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Mechanical Reliability of Fullerene/Tin Oxide Interfaces in Monolithic Perovskite/Silicon Tandem Cells

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Michele De Bastiani, Giovanni Armaroli, Rawan Jalmood, Laura Ferlauto, Xiaole Li, Ran Tao, George T. Harrison, Mathan K. Eswaran, Randi Azmi, Maxime Babics, Anand S. Subbiah, Erkan Aydin, Thomas G. Allen, Craig Combe, Tobias Cramer, Derya Baran, Udo Schwingenschlögl, Gilles Lubineau, Daniela Cavalcoli, and Stefaan De Wolf, Mechanical Reliability of Fullerene/Tin Oxide Interfaces in Monolithic Perovskite/Silicon Tandem Cells, ACS Energy Letters 2022 7 (2), 827-833.

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Mechanical Reliability of Fullerene/Tin Oxide Interfaces in Monolithic Perovskite/Silicon Tandem Cells

- 4 Michele De Bastiani,* Giovanni Armaroli, Rawan Jalmood, Laura Ferlauto, Xiaole Li, Ran Tao,
- 5 George T. Harrison, Mathan K. Eswaran, Randi Azmi, Maxime Babics, Anand S. Subbiah, Erkan Aydin,
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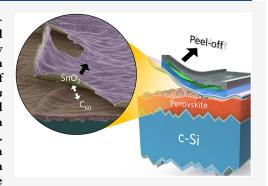
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8 ABSTRACT: High-efficiency perovskite-based solar cells comprise sophisti9 cated stacks of materials which, however, often feature different thermal
10 expansion coefficients and are only weakly bonded at their interfaces. This may
11 raise concerns over delamination in such devices, jeopardizing their long-term
12 stability and commercial viability. Here, we investigate the root causes of
13 catastrophic top-contact delamination we observed in state-of-the-art *p-i-n*14 perovskite/silicon tandem solar cells. By combining macroscopic and
15 microscopic analyses, we identify the interface between the fullerene electron
16 transport layer and the tin oxide buffer layer at the origin of such delamination.
17 Specifically, we find that the perovskite morphology and its roughness play a
18 significant role in the microscopic adhesion of the top layers, as well as the film
19 processing conditions, particularly the deposition temperature and the



20 sputtering power. Our findings mandate the search for new interfacial linking strategies to enable mechanically strong 21 perovskite-based solar cells, as required for commercialization.

n the past few years, monolithic perovskite/silicon tandems, combining perovskite and silicon solar cell technologies, have enabled high power conversion 25 efficiencies (PCEs) in a possible cost-effective way, which 26 holds great promise for their mass production. 1-3 To date, 27 most of the tandem research has focused on pursuing PCE 28 increases, 4-9 often by introducing sophisticated stacks of 29 materials. However, for commercialization, tandems need to be 30 integrated into solar panels, which may pose significant cell-to-31 module related technological challenges, 10 which urgently need 32 to be identified and mitigated. Conventional monofacial singlejunction crystalline silicon (c-Si) photovoltaic (PV) modules 34 consist of a front glass sheet, strings of series-connected c-Si 35 solar cells, sandwiched between two encapsulant layers (front 36 and rear, at present usually made from ethylene vinyl acetate, 37 EVA), and a polymeric backsheet. 10,11 This stack is then 38 laminated by vacuum annealing to melt and solidify the 39 encapsulant layers, which also aids in anchoring the strings of 40 cells in the module. For module integration of perovskite/ 41 silicon tandem solar cells, this process should be altered. 42 Indeed, due to the sensitivity of perovskites to moisture, 12 the 43 backsheet needs to be replaced with a rear glass sheet, acting as

a more effective barrier; such glass/glass module technology is 44 already well established for bifacial c-Si PV technology. 11 45 Moreover, classic module lamination tends to shrink the 46 encapsulant layers upon solidification, which can be several 47 centimeters over the module dimensions. We find this often to 48 cause tandem-device delamination, resulting in catastrophic 49 module failure. For lab-scale devices, this can be resolved by 50 removing the encapsulant layers and sealing the glass/glass 51 modules only at their edges, for instance with butyl-rubber 52 derivatives. 13-15 However, for larger modules, the absence of 53 encapsulants may compromise the anchoring and structural 54 stability of the strings of fragile cells. Therefore, understanding 55 and resolving tandem delamination is a key challenge toward 56 its commercialization. 16 In 2018, Cheacharoen et al. reported 57 on delamination of single-junction perovskite solar cells 58

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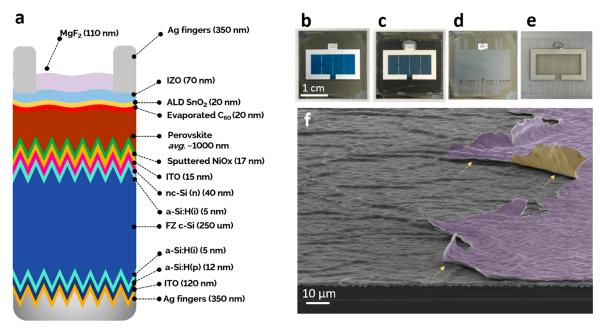


Figure 1. Delamination of the top electrode: (a) structure of the p-i-n tandem. (b) Picture of the tandem solar cell, (c) covered by tape, (d) after the peeling, with the emerging surface, and (e) peeled part left on the tape. (f) False-colored tilted SEM image of the peeled electrode. The peeled surface presents the typical wrinkles of the perovskite surface. The purple area represents the top of the Ag/MgF_2 electrode, while the yellow area the lift-off film that delaminated. The yellow arrows indicate the interface where delamination happens.

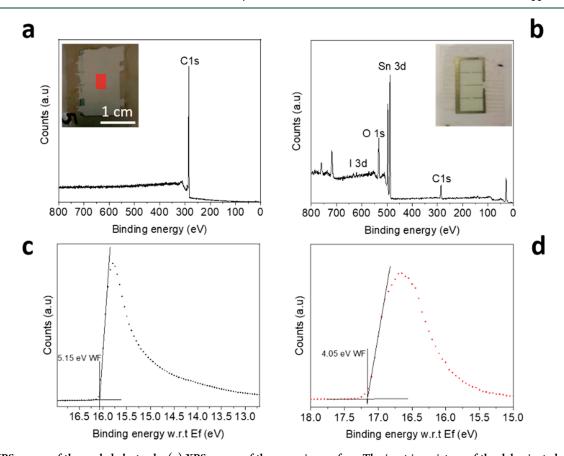


Figure 2. XPS survey of the peeled electrode. (a) XPS survey of the emerging surface. The inset is a picture of the delaminated sample. The red square represents the XPS probed area. (b) XPS survey of the peeled electrode. The inset represents the peeled electrode. (c) UPS spectrum of the emerging surface. (d) UPS spectrum of the peeled electrode.

₅₉ (PSCs) in the *p-i-n* architecture, the same configuration as ₆₀ most efficient perovskite/silicon tandems. ^{13,14} With double ₆₁ cantilever beam experiments, they found that the delamination

occurs within the electron-selective contact, particularly in the $_{62}$ phenyl-C61-butyric acid methyl ester (PCBM) film. This film $_{63}$ features the lowest fracture energy among the whole device $_{64}$

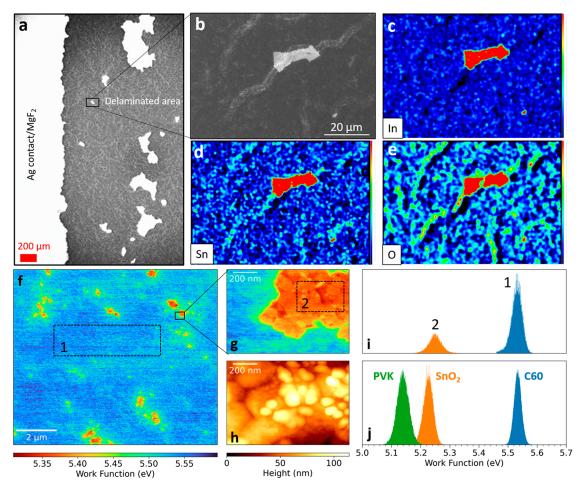


Figure 3. Microscopic investigation of the delamination. (a) Large area overview SEM image at the edge of the peeled area. (b) Closer SEM top-view image of the investigated area. (c-e) EDX mapping of indium, tin, and oxygen, respectively. (f) 10 μ m² KPFM map of a delaminated tandem solar cell. (g, h) 1 μ m² close-up of one of the residuals as measured by KPFM and dynamic AFM morphology, respectively. (i) Work function distributions of regions 1 (blue) and 2 (orange), corresponding to the regions delimited by dashed rectangles in f) and g). (j) Work function distributions of calibration samples consisting of Si/ITO/Perovskite (green), Si/ITO/perovskite/C₆₀ (blue), and Si/ITO/perovskite/C₆₀/SnO₂ (orange).

65 stack, resulting in its rupture under stress. 13,14 Here, we 66 thoroughly investigate the nature of delamination mechanism 67 in state-of-the-art p-i-n tandems (Figure 1a) by intentionally 68 peeling-off the top electrode (Figure 1b-e). We found that, 69 the top electrode fully delaminates, even preserving the pristine 70 conductivity of the front transparent contact (Figure S1). For 71 improved understanding of the delamination process, we 72 collected tilted-angle scanning electron microscopy (SEM) 73 images at the peeling interface (Figure 1f). At the bottom of 74 the image, the typical textured surface of the c-Si bottom cell is 75 visibly covered by the perovskite layer. The perovskite exhibits 76 on its surface the characteristic wrinkles induced during the 77 crystallization process. These wrinkles are induced by the 78 presence of Cs in the perovskite formulation and the presence 79 of the textured substrate underneath. 17 The purple area 80 highlights the top part of the contact (the Ag finger is covered 81 by the MgF₂ anti-reflective coating (ARC)) that is partially 82 lifted, while the yellow area represents the film that 83 delaminated.

f1

To identify the nature of the layers that delaminate, we so investigated both exposed surfaces of the failed device interface, with a combination of surface sensitive (1–10 nm) X-ray and ultraviolet photoelectron spectroscopies (XPS/ 88 UPS), energy dispersive X-ray analysis (EDX), and Kelvin

probe force microscopy (KPFM). Figure 2a shows the XPS 89 f2 survey scan of the films present on the surface emerging from 90 the tandem (red square in the inset). The spectrum shows the 91 typical feature of carbon in the form of fullerene (C_{60}) , a single 92 C1s peak, accompanied by characteristic shake-up satellite 93 features, 18 with traces of elements belonging to the perovskite, 94 but not of elements related to the contact (see Figure S2 for 95 more details). From the quantification of the peak areas, we 96 identified the material present on the tape (Figure 2b) as the 97 atomic layer deposited (ALD) SnO₂ buffer layer (film 98 composition: Sn 24 At%, O 42 At%, C 33% and a trace of I 99 of 0.5%). To further investigate, we acquired UPS spectra of 100 both samples with a depth sensitivity of ~1 nm. Figure 2c 101 shows the UPS spectrum of the surface emerging from the 102 tandem. The secondary electron cut-off (SECO) indicates a 103 work function (WF) of 5.15 eV, which matches well with that 104 of pristine C₆₀ measured independently on a freshly evaporated 105 C₆₀ layer as well as resulting in an acceptable ionization energy 106 (IE) of 6.50 eV (calculated from WF + VBM $- E_f$). Figure 2d 107 shows the SECO of the film present on the tape side. The 108 energy levels are univocally attributed to SnO2, with a deep 109 valence band at -7.90 eV (resulting in a WF of 4.05 eV). 19,20 110 The UPS analysis confirms the finding of the XPS analysis, 111 suggesting that the delamination happened on a macroscopic 112

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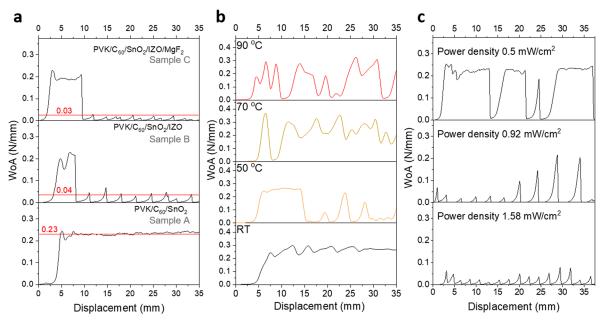


Figure 4. (a) 180-degree peel-off test for tandem test structures. PVK is the perovskite layer. Sample A (PVK/C60/SnO₂); sample B (PVK/ $C_{60}/SnO_2/IZO/SnO_2/IZO/SnO_2/IZO/MgF_2$). The red line averages the adhesion energy in N/mm. (b) 180-degree peel-off test for three identical test structures: PVK/ C_{60}/SnO_2 annealed at different temperatures: RT black, 50 °C orange, 70 °C yellow, 90 °C red. (c) Peel-off tests for tandem structures with the IZO layer deposited with different powers. The sample labeled 0.92 mW/cm² is the reference deposition for tandem applications.

 113 scale at the interface between the fullerene and the SnO_2 buffer 114 layer, as evidenced by the area bulk averaging property of the 115 techniques.

To understand the microscopic nature of the delamination 117 we combined EDX topography with KPFM mapping. Figure 118 3a shows a low-magnification SEM top view of the 119 delaminated interface of the tandem; the white bright side 120 represents the MgF₂ top layer, whereas the dark side is the 121 emerging surface. With a closer look, we noticed that the 122 delamination is not uniform. Indeed, we spotted several 123 micrometer-sized areas where the top contact appears to be 124 intact. Moreover, the morphology of the perovskite is not 125 perfectly flat, and we noticed a difference in contrast on top of 126 the wrinkles, induced by perovskite crystallization. Therefore, 127 we performed EDX topography on one of those regions, where 128 the top electrode overlaps on top of a wrinkle (Figure 3b). The 129 EDX mapping of In, Sn, and O (Figure 3c-e) clearly shows 130 that the bright area is part of the top electrode stack (which in 131 this region consists of the ALD-SnO₂ buffer layer and indium 132 zinc oxide (IZO) electrode) that did not delaminate with the 133 rest of the film. Moreover, we noticed traces of Sn and O on 134 top of the wrinkle, suggesting the presence of the SnO₂ buffer 135 layer. This is of significant importance since the microscopic 136 roughness of the materials can have a fundamental role in controlling the adhesion between the layers. To further investigate the microscopic nature of the delamination we took advantage of KPFM mapping in an argon ambient and in dark conditions, to avoid sample degradation during the measurement. Figure 3f shows a 10 μ m² KPFM scan of a delaminated tandem solar cell. This map confirms the nonuniformity of the delamination at the micrometer scale, with 144 clear presence of low WF residuals on top of a high WF 145 substrate. Figure 3g,h shows a 1 μm^2 KPFM and morphology 146 close-up of one of the residuals, respectively. We note the close 147 correlation between the WF map and morphology, confirming 148 that the micrometer-sized islands are residuals of a different

chemical species than the substrate. The morphology and 149 phase maps of the delaminated solar cell are reported in Figure 150 S3. Figure 3i shows the distribution of the WFs measured in 151 regions 1 (substrate) and 2 (residual), as indicated in Figure 2f 152 and 3g by dashed rectangles. To assess the nature of the two 153 species, we measured WF distributions of calibration samples 154 consisting of Si/ITO/perovskite, Si/ITO/perovskite/C₆₀, and 155 Si/ITO/perovskite/C₆₀/SnO₂ structures, shown in Figure 3l as 156 green, blue, and orange histograms, respectively. The KPFM 157 and morphology maps of the calibration samples are reported 158 in Figure S3. The WF values measured by KPFM on the 159 reference samples match well the values obtained by UPS scans 160 on the same samples, as shown in Figure S4. A comparison 161 with the distribution of the delaminated solar cell unequiv- 162 ocally shows that the exposed layer consists of a C₆₀ film with 163 SnO₂ residuals on top.

To better understand the delamination mechanism, we 165 performed density functional theory simulations of the $C_{60}/$ 166 SnO₂ interface to model the adhesion between the two 167 materials. Specifically, we studied various orientations of the 168 C_{60} molecule on the SnO-terminated (110) surface of SnO₂. 169 We found that the carbon atoms shared by pentagons and 170 hexagons of the C₆₀ molecule interact with both the Sn and O 171 atoms of the SnO₂ surface with a binding energy of -0.28 eV. 172 The optimized structure is shown in Figure S5. The Bader 173 charge analysis demonstrated a transfer of less than 0.02 174 electrons from the C₆₀ molecule to the SnO₂ surface. Finally, 175 we determined that the distance between the C₆₀ molecule and 176 SnO₂ surface is 3.22 Å, falling into the physisorption range. 177 With this information at hand, we then evaluated the fracture 178 energy of the C₆₀/SnO₂ interface, namely the work of adhesion 179 (WoA), using 180° peel-off measurements (Figure 4a). To 180 f4 isolate the fracture, we realized different test structures on top 181 of perovskite films that mimic the tandem architecture: $C_{60}/$ 182 SnO₂ (sample A), C₆₀/SnO₂/IZO (sample B), and C₆₀/SnO₂/ 183 IZO/MgF₂ (sample C). Surprisingly, we found that the WoA 184

185 between the C_{60} and the SnO_2 bilayer (\sim 0.23 N/mm) is 186 higher than that of the peeling tape interface (~0.20 N/mm, 187 see Figure S6). Indeed, we did not notice any delamination on 188 sample A. However, when the SnO₂ is capped with a sputtered 189 IZO layer as transparent electrode (sample B) we experienced 190 the same delamination behavior of the tandem itself, fracturing 191 at the C_{60}/SnO_2 interface. Moreover, we noticed that the 192 delamination happens via a slip-and-stick mechanism and, as 193 expected, is accentuated in the presence of film edges (see 194 Figure S7). From the delamination profile of sample B we 195 evaluated a WoA of 0.04 N/mm. Next, we found that coating 196 the IZO layer with an additional ARC layer of MgF₂ (sample 197 C) further reduces the WoA of the C₆₀/SnO₂ interface (0.03 198 N/mm). The MgF₂ layer is adopted at the single-cell level to 199 enhance the current response; it is not meant to be included at 200 the module level, since the encapsulant features a similarly low 201 refractive index. However, at the lab level and for practical 202 purposes, tandem devices are often laminated with MgF₂ either 203 for stability or outdoor performance evaluation. ^{4,21} In our case, 204 we found that the presence of MgF2 as second ARC is 205 deteriorating the long-term stability of the device, as it 206 enhances the possibility of delamination. However, the lower 207 adhesion energy attributed to the presence of IZO or MgF₂ is 208 not due to the layers themselves, but rather to a weakening of 209 the C₆₀/SnO₂ interface during the IZO sputtering or MgF₂ 210 thermal evaporation processes. Indeed, it is likely that during 211 these depositions the sample heats up, particularly during the 212 MgF₂ deposition (reaching temperature close to \sim 50 °C). The 213 higher temperature weakens the bonding between C₆₀ and 214 SnO₂, favoring the delamination process. Therefore, to validate 215 our hypothesis, we performed a second peel-off experiment 216 (Figure 4b) with four identical test-structures of perovskite/ 217 C₆₀/SnO₂ but annealed at different temperatures (room 218 temperature (RT) gray line, 50 °C orange line, 70 °C yellow 219 line, and 90 °C red line). The outcome of the experiment 220 validated our hypothesis. Indeed, the sample without annealing 221 (RT) showed a pattern similar to sample A in Figure 4a in 222 terms of profile and peeling force. On the contrary, a mild 223 annealing at 50 °C (and consistently at higher temperatures) 224 showed the clear features of delamination, as evidenced by the 225 pictures of the samples in Figure S8. Lastly, we shifted our 226 attention to the impact of the IZO deposition. The direct 227 deposition of TCOs by radio frequency (rf) sputtering is 228 known to possible create damage in the underlying layers. 22 229 Even in silicon heterojunction solar cell manufacturing the 230 TCO deposition is followed by an annealing step to recover 231 the damage done to the amorphous silicon contact layers 232 during such sputtering. In perovskite/silicon tandems, the 233 SnO₂ buffer layer protects the soft fullerene and perovskite 234 layers from the deposition of IZO. Figure 4a shows a clear 235 difference between sample A and B, suggesting that the IZO 236 deposition affects the WoA. Therefore, we deposited IZO 237 layers with different power densities: 0.5, 0.92, and 1.58 mW/ 238 cm², which represent soft deposition, our baseline deposition, 239 and a faster deposition conditions, respectively (all the films 240 share the same IZO thickness). Figure 4c shows the WoA 241 profiles for the three samples. We noted that there is a 242 correlation between the deposition power and the interfacial 243 mechanical properties. Indeed, at higher power the samples 244 delaminate easier, showing a lower WoA. To validate our 245 findings, we performed a statistical analysis over a batch of six 246 samples. Then we determined the average energy per sample 247 by integrating the WoA (Figure S9). The distribution clearly shows that the deposition of the IZO plays a key role in the 248 delamination and suggests that a precise control of the 249 deposition conditions is strategic to prevent this issue.

Few works in the past addressed delamination in PSCs. 251 Cheacharoen et al., investigated this problem at the single- 252 junction level and proposed the fracture of the PCBM layer, a 253 functionalized version of C_{60} , as the origin.^{13,14} Here we 254 propose that the delamination originates at the C₆₀/SnO₂ 255 interface with a neat separation of the two films at the 256 macroscopic level, but influenced by the perovskite roughness 257 at the microscopic level. Yet, in both cases, it is clear that the 258 presence of the fullerene (or its derivatives) poses a serious 259 roadblock toward the development of mechanically stable 260 perovskite-based solar cells. Indeed, the challenge is not limited 261 to the fabrication of modules, but also to the stability of the 262 performances. In real applications, the temperature of the 263 tandems can reach up to 50-60 °C at the peak-sun hours. 1,23 264 The periodic temperature changes typical for outdoor 265 performance impose cyclic stresses to the materials, in 266 particular to those that have different thermal expansion 267 coefficients. Therefore, it is of high urgency to address the 268 delamination issue at the widely used C₆₀ interface within the ²⁶⁹ perovskite community.

Fullerene-based n-type contacts are an iconic part of p-i-n 271 PSCs,²⁴ in particular thanks to their unique property in 272 reducing the hysteresis in the current-voltage character- 273 istic.^{25,26} Currently, there are no reasonable candidates that can ²⁷⁴ be used in this polarity configuration as an alternative to 275 fullerenes without losing performance, stability, or exacerbating 276 hysteresis.²⁷ Therefore, the best approach for p-i-n PSCs to 277 address delamination is the functionalization of the fullerene 278 and its surface.²⁸ In this direction, in tandems, particular ²⁷⁹ attention should be given toward the realization of a strong 280 chemical bond between the C₆₀ and the buffer layer (inserted 281 between C₆₀ layer and sputtered transparent top electrode), to 282 enable a proper lamination of stable perovskite/silicon 283 tandems. This bond can be enhanced either with an in situ 284 approach or with other layers deposited on top of the fullerene. 285 In both cases, the treatment must respect the perovskite 286 constrains, in terms of solvent compatibility and temperature 287 processing. In parallel, particular attention should be given to 288 preserve the electronic properties of the ETL and to avoid 289 parasitic absorption that can affect the current output of the 290 tandem. Lastly, we proved that the processing conditions for 291 the tandem fabrication have a significant role in delamination. 292 Temperature treatments or post-annealing treatments neg- 293 atively affect the weak adhesion between C₆₀ and SnO₂ and ²⁹⁴ they should be minimized or avoided completely. Moreover, 295 the impact of the sputtering process should be reduced for 296 example employing soft-landing depositions such as the hollow 297 cathode technique and the parallel sputtering configuration. 298

In this work, we showed the origin of the delamination in 299 perovskite/silicon tandem solar cells. Delamination is among 300 the most serious concerns for the manufacturing of tandem 301 modules and for the stability of the tandem performances, yet 302 hardly discussed to date. Contrarily to what has been reported 303 earlier for single-junction PSCs, we found that delamination 304 happens at the interface between the C_{60} extraction layer and 305 the SnO_2 buffer layer. Moreover, we realized that the adhesion 306 between the two layers is influenced by the perovskite 307 morphology; indeed, the wrinkles induced during the perov- 308 skite crystallization retain microscopically the adhesion 309 between the C_{60} and SnO_2 . This provides the opportunity in 310

311 the near future to engineer the roughness of the perovskite 312 layer in such a way that the probability for delamination to 313 occur is reduced. Furthermore, we showed that the temper-314 ature during the processing of the tandem has an influence on 315 the adhesion between the C_{60} and SnO_2 . Such an under-316 standing is pivotal to improve the tandem fabrication, toward 317 more stable performances.

8 ASSOCIATED CONTENT

9 Supporting Information

320 The Supporting Information is available free of charge at 321 https://pubs.acs.org/doi/10.1021/acsenergylett.1c02148.

Experimental section; peeling of the top electrode; XPS spectra after the peeling of the electrode; morphology and KPFM maps; work function comparison; DFT calculations; work of adhesion calibration and stick-and-slip behavior; effect of temperature on the delamination; statistic distribution of the work of adhesion as a function of the IZO sputtering power (PDF)

Video showing the 180° stick-and-slip behavior (MP4)

AUTHOR INFORMATION

331 Corresponding Authors

Michele De Bastiani – KAUST Solar Center (KSC), Physical 332 Sciences and Engineering Division (PSE), King Abdullah 333 University of Science and Technology (KAUST), Thuwal 334 23955-6900, Kingdom of Saudi Arabia; o orcid.org/0000-335 0002-4870-2699; Email: michele.debastiani@kaust.edu.sa 336 Stefaan De Wolf – KAUST Solar Center (KSC), Physical 337 Sciences and Engineering Division (PSE), King Abdullah 338 University of Science and Technology (KAUST), Thuwal 339 23955-6900, Kingdom of Saudi Arabia; o orcid.org/0000-340

0003-1619-9061; Email: stefaan.dewolf@kaust.edu.sa

Giovanni Armaroli – Department of Physics and Astronomy,

342 Authors

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University of Bologna, 40127 Bologna, Italy
 Rawan Jalmood – KAUST Solar Center (KSC), Physical
 Sciences and Engineering Division (PSE), King Abdullah
 University of Science and Technology (KAUST), Thuwal
 23955-6900, Kingdom of Saudi Arabia

Laura Ferlauto – Department of Physics and Astronomy,
University of Bologna, 40127 Bologna, Italy;
Interdepartmental Center for Industrial Research of the
University of Bologna (CIRI-MAM), 40136 Bologna, Italy;
orcid.org/0000-0003-2131-6795

Xiaole Li – King Abdullah University of Science and Technology (KAUST), Physical Science and Engineering Division, Mechanics of Composites for Energy and Mobility Lab., Thuwal 23955-6900, Saudi Arabia

Ran Tao – King Abdullah University of Science and Technology (KAUST), Physical Science and Engineering Division, Mechanics of Composites for Energy and Mobility Lab., Thuwal 23955-6900, Saudi Arabia

George T. Harrison – KAUST Solar Center (KSC), Physical Sciences and Engineering Division (PSE), King Abdullah University of Science and Technology (KAUST), Thuwal 23955-6900, Kingdom of Saudi Arabia

Mathan K. Eswaran – KAUST Solar Center (KSC), Physical Sciences and Engineering Division (PSE), King Abdullah University of Science and Technology (KAUST), Thuwal 23955-6900, Kingdom of Saudi Arabia

Randi Azmi – KAUST Solar Center (KSC), Physical Sciences	370
and Engineering Division (PSE), King Abdullah University of	371
Science and Technology (KAUST), Thuwal 23955-6900,	372
Kingdom of Saudi Arabia	373
Maxime Babics – KAUST Solar Center (KSC), Physical	374
Sciences and Engineering Division (PSE), King Abdullah	375
University of Science and Technology (KAUST), Thuwal	376
23955-6900, Kingdom of Saudi Arabia	
Anand S. Subbiah – KAUST Solar Center (KSC), Physical	377
	378
Sciences and Engineering Division (PSE), King Abdullah	379
University of Science and Technology (KAUST), Thuwal	380
23955-6900, Kingdom of Saudi Arabia; o orcid.org/0000-	381
0002-7505-3209	382
Erkan Aydin – KAUST Solar Center (KSC), Physical Sciences	
and Engineering Division (PSE), King Abdullah University of	384
Science and Technology (KAUST), Thuwal 23955-6900,	385
Kingdom of Saudi Arabia; o orcid.org/0000-0002-8849-	386
2788	387
Thomas G. Allen - KAUST Solar Center (KSC), Physical	388
Sciences and Engineering Division (PSE), King Abdullah	389
University of Science and Technology (KAUST), Thuwal	390
23955-6900, Kingdom of Saudi Arabia	391
Craig Combe – KAUST Solar Center (KSC), Physical	392
Sciences and Engineering Division (PSE), King Abdullah	393
University of Science and Technology (KAUST), Thuwal	
	394
23955-6900, Kingdom of Saudi Arabia	395
Tobias Cramer – Department of Physics and Astronomy,	396
University of Bologna, 40127 Bologna, Italy; o orcid.org/	397
0000-0002-5993-3388	398
Derya Baran – KAUST Solar Center (KSC), Physical Sciences	
and Engineering Division (PSE), King Abdullah University of	400
Science and Technology (KAUST), Thuwal 23955-6900,	401
Kingdom of Saudi Arabia; o orcid.org/0000-0003-2196-	402
8187	403
Udo Schwingenschlögl – KAUST Solar Center (KSC),	404
Physical Sciences and Engineering Division (PSE), King	405
Abdullah University of Science and Technology (KAUST),	406
Thuwal 23955-6900, Kingdom of Saudi Arabia;	407
orcid.org/0000-0003-4179-7231	408
Gilles Lubineau – King Abdullah University of Science and	409
Technology (KAUST), Physical Science and Engineering	410
Division, Mechanics of Composites for Energy and Mobility	411
Lab., Thuwal 23955-6900, Saudi Arabia; o orcid.org/	412
0000-0002-7370-6093	413
Daniela Cavalcoli – Department of Physics and Astronomy,	414
University of Bologna, 40127 Bologna, Italy; o orcid.org/	
0000-0002-2417-1248	415
0000-0002-241/-1248	416
Complete contact information is available at:	417
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