscript (postprint) of the following publication:

Published Version:

Carnevali D., D'Oliveira A., Rigamonti M.G., Cavani F., Patience G.S. (2022). Pt-WO₃ oxydehydrates fructose to furans in the gas phase. CHEMICAL ENGINEERING JOURNAL, 429, 1-10 [10.1016/j.cej.2021.132337].

Availability:

This version is available at: <https://hdl.handle.net/11585/898252> since: 2024-05-27

Published:

DOI: <http://doi.org/10.1016/j.cej.2021.132337>

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Pt-WO₃ oxydehydrates fructose to furans in the gas phase

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Abstract

Bio feedstocks are destined to replace fossil fuels for specialty chemicals but current biorefineries mainly ferment hexose—the most abundant feedstock—to ethanol. The maximum theoretical carbon atom efficiency of this process is 67% but the market price of biofuels is several-fold lower than biochemicals and monomers. We report for the first time a gas phase catalytic process that dehydrates fructose to 5-hydroxymethyl furfural (HMF). A two-fluid nozzle atomizes aqueous solutions of fructose into a fluidized bed operating at 350 °C. The solution forms an aerosol (droplet size of 30 μm), which contacts the hot Pt-WO₃/TiO₂ catalyst and reacts to HMF rather than caramelizing. The maximum yield reached 21% and it increased slightly with temperature, and decreased with increasing catalyst inventory; it was less sensitive to O₂ concentration, Pt loading on the catalyst, liquid feed flow rate, and fructose feed concentration. At the optimal condition, selectivity continued to increase with time even after 3 h reaction. Selectivity to 2,5-diformyl furan reached 42% at 250 °C with HMF as a feedstock.

Keywords: fluidized bed, oxydehydration, fructose, platinum, atomization, 5-hydroxymethyl furfural

1. Introduction

The elevated oxygen/carbon ratio of carbohydrates versus petroleum constitutes an advantage to produce specialty chemicals and monomers. Sugar fermentation to bio-ethanol dominates the market at a maximum theoretical carbon atom yield of 67% [1]. However, specialty chemicals command prices several-fold higher than that of bioethanol at fuel value. Fructose dehydrates to 5-hydroxymethyl furfural (HMF), a green intermediate, with a greater selectivity than glucose due to the similar spatial conformation and the faster enolisation reaction [2]. Hydrogen reacts with HMF to dimethyl furan and dimethyl tetrahydrofuran (Figure 1)—a biofuel [3, 4]— while the hydrogenolytic ring opening produces adipic acid—a monomer for nylon-6,6 [5]. Oxygen reacts with HMF to 2,5-diformyl furan [6, 7, 8] and further to 2,5-furandicarboxylic acid (FDCA) [9, 10]. FDCA is the furanic substitute of terephthalic acid, which is a promising substitute for polyethylene terephthalate. Avantium developed the YXY technology that converts HMF to an ether with methanol/ethanol followed by an oxidation step to FDCA [11, 12]. Acidic catalysts, ionic liquids, and supercritical water dehydrate fructose and glucose to HMF [13, 14, 15, 16, 17, 18, 19]. Organic solvents are necessary to extract the product otherwise HMF hydrolyzes to levulinic acid and formic acid, or polymerizes to insoluble compounds—humins [20, 21, 22] (Figure 1).

Sn-Beta zeolite in tetrahydrofuran and water convert carbohydrates at 70% selectivity [23]. Other organic solvents include alkylphenol [24], dimethylsulfoxide (DMSO) and methylisobutylketone [25, 26] and ethyl acetate [27]. These processes require contact times that range from minutes to hours because of the poor mass and heat transfer characteristics of multiphase (liquid) reactors.

Metal-based catalysts [9, 10, 28, 29, 30, 31] or enzymatic processes [32, 33, 34] oxidize HMF to FDCA. Tandem processes in a single vessel reduces complexity

28 like the multiphase reactor with methyl-isobutyl ketone and 2-butanol as organic
29 phase [35]; the aqueous solution dehydrates fructose to HMF, while the organic
30 phase extracts it and further oxidizes to FDCA [36]. Pt/C oxydehydrates fruc-
31 tose to FDCA in γ -valero lactone and H₂O [37]. Combination of ionic liquids
32 and not-noble metals avoid the organic phase and allows the one pot reaction
33 [38]. Fluidized bed reactors operate at higher temperature with superior mass
34 transfer and, consequently, reaction rates orders of magnitude higher. FBRs
35 pyrolyze biomass into energy and chemicals [39]. Glass beads in an FBR cracks
36 aqueous solutions of sugar sparged into the bed [40, 41] Fast pyrolysis of cellulose
37 in FBRs approach 62 % yields of levoglucosan, 3.5 % of HMF and 1 % of furfural
38 [42]. Immobilized anaerobic sludge produces biohydrogen and bioethanol [43].
39 A magnetically stirred fluidized bed reactor ferments glucose to ethanol within
40 95 % of the theoretical yield [44]. Two anaerobic fluidized bed reactors at 55 °C
41 product H₂ and ethanol molar fractions of 59 % for a xylose-glucose mixture
42 [45].

43 We demonstrated the versatility of atomizing liquids into catalytic fluidized
44 beds: VPO partially oxidizes xylose to C2-C4 carboxylic acids [46]; WO₃/TiO₂
45 dehydrates glycerol to acrolein [47]; decarbonylates fructose to furfural [48]; and,
46 Keggin-type catalyst oxydehydrates 2-methyl,1-3-propanediol to methacrylic
47 acid [49]. Here we investigated fructose dehydration to HMF in a μ -fluidized
48 bed reactor. A nozzle atomized the aqueous liquid feed directly into the cat-
49 alytic bed. We screened temperature, O₂ concentration, catalyst loading, Pt
50 content on the catalyst, liquid flow rate, feed fructose mass concentration with
51 a Plackett-Burman experimental design. The experimental plan was based on
52 three levels of temperature and O₂:fructose molar ratio and two levels for cata-
53 lyst loading.

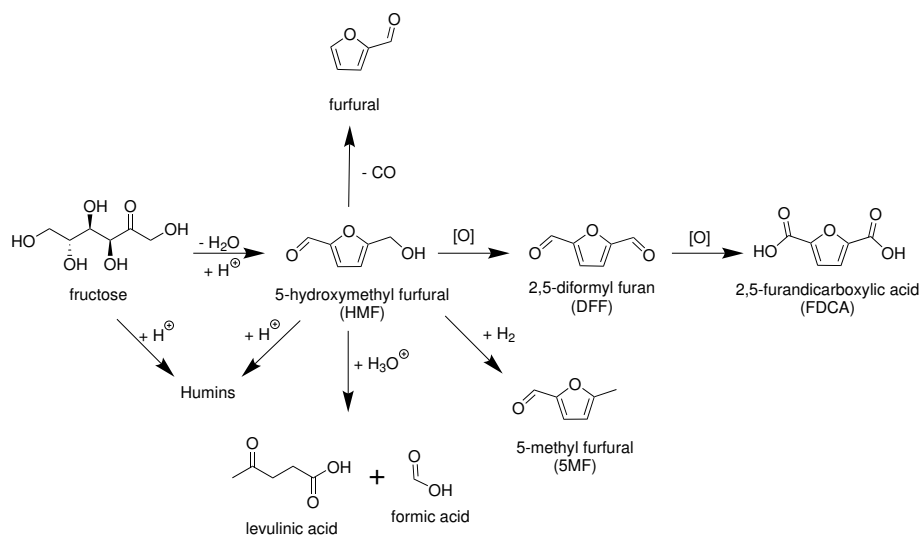


Figure 1: Fructose dehydrates to HMF. Organic solvents suppress the polymerization to humins and the rehydration to levulinic acid and formic acid. Decarbonylation leads to furfural, while the hydrogenation produces 5MF. HMF oxidation gives DFF and further FDCA, the furanic substitute of terephthalic acid.

54 2. Experimental section

55 A furnace heated a 15 mm ID by 400 mm high quartz tube. Three thermo-
 56 couples measured the temperature along the length at 20 mm below the bed,
 57 5 mm — inside the bed, 90 mm above the distributor, and a fourth monitored
 58 the temperature in the exit line. The reactor operated at 1.4 bar while the
 59 ΔP between the inlet and outlet—0.001 bar during the reaction. A quartz frit,
 60 with a porosity of 150 μm to 200 μm , ensured the gas was distributed uniformly
 61 across the reactor diameter (Figure 2). A stream of O_2 in Ar fluidized the cat-
 62 alytic bed and burned the coke formed during the reaction. A nozzle atomized
 63 the aqueous fructose solution into the Pt- WO_3/TiO_2 catalytic bed. An HPLC
 64 pump metered the liquid solution feedrate while 50 mL min^{-1} of argon atomized
 65 it to produce an effervescent spray (Figure 3c) with droplets less than 30 μm
 66 to minimize catalyst agglomeration and blocking the nozzle. A ceramic tube
 67 enveloped the injector to reduce the heat transfer and ensure that the solvent

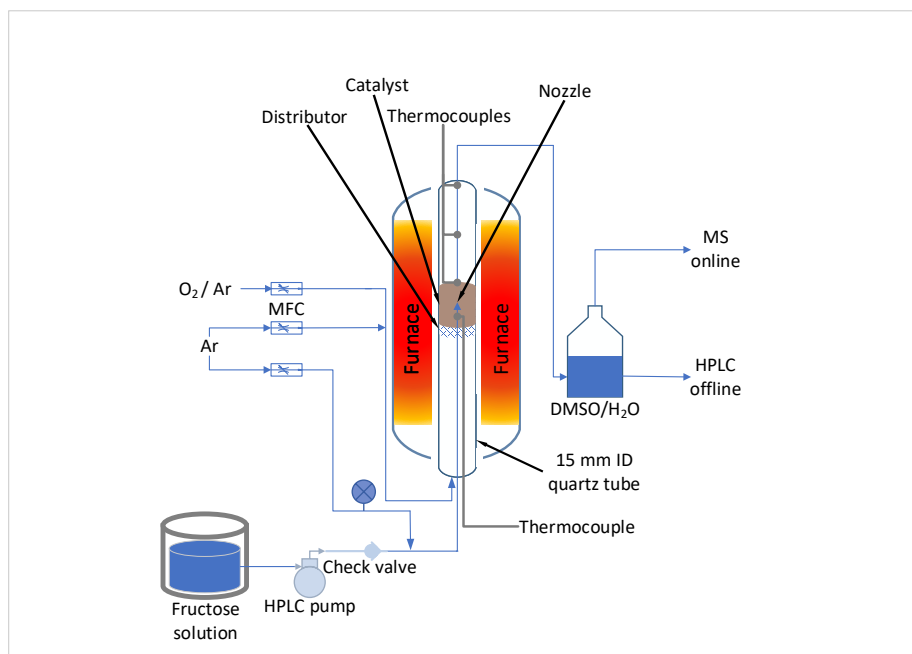


Figure 2: A nozzle atomizes the fructose solution directly into the catalytic bed. A DMSO/H₂O quench traps the products and an HPLC analyzes the trend. An online MS monitored non-condensable gases.

68 evaporated in the bed rather than the injector; A stream of 50 mL min⁻¹ of argon
 69 flushed the annular space between the injector and ceramic tube. The exit line
 70 (uninsulated) fed into a quench in an ice bath The quench fluid contained 25 g
 71 dimethyl sulfoxide to improve furanic solubility and 25 g H₂O. An on-line mass
 72 spectrometer (MS) with a multiple ion detector monitored non-condensable gas
 73 concentrations—CO, CO₂, O₂, Ar, CH₄, while an HPLC quantified the liquid
 74 samples collected each 15 min during the first hour and then each 30 min until
 75 the end of the experiment (Figure 2). Glycerol was the internal standard for
 76 the HPLC analysis. At the end of each experiment we cleaned the exit line with
 77 5 mL of water and analyzed this sample.

78 Product selectivity, S_i , is based on a molar balance around each component
 79 i , n_i^{out} :

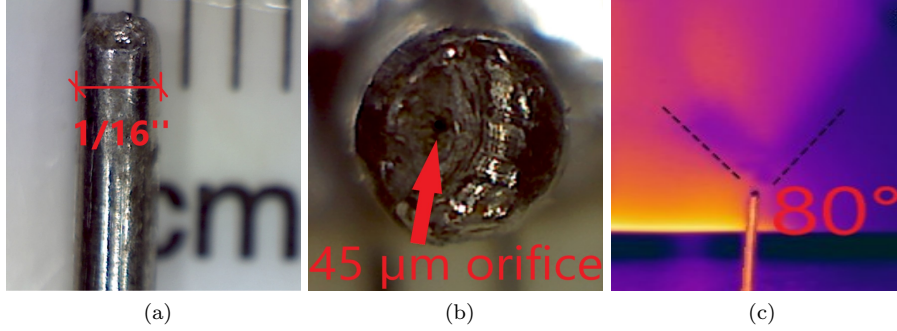


Figure 3: 1/16" (1.59 mm) stainless steel pipe filed at the top to obtain an orifice of 45 μm . The IR camera shows that the atomization and the evaporation at the orifice decreased the temperature at the tip, forming a full cone with an angle of 80°.

$$S_i = \frac{\sum_j n_{i,j}^{\text{out}} / \vartheta_{i,j}}{n_{\text{fr}}^{\text{in}} - n_{\text{fr}}^{\text{out}}} \cdot 100 \quad (1)$$

80 where $n_{\text{fr}}^{\text{in}}$ and $n_{\text{fr}}^{\text{out}}$ are the moles of fructose entering and exiting the system and
 81 ϑ_i is the stoichiometric coefficient for the carbon component of each reaction j .
 82 The median droplet size diameter, d_{50} , exiting the nozzle of an internal mixing
 83 air-assist atomizer is [50]:

$$d_{50} = 20 u_L^{0.5} m_L^{0.1} d_L^{0.1} \sigma^{0.2} \rho_g^{-0.3} \Delta U^{-1.0} \left[1 + \frac{m_L}{m_g} \right]^{0.5} \quad (2)$$

84 where u_L is the superficial velocity, m_L and m_g the mass flow of the liquid
 85 and the gas, d_L the orifice dimension, σ is the surface tension and the ΔU the
 86 relative velocity between the liquid and the gas.

87 2.1. Materials

88 All the reagents are analytical grade without further purification. We ac-
 89 quired D-fructose(99 %) from Alfa Aesar. We purchased 5-hydroxymethyl fur-
 90 fural (99 %), furfural (99 %), 5-hydroxymethyl-2-furancarboxylic acid, 5-formyl-
 91 2-furoic acid, 2,5-furandicarboxylic acid (97 %), 2,5-furandicarboxaldehyde (97 %),

92 5-methyl-2-furaldehyde ($\geq 98\%$), and tetraammineplatinum(II) nitrate ($\geq 99.9\%$)
93 and ammonium (para)tungstate hydrate ($>99.99\%$) from Sigma Aldrich. Air
94 Liquide Canada supplied the gases: argon ($> 99.7\%$), 10.0% O_2 balance Ar, and
95 a mixture of CO (1.04%), CO_2 (1.01%), CH_4 (1.03%) balance Ar. Huntsman
96 Corporation supplied the titanium dioxide (Hombikat 110100).

97 *2.2. Catalyst preparation*

98 We sieved the support powder from $90\ \mu\text{m}$ to $150\ \mu\text{m}$ in diameter. The crys-
99 talline phase of the titania was pure anatase. A successive wetness impregnation
100 method deposited first WO_3 and then Pt on the TiO_2 support. Initially we de-
101 termined the total pore volume by dropwise addition of water. Ammonium
102 paratungstate dissolved in a volume of water equivalent to the pore volume of
103 the support. A rotary evaporator operating at 100 rpm for 3 h mixed the active
104 phase and support. The catalyst then dried at $70\ ^\circ\text{C}$ and 300 mbar for 2 h. The
105 powder then calcined in a furnace at $120\ ^\circ\text{C}$ for 4 h to completely remove traces
106 of water. The furnace then ramped temperature at $2.5\ ^\circ\text{C}\ \text{min}^{-1}$ to $600\ ^\circ\text{C}$ in
107 air. The powder remained in the furnace at this temperature for 4 h.

108 *2.3. Analytical instrumentation*

109 A Philips X'PERT diffractometer generated XRD spectra with a monochro-
110 matic $\text{Cu-}k\alpha$ beam, $\lambda = 0.15406\ \text{nm}$, at 50 kV and 40 mA. It scanned the
111 gonio axis from 20° to 85° , at a rate of $0.01\ ^\circ\ \text{s}^{-1}$. The crystalline phases were
112 identified with the ICDD database and the Rietveld refinement (X'PERT high-
113 score) gave a semi-quantitative characterization for the phases' weight compo-
114 sition. The Scherrer approximation defined the average cubic crystallite size:
115 $D = 0.94\lambda/\beta\text{Cos}\theta$, where λ is the mentioned instrument wavelength, β is the
116 full-width at half-maximum peak height (FWHM, rad), and θ is the Bragg angle
117 for the most intense peak (half of the 2θ position).

118 The FE-SEM-JEOL JSM-7600F scanning electron microscope (SEM) ac-
119 quired the catalyst images between 5 kV to 30 kV, using secondary and backscat-
120 tered electrons detectors (secondary electron image —SEI, low secondary elec-
121 tron image —LEI and backscatter image —LAbE). The energy dispersive X-ray
122 detector (EDX) mapped the surface of the catalyst and qualitatively quantified
123 the composition and the different phase regions.

124 A laser diffractometer (Horiba, LA-950) evaluated the particle size distribu-
125 tion (PSD) based on the Mie Theory:

$$D_{4,3} = \frac{\sum d_i^4 \cdot N_i}{\sum d_i^3 \cdot N_i} \quad (3)$$

126 with N_i as number of particles with diameter d_i . The particle refractive index
127 was $2.75 + 0.00i$ (R and Chi parameter below 0.05).

128 A Quantachrome Autosorb-1 N₂ physisorption instrument recorded the ad-
129 sorption and desorption isotherms at 77 K. A degasser, operating under vacuum
130 at 300 °C for 6 h, removed the gas adsorbed on the surface [51]. The Brunauer-
131 Emmett-Teller (BET) theory regress the specific surface area at P/P_0 0.05 to
132 0.3. The instrument estimated the mesopore size distribution over the desorp-
133 tion branch (P/P_0 0.15-0.995), based on the Barrett-Joyner-Hallender (BJH)
134 theory. The total pore volume is evaluated at the maximum filling pressure
135 (P/P_0 0.995), considering all pores with a diameter smaller than 300 nm.

136 A LECO CS744 CHN analyzer measured carbon build up on the catalyst
137 surface after each experiment. An internal balance measured the sample weight
138 loss, when heated above 1000 °C in air. A further CO trap converted the re-
139 maining carbon monoxide to CO₂.

140 A Varian ProStar 325 HPLC, equipped with a UV detector at 260 nm, quan-
141 tified species concentration of the liquid samples. A MetaCarb 87H column, kept
142 at 60 °C, separated the compounds. The pump flowed a 0.05 N aqueous H₂SO₄

143 solution at 0.35 mL min^{-1} . Each analysis lasted 70 min to ensure the products
144 separation.

145 **3. Results and discussion**

146 *3.1. Catalyst characterization*

147 *3.1.1. Fluidization and particle size distribution*

148 Geldart classified particles into 4 categories based on the catalyst diameter
149 and the differential of the particle density and the gas density [52]. Geldart
150 group A powders are best suited for catalytic fluidized beds with diameters
151 (d_{50}) on the order of $70 \mu\text{m}$. Based on the Horiba LA-950, the average spher-
152 ical particle diameter of fresh catalyst increased from $85 \mu\text{m}$ to $95 \mu\text{m}$ (Figure
153 4). Coke covered the surface (SEM-EDX) and increased the average particle
154 diameter by $10 \mu\text{m}$. The bulk density was 770 kg m^{-3} , so that we classify it as
155 a group A powder.

156 The minimum fluidization velocity, u_{mf} , with 3 g of catalyst in the reactor
157 was 8 mm s^{-1} . Catalyst attrition resistance is a major concern for fluidized
158 beds particularly with high velocity jets where particles collide and fragments or
159 cleaves surface asperities. To prevent this phenomena we opted for the catalyst
160 synthesis by incipient wetness impregnation, which minimizes surface defects
161 and thus asperities. We tested the attrition rate in an air jet mill according to
162 the ASTM 5757 [53]. The high velocity simulates the mechanical stress coming
163 from the nozzle and the distributor. A filtered vessel collected the elutriated fines
164 after 24 h. The catalyst attrits at 5.4 mg h^{-1} , which is well within commercial
165 practice [54].

166 *3.1.2. XRD*

167 We analyzed the calcined catalyst before reaction with a mass fraction of 5 %
168 WO_3 on TiO_2 and 0.5 % Pt or 1.5 % Pt. We characterized the catalyst at the end

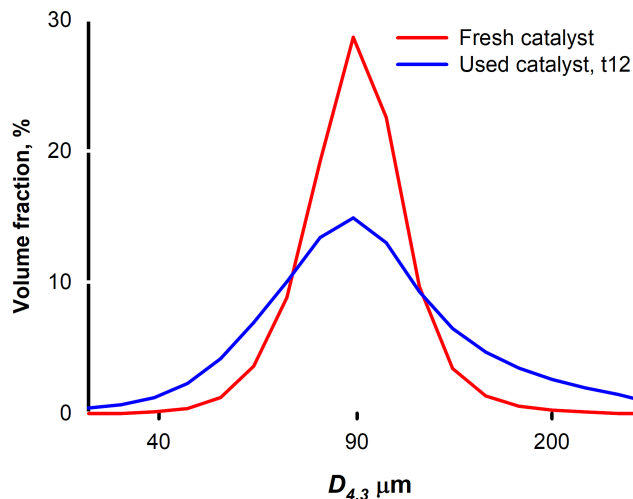


Figure 4: Catalyst particle size distribution in logarithmic scale. Coke deposits broadened the peak and increased the average.

Table 1: Variation of the catalyst physical characteristics after the reaction

Property	Fresh	Used
d_{50} , μm	85	95
SA, m g^{-2}	51.4(1)	71(2)
V_{pore} , mL g^{-1}	0.165	0.064
u_{mf} , mm s^{-1}	8	
ρ_{bulk} , kg m^{-3}	770	
Attrition resistance, mg h^{-1}	5.4	5.4

169 of experiment t12 (1.5% Pt), which had the most coke. XRD analysis detected
 170 two crystalline phases: anatase for the titania (ref: 96-900-9087) and platinum
 171 (ref: 96-101-1114) while EDX confirmed the presence of W since it was below the
 172 XRD detection limit [48]. The titania support maintained a tetragonal structure
 173 during calcination and reaction. The platinum presented a cubic structure, with
 174 a submicron crystallinity, which increased with Pt loading and decreased due to
 175 the coke deposition during the reaction. SEM confirmed the results, providing
 176 images of crystals with several hundred nanometers size and a round-prismatic
 177 shape. Each crystal contained several crystallites, growing in different directions

Table 2: D crystallite size (standard deviation among Pt signals); Riet.Pt Rietveld refinement of the Pt phase, the complementary fraction was anatase TiO_2 ; BET surface area by nitrogen physisorption, results are within $\pm 3\%$ ($n = 3$, 95 % confidence interval, CI); ϕ pore volume ($\text{CI} \pm 8 \times 10^{-5} \text{ mL g}^{-1}$); $\Delta_{dS(d)} dS(d)$ characteristic pore median (ads. BJH for mesopore and QSDFT for micro); $V - t$ micropore area.

WO_3/TiO_2	D nm	Riet. Pt g g^{-1}	BET $\text{m}^2 \text{g}^{-1}$	V_{pore} mL g^{-1}	$\Delta_{dV(d)}$ nm	$V - t$ $\text{m}^2 \text{g}^{-1}$
	na	na	63.8(0.1)	0.180	9.6(0.1)	4.3(0.5)
0.5 % Pt	52(7)	0.008	na	na	na	na
1.5 % Pt	88(2)	0.03	51.4(0.1)	0.165	11.0(0.1)	1.0(0.5)
Used, t12, 1.5 % Pt	60(10)	0.02	71(2)	0.064	0.7(0.3)	50(2)

178 (Figure 9). At 50 kV, the X-ray penetrated the catalyst down to 35 μm (Pott's
179 equation): this surface analysis overestimated the Pt fraction with respect the
180 TiO_2 support. As coke builds up, the intensity of the Pt signals decrease and
181 broaden (Table 2). During calcination, WO_3 precursor penetrated the titania
182 lattice thereby reducing the tungsten signal. Calcination at 600 $^\circ\text{C}$ was low
183 enough to minimize phase segregation and so the WO_3 remained amorphous.
184 A weak, unidentified peak emerged at 31.6 $^\circ$ after reaction. Reaction conditions
185 may have crystallized part of the amorphous WO_3 in the mesoporous titania
186 structure however, SEM-EDX could not confirm WO_3 crystals on the surface of
187 the catalyst but N_2 physisorption detected a decrease in pore size after reaction.
188 The small crystallite size (30 nm) and the strong chemical interaction with the
189 surrounding environment (coke and titania) shift the signal.

190 3.1.3. BET

191 The TiO_2 support and tungsten salt precursor contribute most to the specific
192 surface area (SSA), pore size distribution and pore volume (PV) of the catalyst
193 after calcination (Figure 6) [48]. Calcined catalyst has a type IV isotherm and
194 an $H2$ hysteresis loop: mesoporous structure with a narrow distribution of pore
195 necks. A mass fraction of 1.5 % Pt decreased the SSA with respect to calcined
196 WO_3/TiO_2 catalyst. EDX images show Pt on the surface but not in the interior

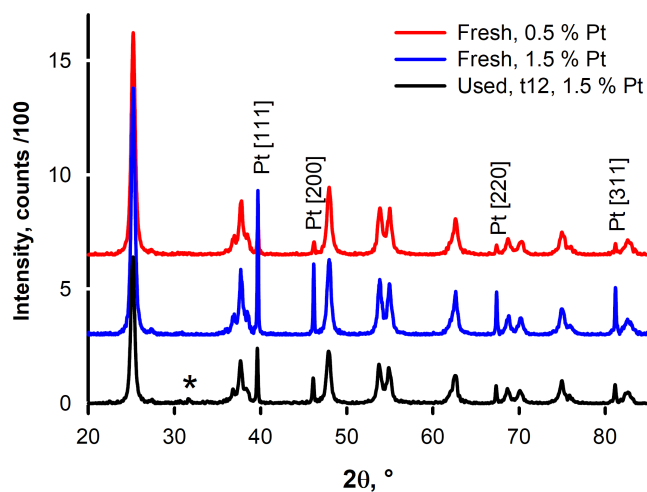


Figure 5: Stacked spectra recorded with the same conditions and smoothed with an 11 points cubic function, Cu- $k\alpha$ sidebands were removed: coke deposits on the used sample reduced the signal to noise ratio. Four sharp Pt signals (39.6° , 46.0° , 67.4° , 81.2°) and their respective planes $[hkl]$ have been identified. The remaining peaks belong to the titania support (anatase) [55].

197 so the drop in SSA and PV is due to pore-blocking. Pt obstructed pores smaller
 198 than 10 nm, which increased the characteristic pore median ($dS(d)$) by 1 nm.
 199 The “t12” catalyst has a type I-IV isotherm and an open $H4$ hysteresis: a
 200 microporous network developed as coke partially filled the internal mesoporous
 201 structure. Despite coke deposits, furanic selectivity improved with time. The
 202 SSA increased with respect to calcined catalyst, suggesting a selective coke
 203 deposit. This phenomenon decreased the reagent and product degradation,
 204 despite the pore size dropping from 11.0 nm to 0.7 nm) and the lower pore volume
 205 (Table 2). The BJH surface distribution shrunk in the mesopore region. The
 206 quenched solid state functional theory (QSDFIT) for SSA deviated less than 5 %
 207 from the BET SSA.

208 3.1.4. Field Emission Scanning Electron Microscopy (FE-SEM)/EDX

209 The tungsten oxide was homogeneously dispersed on the titania support.
 210 Pt crystals were poorly dispersed on the surface as SEM images show regions

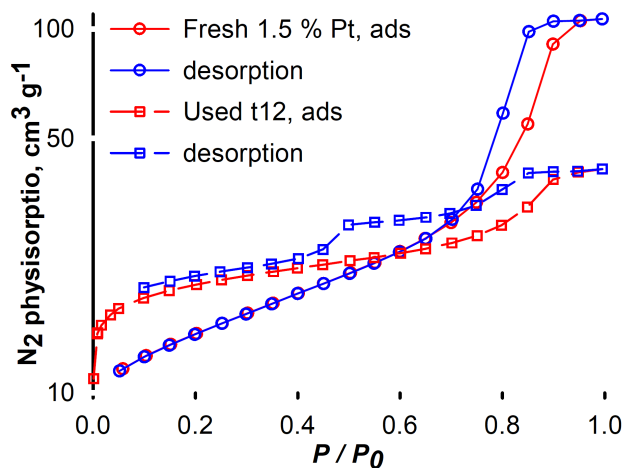


Figure 6: Nitrogen physisorption isotherms. The used catalyst loses the microporous fraction and the total pore volume decreases as a consequence. Carbon obstructing the mouth of the micropores accounts for the large reduction at $P/P_o > 0.7$.

211 with bright spots with Pt particles (Figure 7). Furthermore, some particles
 212 have much more Pt than others. The Pt submicron crystals were 250 μm on
 213 average (Figure 8). After reaction, Pt particles formed agglomerate with several
 214 hundred crystals but the powder remained free flowing. Only on the sparger tip
 215 circumference did powder agglomerate [46].

216 An EDX scan at 20 kV of the catalyst surface to a depth of 10 μm confirmed
 217 that W covered the surface uniformly. On the contrary, Pt forms submicron
 218 crystals rather than forming a monolayer on the surface or in the interior.
 219 Titanium-oxygen molar ratios were coherent with the TiO_2 composition. Pt
 220 was only in the metallic form since the EDX oxygen image showed dark spots
 221 corresponding to the Pt crystals (Figure 10).

222 We crushed used catalyst and the SEM images of the chunks showed no coke
 223 in the interior. As much as (20 μm) of coke covered some of the particles but
 224 most of it was homogeneously distributed on the surface (Figure 10). Clearly,
 225 since the carbon coverage was uniform WO_3 rather than Pt initiated the growth
 226 of the coke layer. An EDX spectrum on the coke deposit identified a molar

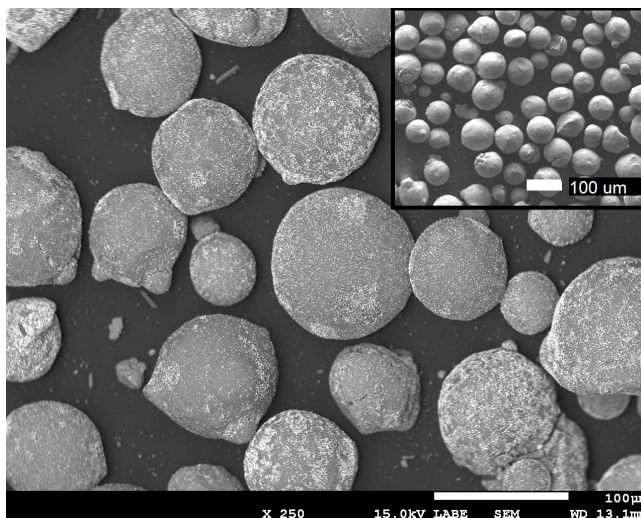


Figure 7: Fresh 1.5 % Pt over WO_3/TiO_2 particles. The LABe detector enhanced the signal from heavy elements and the Pt crystals appeared as bright white spots.

227 composition of 90 % soft carbon type and 10 % oxygen.

228 3.2. Internal-mixing two-fluid nozzle

229 Operating the fluidized bed was problematic due to frequent interruptions in
 230 the fluid flow due to solids build up in the sparger. The large surface to volume
 231 ratio of the sparger was a contributing factor as the water would evaporate in the
 232 tube and the fructose would then crystallize. We injected Ar at 50 mL min^{-1} to
 233 reduce the residence time of the solution in the tube and improve the effervescent
 234 spray of the liquid. The gas and fluid first mix at the t-junction below the
 235 sparger tip. We reduce the internal diameter of the top part of a stainless
 236 steel pipe of 1.6 mm OD and 0.127 mm ID (Figure 3a) to create a $45 \mu\text{m} \pm 5 \mu\text{m}$
 237 orifice (Figure 3b), which is a 65 % reduction of the internal diameter. The
 238 setup produced a full cone spray with an angle of $80^\circ \pm 5^\circ$, measured by infrared
 239 camera after heating the nozzle to 400°C .

240 Based on Equation 2, the median droplet size was $5 \mu\text{m}$, with a Weber num-
 241 ber of 7. The gas flow was laminar around the particles ($N_{\text{Re}} = 11$) and at the

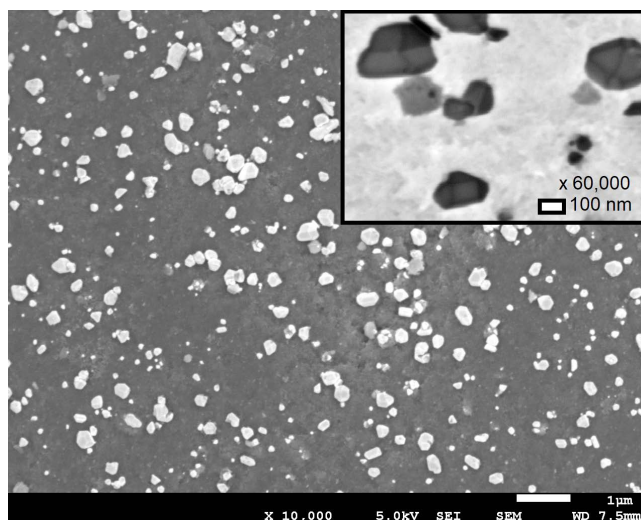


Figure 8: Fresh 1.5% Pt over WO_3/TiO_2 particles. The metallic platinum crystals appeared as multi-facets prisms. Considering their sizes (submicron), the crystallite size of 88 nm (XRD) and the crystal structure of metallic Pt (cubic), several crystallites compose the crystal.

242 orifice ($N_{\text{Re}} = 750$). Higher Re and We numbers increase the atomization speed
 243 and reduce the droplet diameter. Internal mixing increased the contact between
 244 the gas and the liquid producing finer droplets [50].

245 3.3. Screening test and full factorial design

246 A Plackett-Burman screening design assessed the influence of six factors:
 247 temperature (150 °C and 300 °C), O_2 :fructose molar ratio (2:1 and 20:1), catalyst
 248 mass (2.5 g and 5 g), Pt loading (0.5% and 1.5%), feed flow rate ($50 \mu\text{L min}^{-1}$
 249 and $100 \mu\text{L min}^{-1}$) and feed fructose mass concentration (2.5% and 5%). The
 250 design comprised 12 experiments.

251 All the tests demonstrated total conversion of fructose and produced coke,
 252 COx, and various organic compounds. Some of the fructose degraded along the
 253 walls and exit line.

254 The dehydration reaction was independent of oxygen concentration but it
 255 helped control coke build-up on the surface. The two levels of mass of catalyst

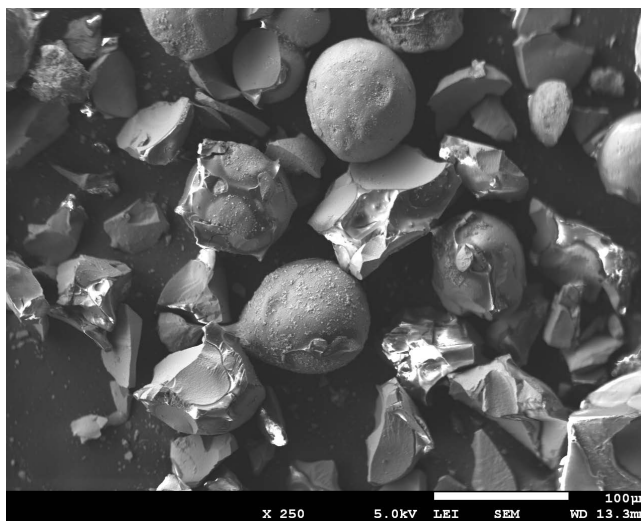


Figure 9: Used “t12” catalyst’s surface. Shiny “metallic-lookalike” coke chunks were dispersed around the spherical catalyst particles after mechanical breakage. Some particles broke as well.

256 loaded varied the contact time, while two flow rates modified the weight hour
257 space velocity and the gaseous partial pressure of water.

258 Catalyst loading accounted for most of the variance in the data: furanic
259 products selectivity was greater with less catalyst. The maximum total product
260 selectivity never exceeded 6 %, due to the extreme conditions of the screening
261 test. CO_2 and CO rose with temperature, reaching 59 % and 4 % at 300 °C,
262 respectively. Furthermore, higher oxygen concentration produced more CO_2 .
263 HMF, the dehydration product, increased with higher liquid flow rate and lower
264 catalyst loading. Increasing the partial pressure of water increased the cat-
265 alytic surface saturation, lowering the degradation kinetics. HMF conversion
266 increased with higher contact time. Furfural, the decarbonylation product of
267 HMF (Figure 1), depended only on catalyst loading—it increased with longer
268 contact time. Maximizing the contact time, determined the fructose and the
269 intermediate degradation to coke and CO_x . HMF hydrodehydrates to 5MF
270 (Figure 1). Higher temperature and lower catalyst loading increase selectivity.

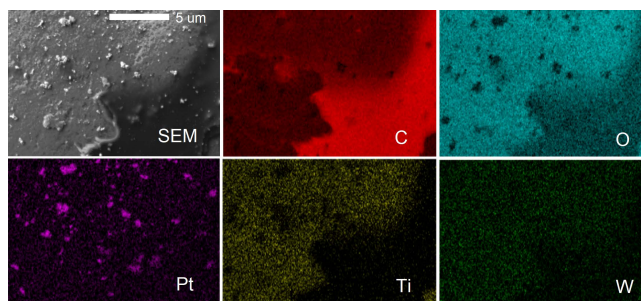


Figure 10: SEM and EDS mapping of the used “t12” catalyst’s surface. Carbon (C, red) partially covered the surface and suppressed the underlying elements’ signals. Oxygen (O, blue) was predominant were titanium was also present (Ti, yellow), less were carbon was present and absent were platinum was present (Pt, violet). Tungsten (W, green) was homogeneously distributed along with titanium.

271 Furthermore, lower O_2 concentration reduces the conversion of H_2 to water, in-
 272 creasing the hydrogenation reaction rate. Increasing the Pt favoured hydrogen
 273 adsorption, and consequently 5MF.

274 Oxygen reacts with HMF to HMFCA and DFF (Figure 1). Oxidation kinet-
 275 ics of the hydroxyl moiety of HMF is faster than the conversion of the aldehydic
 276 functional group. DFF only reached a maximum selectivity of 1%, while HM-
 277 FCA never exceeded 0.05%. Lower catalyst loading and higher temperature
 278 increased the selectivity, which is consistent for a high activation energy for
 279 HMF oxidation. Furthermore, as for all the furanic compounds, lower catalyst
 280 loading reduced the contact time and the degradation process. A further oxi-
 281 dation of HMFCA and DFF led to FDCA. The amount of catalyst tested was
 282 high, leading to elevated contact time and increasing the degradation.

283 We executed a full factorial design including three levels for temperature
 284 (300 °C, 350 °C, and 400 °C) and O_2 content (0.5, 1 and 10 molar ratio with
 285 fructose) and two levels of catalyst loading (1.5 g and 3 g). We kept Pt loading
 286 (1.5%) constant, increasing the liquid flow rate ($300 \mu\text{L min}^{-1}$) and keeping the
 287 fructose mass percentage in the feed at 2% (Table 3).

288 The contact time, τ , between the fructose injected and the catalyst varied

Table 3: Fructose oxydehydration full factorial design of experiments over 1.5% Pt-WO₃/TiO₂. Factors include catalyst loading (2 levels), temperature (3 levels), and O₂:fructose molar ratio 3 levels). The selectivities are calculated from time 0 min to 180 min. HMF: 5-hydroxymethyl furfural; FUR: furfural; 5MF: 5-methyl furfural; DFF: diformyl furan.

Exp #	Cat g	T °C	O ₂ /fruct	S _{CO₂} %	S _{CO} %	S _{CH₄} %	S _{Coke} %	S _{HMF} %	S _{FUR} %	S _{5MF} %	S _{DFF} %
1	3	300	0.5	6	6	9	8	0	5	3	1
2	3	400	1	12	10	5	10	4	5	1	1
3	1.5	300	10	20	4	17	6	6	4	0	1
4	1.5	400	1	2	3	1	12	9	3	0	0
5	3	350	10	4	3	4	55	3	2	1	1
6	3	300	1	3	12	2	43	3	1	0	0
7	1.5	350	10	0	2	0	21	1	1	0	0
8	3	350	0.5	8	5	4	54	0	5	4	3
9	1.5	300	0.5	2	0	1	13	0	1	0	0
10	1.5	300	1	4	2	3	36	5	6	1	1
11	3	350	1	12	6	5	57	1	5	4	3
12	1.5	350	1	7	5	5	49	11	6	1	2
13	1.5	350	0.5	4	3	4	31	12	6	1	1
14	1.5	400	1	7	3	5	48	7	3	1	3
15	3	400	10	47	1	17	43	0	0	0	0
16	3	300	10	41	1	15	66	1	2	0	1
17	3	400	0.5	4	2	2	24	1	9	6	2
18	1.5	400	10	11	8	3	20	0	7	4	2

289 between 0.3s to 0.4s and fructose conversion was complete for all experiments
290 (Table 3). The carbon balance was between 57% to 97%. Carbon losses were
291 due to product degradation on the reactor wall or inside the exit line. The
292 catalyst becomes increasingly selective with time and this induction time can
293 exceed 2 h so the reported selectivities are pessimistic since they are calculated
294 based on the 3 h from when the pump started. The mass balance of several tests
295 were less than 50% so we have ignored these tests while assessing the impacts
296 of the various factors. The sum of the selective oxidation products—HMF,
297 furfural, 5-methyl furfural, and DFF—reached 20%. The highest yield of DFF
298 was only 3% but HMF, the first step of the process, reached 12%. According to
299 a power-law regression model, the furanic’s concentration increases linearly with
300 temperature but decreases with the square root of mass of catalyst and decreases
301 to a lower power with the oxygen:fructose ratio—feeding more oxygen reduces
302 the productivity (Figure 11). The correlation explains 63% of the variance in

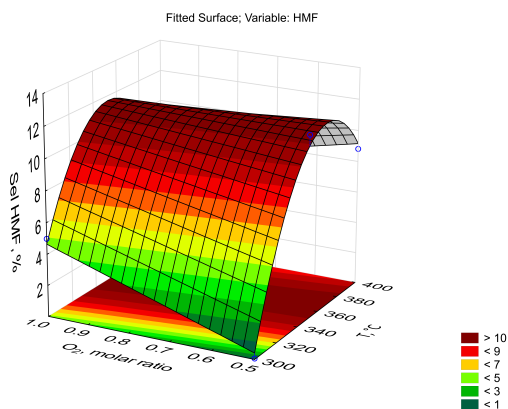


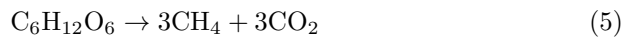
Figure 11: Surface chart of HMF selectivity with 1.5 g catalyst loading.

303 the data but excludes experiments for which the mass balance closure is less
 304 than 50%. The reason relates to the temperature, which was too low to react.

305 The CO_2 selectivity reached 20% while the maximum CO selectivity and
 306 CH_4 selectivity were 12% and 17%, respectively. The concentration of CO_2
 307 was highly correlated with CH_4 . Excluding experimental data for which the
 308 mass balance closed to below 50%

$$\text{CH}_4 = 1.2 \frac{\text{CO}_2}{W} \quad R^2 > 0.9 \quad (4)$$

309 where W is the mass of catalyst (Figure 12). Data CO_2 selectivity was es-
 310 sentially independent of temperature; it increased with the square-root of the
 311 O_2 :fructose ratio, and increased more than linearly with the mass of catalyst.
 312 Considering the complete decomposition to the stoichiometric lowest common
 313 denominator, we would expect a strong correlation between S_{CO_2} and S_{CH_4}



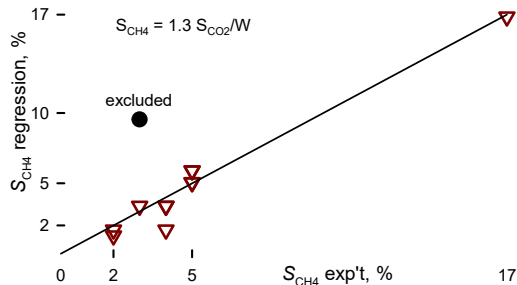


Figure 12: CH₄ parity plot. Data from 1 experiment was excluded because of the poor mass balance (closed circle).

314 or S_{CO} and S_{H_2O}



315 The strong correlation of the former could be related to the decomposition of a
 316 C₂ substrate like methylformate. Dimerization of formaldehyde leads to methyl-
 317 formate and this Tishchenko-like reaction is improbable at the reaction condi-
 318 tions. Feeding formalin across the reactor at these conditions would confirm
 319 this reaction mechanism. We exclude methanation as a reaction pathway and
 320 sequential combustion of methane from the oxygen in the fructose as this would
 321 produce water. Coke formation is related to the decomposition of the feed or
 322 the products on the catalyst and built up in all experiments and agglomerated.

323 3.4. HMF to DFF

324 We investigated the oxidation of HMF to DFF at four temperatures be-
 325 tween 250 °C to 400 °C and two catalyst loading, 1.5 g and 5 g, maintaining the
 326 O₂:HMF molar ratio of 2 (Table 4). Higher catalyst loading reacted all the
 327 HMF at the expense of DFF selectivity which approached at most 4%. On the
 328 other hand, at low catalyst loading and 350 °C or 400 °C DFF selectivity was
 329 26 % and 16 %, respectively. Conversion dropped to 86 % at 250 °C and DFF
 330 selectivity increased to 42 %.

Table 4: Higher contact time increase the degradation kinetic. Decreasing the temperature decreases the conversion but raise the DFF selectivity. The O₂:HMF ratio was 2 for all experiments.

Mass g	T °C	Conversion %	S_{CO_2} %	S_{CO} %	S_{FUR} %	$S_{5\text{MF}}$ %	S_{DFF} %
1.5	350	100	6	6	9	11	26
5	350	100	4	6	0	1	0
1.5	400	100	23	6	4	12	16
5	400	100	11	5	1	2	4
1.5	300	92	3	28	1	11	15
1.5	250	86	15	18	6	18	42

331 5MF, the main by-product of the reaction, is mainly controlled by temper-
 332 ature and catalyst inventory. In fact, at higher contact time, the selectivity
 333 dropped to 2%, while decreasing the temperature from 400 °C to 200 °C, the
 334 selectivity increased from 12% to a maximum of 18%. Furfural, the other main
 335 by-product, remained almost stable around 6% for all the reactions with lowest
 336 amount of catalyst, but ranged was 1% with 5 g of catalyst Coke built up on
 337 the catalyst, but was insensitive to either temperature or catalyst loading.

338 CO and CO₂ the selectivity varied considerably with both temperature and
 339 catalyst loading. At low temperature and low catalyst loading, CO was higher
 340 than CO₂, but increasing the two variables, the ratio became 1:1 and with a
 341 further increase CO₂ selectivity became higher than that of CO. The higher
 342 contact time increased the degradation of the molecules and carbon oxide selec-
 343 tivity increased with temperature.

344 4. Conclusions

345 Gas phase fructose oxydehydration is a new pathway to platform chemi-
 346 cals from organic feedstocks. It avoids organic solvents, decreases reaction time
 347 to fractions of a second, and facilitate product separation. Fructose first de-
 348 hydrates to HMF followed by tandem reactions to furfural, 5-MF, and DFF.

349 Other undesirable products are CO, CO₂, CH₄, and coke. The CH₄ is linearly
350 correlated with CO₂ while the selectivity to coke was highest among the prod-
351 ucts detected. Generally, the mass balance was greater than 50 % but for 5 of
352 the 18 experiments in the full factorial design it was less than this. HMF se-
353 lectivity from fructose reached 12 % at 350 °C. Other partial oxidation product
354 selectivities were less than 7 %. Even shorter contact times are required to im-
355 prove selectivity and reduce conversion. Since the catalyst induction time was
356 on the order of 2 h (the catalyst continued to activate), the product selectivities
357 are certainly higher. Coke built up on the catalytic surface, agglomerated the
358 catalyst but also covered the strongest acid sites, enhancing the selectivity to
359 the furanic compounds. Feeding HMF rather than fructose demonstrated that
360 lower temperatures are required to increase the furanic's selectivity.

361 **Acknowledgments**

362 The mobility of the authors has been facilitated by the Mitacs Globalink
363 Research Award (IT12679) and the Natural Sciences and Engineering Council
364 of Canada (Create Flow Chemistry, 449307-2014).

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